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* as contained within the document entitled "Guidelines for completing the monitoring report form (CDM-MR)" (EB 54 meeting report, annex 34).

MONITORING REPORT

Version ~~2.33.0~~ – ~~20/05/2012~~25/09/2012(dd/mm/yyyy)

N₂O ABATEMENT PROJECT OF CAPRO CORPORATION

4665

Monitoring period #1 (09/06/2011 – 31/08/2011)

SECTION A. General description of the project activity

A.1. Brief description of the project activity:

>>

1. Purpose of the project activity and the measures taken to reduce greenhouse gas emissions;
The proposed project is to reduce N₂O emissions of the tail gas emitted from Caprolactam production process in Capro Corporation (hereinafter “Capro”) by installing catalytic N₂O destruction system.
2. Brief description of the installed technology and equipments;
N₂O treatment system for this project is CRI N₂O abatement system, which is N₂O decomposition catalyst at the tail gas. Therefore, CRI system applies to tertiary treatment, which does not affect the existing yield of caprolactam as it just treats the tail gas. In addition, the catalyst system is remarkably efficient as CRI technology is direct N₂O decomposition process that does not require the addition of any reductant and its pressure drop is small.
3. Relevant dates for the project activity.

Relevant dates (dd/mm/yyyy)	The Actions for Implementation of Project activity
16/11/2010	Starting Construction of N ₂ O abatement system
23/03/2011	Conducting trial run after loading N ₂ O decomposition catalyst
15/04/2011	Installing of Measuring instruments including AMS
20/04/2011	Commissioning start(Plant 1)
27/04/2011	Commissioning start(Plant 2)
02/05/2011	Completing Construction of N ₂ O abatement system and the N ₂ O abatement system started normal operation
23/05/2011 ~27/05/2011	Field Test for Quality Assurance of installation and calibration of AMS (QAL2)
09/06/2011	Registration date of Project The starting date of the crediting period
26/9/2011 ~29/9/2011	Additional Field Test for Quality Assurance of installation and calibration of AMS (QAL2)

4. Total emission reductions achieved in this monitoring period: ~~144,869~~144.751tonCO₂e

A.2. Project Participants

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Name of Party involved	Project participants(*) (as applicable)	Party involved considered as project participants
The Republic of Korea(host)	Capro Corporation Hyosung Ebara Engineering Co., Ltd. Hyosung Corporation	No

A.3. Location of the project activity:

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The geographic location of the Capro caprolactam production plant is shown in Figure 1. The plant is located in the south-eastern part of the Republic of Korea: the east longitude is about 129.3280 and the north latitude is about 35.4958. The full address of this facility is 402-1, Bugok-dong, Nam-gu, Ulsan in Korea.

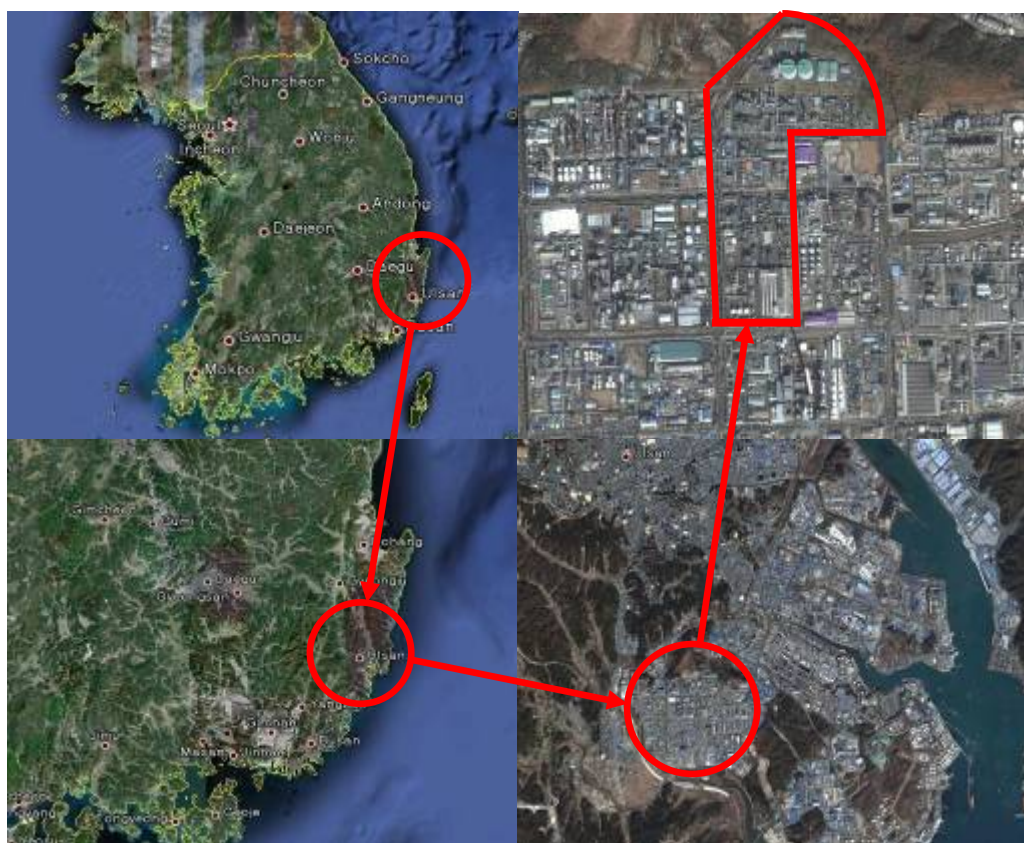


Figure A.1 The location of Capro caprolactam production plant

A.4. Technical description of the project

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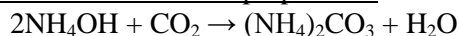
1. General Introduction

Caprolactam is produced by cyclohexane, ammonia, and sulphur as its primary raw materials, and Ammonium sulfate comes out as a by-product, which is supplied as nitrogen fertilizer and a chemical feedstock for industrial uses.

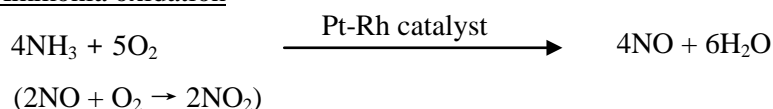
In Capro, the main process of caprolactam production is as follows:

Hydroxylamine sulfate preparation ;

Ammonium carbonate preparation



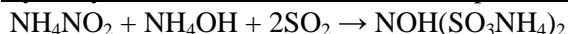
Ammonia oxidation



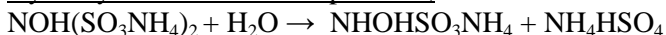
Ammonium Nitrite Preparation:



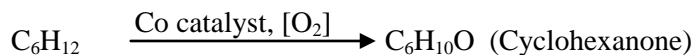
Hydroxylamine disulfonic ammonia Preparation:



Hydroxylamine Sulfate Preparation:



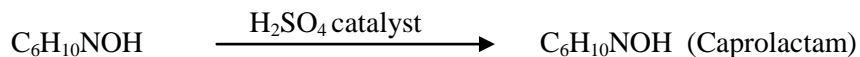
Cyclohexanone preparation



Oximation Reaction:



Beckmann rearrangement:



Cyclohexanone oxime reacts with sulfuric acid catalyst to caprolactam as final product. The structural formula of Beckmann rearrangement is shown in Figure 2.

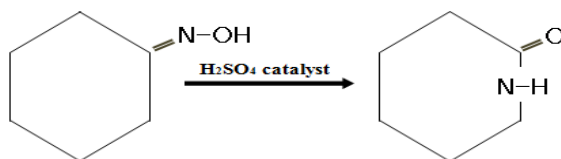


Figure A.2 Structural formula of Beckmann rearrangement

The block flow diagram for existed caprolactam production process of Capro is shown in Figure 3.

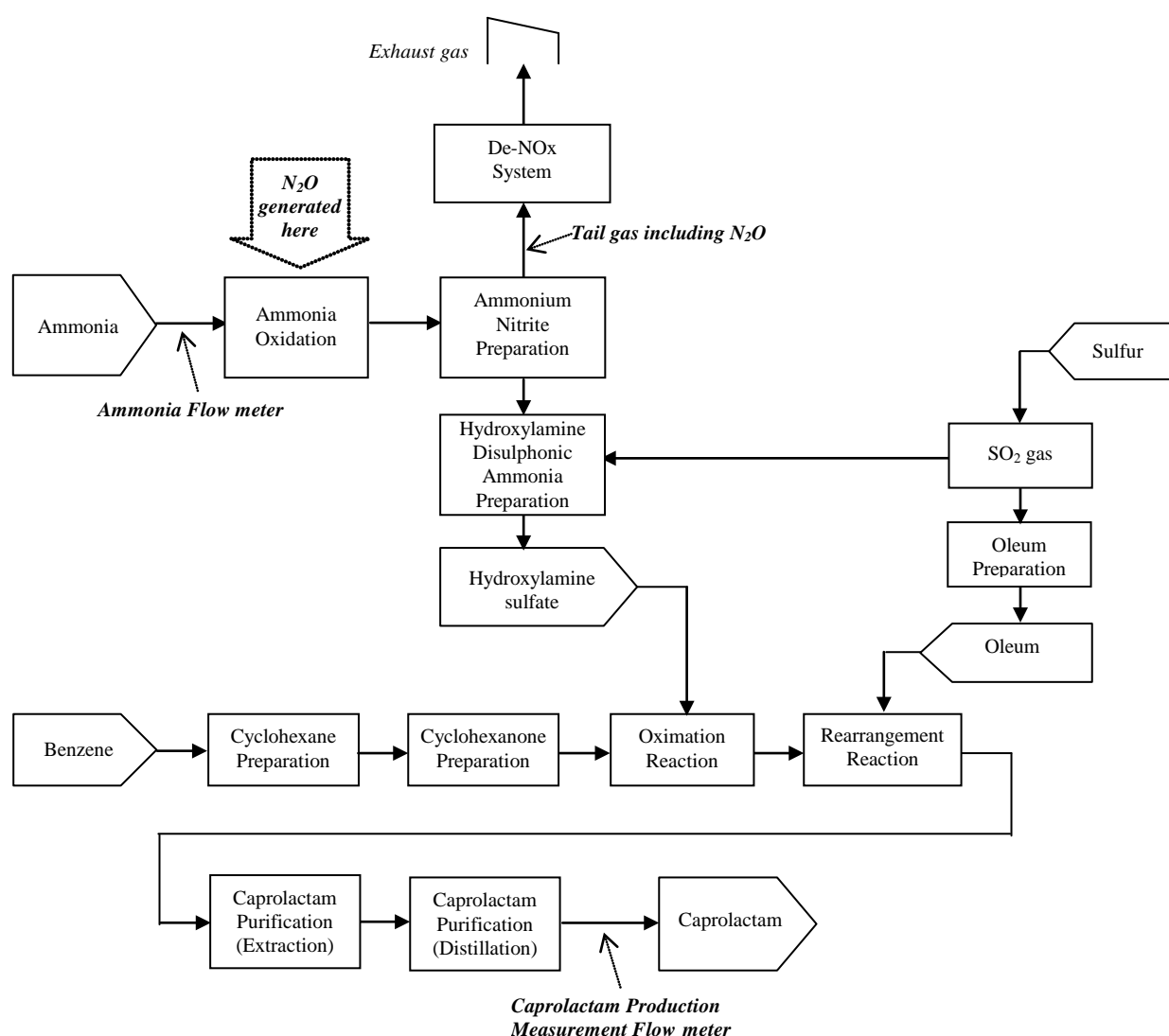
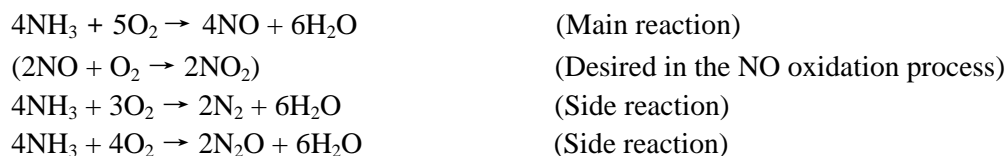


Figure A.3 Block flow diagram for caprolactam production process

Ammonia oxidation reaction is necessary to generate NO and NO₂, which are going to be the reactants for Ammonium nitrite. (This Ammonium nitrite will induce Hydroxylamine sulphate, and finally caprolactam will be produced, through the complicated reaction pathway, as previous stated at the paragraph to explain the main process of caprolactam production.)

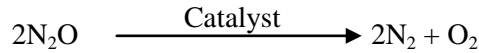
Nitrous oxide (N₂O) is generated as an undesired by-product through the side reaction of Ammonia oxidation as follows:



In this project, two plants (Plant I, Plant II) are included. In each plant, there are two of the Ammonium Oxidation Reactors (AORs), the ammonia gas is equally fed to the both of AORs through the one line with one flow meter. Input ammonia is oxidized by passing through the Pt-Rh Catalyst gauze located in AOR.

2. Project Specific description

De-N₂O system for this project is to destruct the N₂O included in tail gas by catalyst without any reducing agent.



The catalytic reactor designed by Hyosung Ebara Engineering Co. was derived from RTO (Regenerative Thermal Oxidizer), to save the energy required for catalytic reaction to decompose N₂O, and this N₂O destruction facility is the so-called “Regenerative Catalytic System” (Figure 4). Where, liquefied natural gas (LNG, hereafter “natural gas”) is put in to this system as a fuel, not reducing agent, to supply the energy required for the de-N₂O catalytic reaction. Catalyst is provided by CRI.

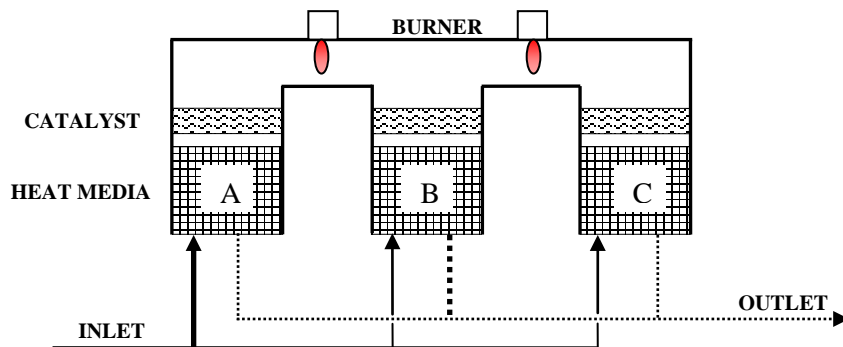


Figure A.4 Overview of Regenerative Catalytic System

The principle of performance can be step-wisely described with Figure 4 as follows: At the inlet of De-N₂O system, in-flowed tail-gas is heated up to 550 °C by going to heat media A (previously heated), before N₂O included in the heated tail is decomposed while that tail gas is pass through catalytic bed located on the top of heat storage media A. And then, N₂O in the once treated tail gas is decomposed again by the next catalyst bed and the heat storage media B, to which the heat hold in two-times-treated tail gas is transfer. After this, two-times-treated tail gas is going out. Next, tail gas is injected in to the heat media B which is charged with heat transferred from the outflow according to the way explain just above. And the tail gas passed through the heat storage media B and the upper catalyst bed is going to the other catalyst bed and the heat media C. Finally, the tail gas from the plant goes to the media C heated by the previous outflow, this tail gas is flowed reversely to the media B and comes out. In this way, tail gas in-and-out is continuously rotated. The same De-N₂O processes have been applied to Plant I and II.

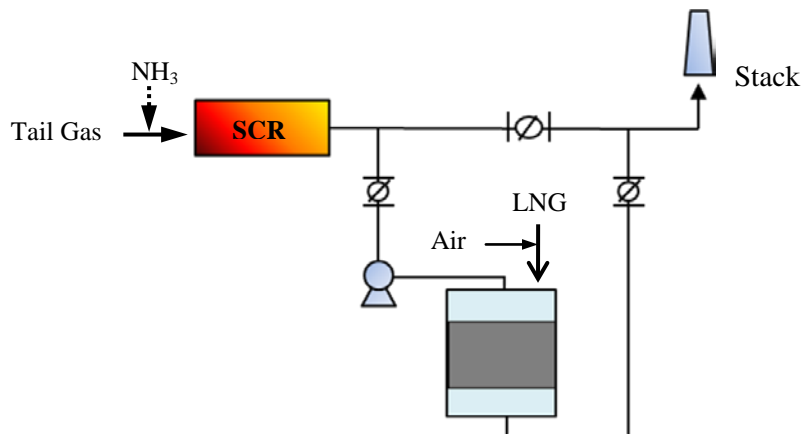


Figure A.5 Overview of the De-N₂O process in Plant I and II

A.5. Title, reference and version of the baseline and monitoring methodology applied to the project activity:

>>

AM0028 (version 05)

“Catalytic N₂O destruction in the tail gas of Nitric Acid Plants or Caprolactam Production”**A.6. Registration date of the project activity:**

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09/06/2011 (dd/mm/yyyy)

A.7. Crediting period of the project activity and related information (start date and choice of crediting period):

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	The date accepted by the Board
The starting date of the crediting period (dd/mm/yyyy)	09/ 06/2011
The length of the crediting period	10years(fixed)

A.8. Name of responsible person(s)/entity(ies):

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The person(s)/entity(ies) responsible for completing CDM-MR

	Capro Corporation	Hyosung Corporation	Hyosung Ebara Engineering Co., Ltd.
Name	Kim, Heung-jae	Choi, Yung-yul	Park, Jong-hoon
Position	Deputy Senior Manager	Junior Associate	General Manager
E-mail	z kim@hcccapro.co.kr	memories37@hyosung.com	heec-jh park@hyosung.com
Phone No.	+82-2-399-1243	+82-2-707-7586	+82-2-707-5841

SECTION B. Implementation of the project activity**B.1. Implementation status of the project activity**

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There is no special event or situation that occurred during the monitoring period which may impact the applicability

1. The starting date of operation of the project activity for both plants: 02/ 05/ 2011
(dd/mm/yyyy)

2. The Information of the actual operation in General

2.1 Operating condition of AOR

In order to avoid that the operation of the caprolactam production plant is manipulated in a way to increase the N₂O generation, thereby increasing the CERs, the operating temperature and pressure of

the ammonia oxidation reactor (AOR), and NH_3 input to the AOR, have been monitored every working day. During the monitoring period #1, actual average daily AOR operation conditions are monitored as below Table B.1.

Table B.1 Summary of the AOR operation data

Plant I		$T_{g,a}$ (°C)	$T_{g,b}$ (°C)	P_{g-1} (Pa)	$A_{OR,d-1}$ (NH_3/d)
	Permit range in PDD	656.57~731.66	662.08~743.92	43,320~98,564	42.250 (maximum)
	Actual average in period 1	712.79	739.33	85,967	38.98
	The number of days outside permit range	none	none	none	none
Plant II		$T_{g,c}$ (°C)	$T_{g,d}$ (°C)	P_{g-2} (Pa)	$A_{OR,d-2}$ (NH_3/d)
	Permit range in PDD	738.95~774.85	734.53~770.57	79,317~96,381	44.557 (maximum)
	Actual average in period 1	758.77	757.36	84,949	42.10
	The number of days outside permit range	1	1	none	none

For Plant I, all of daily average values of the AOR operation condition parameters have been kept within permit range. However, the daily average operating temperature values for two of AORs located at Plant II were deviated from the permit range on July 4, 2011. All of the data for the AOR operating condition were recorded in detail in the emission reductions calculation spreadsheet.

2.2 Ammonia Oxidation Catalyst

The first composition of ammonia oxidation catalyst used during the crediting period are the same kind of catalyst composition already in operation in the specific nitric acid or caprolactam production plant.

Table B.2 The status of ammonia oxidation catalysts installed in AOR

		Plant I	Plant II
Historical supplier of AOR catalyst $G_{com,hist}$		Pt(90%): Rh(10%)	Pt(90%): Rh(10%)
Historical composition of AOR catalyst $G_{sup,hist}$		Johnson Matthey	Johnson Matthey
in period 1	The composition (G_{com})	Pt(90%): Rh(10%)	Pt(90%): Rh(10%)
	Supplier (G_{sup})	Johnson Matthey	Johnson Matthey

2.3 Plant output of Caprolactam

In the case of a nitric acid plant or a caprolactam plant using the Raschig process, baseline emissions are limited to the design capacity of the existing nitric acid or caprolactam production plant. If the actual production of caprolactam ($P_{product}$) exceeds the design capacity ($P_{product,max}$) then emissions related to the production above $P_{product,max}$ will not be claimed for the baseline scenario. Therefore $P_{product}$ of each plant should be monitored.

However, it is not able to be decided whether the actual production of caprolactam exceeds $P_{product,max}$ or not, since those values should be compared on the annual values for comparing each other, and this period is first turn with the number of just 84 days. So, in order to simply make rough estimation to the status of production, the actual average daily output in period 1 was compared with the expected value

of that on the basis of PDD, as shown in Table B.3. As a result, it can be said that actual values are lower for both of plants.

Table B.3 the information of Caprolactam Production

		Plant I	Plant II
PDD	$P_{product, max}$ (tCaprolactam/yr)	63,307	64,965
	Maximum operating day(day/yr)	363	355
	Average daily output(ton/day)	174	183
Period 1	Sub-total output for period(tCaprolactam/day)	13,764	14,416
	No. of operating days(day/period)	84	84
	Average daily output(ton/day)	164	172

All of the data for the actual daily production of caprolactam were listed in detail in the emission reductions calculation spreadsheet.

3. The Information on Special Event

3.1 Events of Plant I

Events information

Initial inspection to the N₂O Abatement System (NAS) of Plant I was carried out on 9th June and 10th June, 2011. The solenoid valve on the N₂O gas inlet damper composing NAS was out of order, and this valve was replaced after by-pass valve was opened 23th of June, 2011. Also NAS system did not working well sometimes on 3rd to 5th of August, 2011. Product facility of Plant I has been unstable for about 5hours on July 25, 2011.

Action of Recalculation

Among the data generated during the time of event caused by shut down or inspection of NAS in Plant I, the data of the volume flow rate and N₂O concentration at the inlet and outlet of the destruction facility (F_{TI-1} , F_{TE-1} , CI_{N2O-1} and CO_{N2O-1}) have been excluded from the emission reduction calculation. Natural gas input for re-heating the tail gas (Q_{NG-1}) and CH₄ concentration at destruction facility outlet (CO_{CH4-1}) are not excluded in order to be conservative, even though those parameters are related with NAS operating. The data measured for the time of shut-down of the product facility were ignored, but the data of Q_{NG-1} and CO_{CH4-1} were considered for conservative calculation.

Here, all of the data of the volume flow rate and N₂O concentration at the inlet and out of the destruction facility (F_{TI-1} , F_{TE-1} , CI_{N2O-1} and CO_{N2O-1}) were measured at the dry basis, and the values were expressed on the same dry basis and should be corrected to normal conditions (101.325 kPa, 0 deg C).

Table B.4 The information of event of Plant I, and the action for calculation

Event		Date			Action for calculation
		dd/mm/yyyy	Time(hourly)		
			from	to	
N ₂ O	inspection	09/06/2011	0:00	24:00	Data from AMS to zero except LNG

Abatement System		10/06/2011	0:00	18:42	input and CH ₄ concentration at destruction facility outlet during the relevant time of event.
	Shut down	23/06/2011	10:03	11:40	
		03/08/2011	18:20	19:50	
		04/08/2011	11:29	24:00	
		05/08/2011	0:00	23:59	
Product Facility	Shut down	25/07/2011	16:08	20:43	All data to zero except LNG input, CH ₄ concentration at destruction facility outlet during the relevant time of event.

3.2 Events of Plant II

Events information

Inspection to the N₂O Abatement System (NAS) of Plant II was also performed on 9th and 10th of June, 2011. The increasing of the pressure of NAS in Plant II was detected with exceeding the normal operation condition range on 4th July, and so the NAS was shut down and fixed with replacing the EMV of RCS (2R-1521) to new one until 5th of July. Product facility of Plant II has been unstable for about 7hours, 19th to 20th of August 2011.

Action of Recalculation

Among the data generated during the time of event caused by shut down or inspection of NAS in Plant II, the data of the volume flow rate and N₂O concentration at the inlet and outlet of the destruction facility (F_{TI-2} , F_{TE-2} , CI_{N2O-2} and CO_{N2O-2}) have been excluded from the emission reduction calculation. Natural gas input for re-heating the tail gas (Q_{NG-2}) and CH₄ concentration at destruction facility outlet (CO_{CH4-2}) are not excluded in order to be conservative, even though those parameters are related with NAS operating. The data measured for the time of shut-down of the product facility were ignored, but the data of Q_{NG-2} and CO_{CH4-2} were considered for conservative calculation.

Here, all of the data of the volume flow rate and N₂O concentration at the inlet and out of the destruction facility (F_{TI-2} , F_{TE-2} , CI_{N2O-2} and CO_{N2O-2}) were measured at the dry basis, and the values were expressed on the same dry basis and should be corrected to normal conditions (101.325 kPa, 0 deg C).

Table B.5 The information of event of Plant II, and the action for calculation

Event		Date			Action for calculation
		dd/mm/yyyy	Time(hourly)		
			from	to	
N ₂ O Abatement System	inspection	09/06/2011	0:00	24:00	Data from AMS to zero except LNG input and CH ₄ concentration at destruction facility outlet during the relevant time of event.
		10/06/2011	0:00	21:40	
	Shut down	04/07/2011	8:36	24:00	
		05/07/2011	0:00	22:40	

Product Facility	Shut down	19/08/2011	18:55	24:00	All data to zero except LNG input and CH ₄ concentration at destruction facility outlet during the relevant time of event.
		20/08/2011	0:00	0:35	

B.2. Revision of the monitoring plan

>>

None

B.3. Request for deviation applied to this monitoring period

>>

None

B.4. Notification or request of approval of changes

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None

SECTION C. Description of the monitoring system

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1. Monitoring points to be measured

1.1 Monitoring Points in Plant I

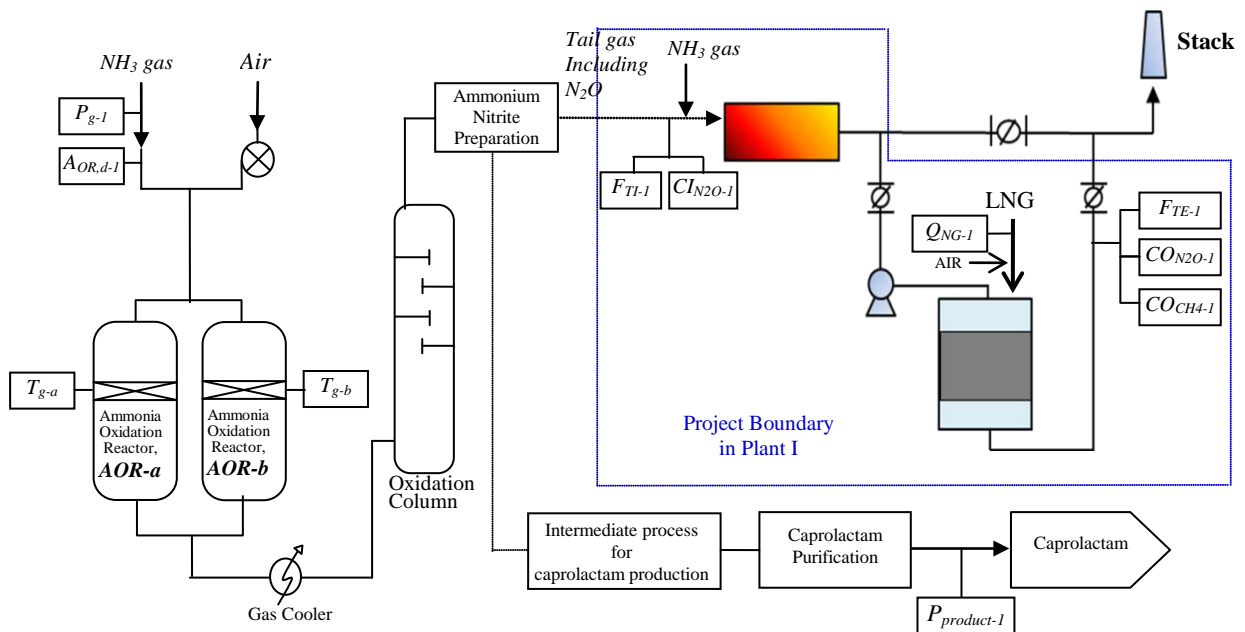


Figure C.1 Monitoring Points in Plant I

Parameter	Description	Tag No.
$A_{OR,d-1}$	Actual ammonia flow rate to AOR in Plant I	FIC-1201
P_{g-1}	Actual operating pressure of the AOR-a, b in Plant I	PI-1205
T_{g-a}	Actual operating temperature of the AOR-a in Plant I	TI-1204
T_{g-b}	Actual operating temperature of the AOR-b in Plant I	TI-1206

F_{TI-1}	Volume flow rate at the inlet of the destruction facility in Plant 1	FI-1521
F_{TE-1}	Volume flow rate at the exit of the destruction facility in Plant 1	FI-1522
CI_{N2O-1}	N_2O concentration at destruction facility inlet in Plant I	AI-1521
CO_{N2O-1}	N_2O concentration at destruction facility outlet in Plant I	AI-1522(a)
Q_{NG-1}	Additional natural gas input for re-heating the tail gas in Plant I	FI-1523
CO_{CH4-1}	CH_4 concentration at destruction facility outlet in Plant I	AI-1522(b)
$P_{product-1}$	Plant output of caprolactam in Plant I	FR-7705

Some tag numbers of measuring devices were change to avoid confusion, because the same tag number had been allocated to two kind of different measuring devices described in PDD. Therefore new tag numbers were given to be clearly identified as follows:

	Parameters	Tag No. in PDD	Actual Tag No. in Period#1
Plant I	CO_{N2O-1}	AI-1522	AI-1522(a)
	CO_{CH4-1}	AI-1522	AI-1522(b)

1.2 Monitoring Points in Plant II

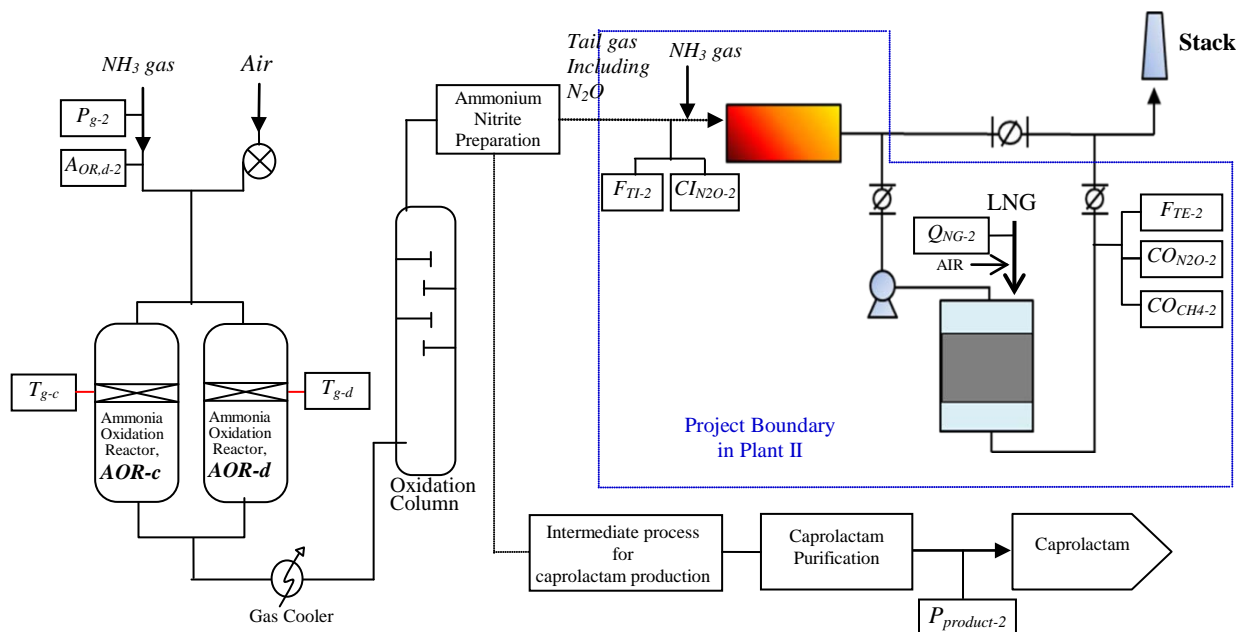


Figure C.2 Monitoring Points in Plant II

Parameter	Description	Tag No.
$A_{OR,d-2}$	Actual ammonia flow rate to AOR in Plant II	2FIC-1201
P_{g-2}	Actual operating pressure of the AOR-c, d in Plant II	2PI-1205
T_{g-c}	Actual operating temperature of the AOR-c in Plant II	2TI-1204
T_{g-d}	Actual operating temperature of the AOR-d in Plant II	2TI-1206
F_{TI-2}	Volume flow rate at the inlet of the destruction facility in Plant II	2FI-1521
F_{TE-2}	Volume flow rate at the exit of the destruction facility in Plant II	2FI-1522

CI_{N_2O-2}	N ₂ O concentration at destruction facility inlet in Plant II	2AI-1521
CO_{N_2O-2}	N ₂ O concentration at destruction facility outlet in Plant II	2AI-1522(a)
Q_{NG-2}	Additional natural gas input for re-heating the tail gas in Plant II	2FI-1523
CO_{CH_4-2}	CH ₄ concentration at destruction facility outlet in Plant II	2AI-1522(b)
$P_{product-2}$	Plant output of caprolactam in Plant II	2FI-7705

Some tag numbers of measuring devices were change to avoid confusion, because the same tag number had been allocated to two kind of different measuring devices described in PDD. Therefore new tag numbers were given to be clearly identified as follows:

	Parameters	Tag No.in PDD	Actual Tag No. in Period#1
Plant II	CO _{N₂O-2}	2AI-1522	2AI-1522(a)
	CO _{CH₄-2}	2AI-1522	2AI-1522(b)

2. Data Collection Procedure

The data of the AOR operating parameters (A_{OR} , T_g , P_g) and the productivity of caprolactam are logged and stored by the existed DCS (Distributed Control System) which has been independently operated for Plant I and II before starting this project.

Besides, DAS (Data Acquisition System) is newly installed to log the relevant data to the N₂O decomposition amount and CH₄ emission by operating N₂O abatement system. DAS consists of an 'Electronic Evaluation Unit (EEU)' and two of 'Data Communication Units (DCUs)' located at Plant I and II.

Major function of DCU is to record the raw measurement data from Automated Measuring System (AMS), and to transmit those to EEU. DCU can store temporarily the record of raw measurement data with the ring memory of 16days minute values. In addition, the data of AOR operation and caprolactam productivity are delivered from DCS and recorded by DCU respectably, and then transmitted to EEU. Q_{NG} is measured by Flow meter separately installed from AMS and CO_{CH₄} are also measured at the outlet by dual channel-NDIR by which the concentration of N₂O and CH₄ is measured separately. Therefore it is aggregated, recorded and stored by EEU that not only the AMS data but also the AOR data and productivity data. However, if there is a discrepancy between the DCS data and the EEU and/or DCU data, DCS data should be taken.

EEU satisfies the requirements described in AM0028 / Version 05 as below:

- Evaluation unit needs to take into account registration, mean average determination, validation, and evaluation;
- The system and concept of emission data processing needs to be described;
- Protocols and out-prints are required.

With EEU, these raw measurement data transmitted from DCUs are integrated after the measurement uncertainty determined by QAL 2 test is subtracted from them. Then, those are converted to the average values at the end of the every integration interval (1 hour), and validated. Negatively validated average values are set to zero. Validated average values outside the valid calibration range are to be stored with the associated time and with their status and are to be logged on EEU at the end of the day and year. EEU has the storage capacity of 5year-ring memory.

The calibration curve for the measuring instrument is determined using a standard reference method. The validity of the calibration curve is proved by EEU. The validity range for the calibration is specified in the calibration report. This calibration reports are printed and kept for back-up.

External hard disk drive (HDD) is installed for back-up and long storage of the data and relevant reports for verification, replaced by new one every 4 years, old HDDs are kept holding with attention during the 10years of crediting period and 2 additional years according to AM0028 / Version 05.

Table C.1 The information of the data collection and storage devices except DCS

		Supplier	Model No.	Serial No.
DCU(Data Communication Unit)	Plant 1	DURAG	D-EMS 500 KE	1301581
	Plant 2	DURAG	D-EMS 500 KE	1301582
EEU (Electronic Evaluation Unit)		DURAG	D-EMS 2000 SWE	1301567
External Hard disk drive(HDD) for backup		DURAG	D-EMS 2000 RED	1301578

The role of the new PC for back-up is to display and record the hourly data from EEU, the monthly data of supplied LNG, and the other information including the events list, working diary and so on.

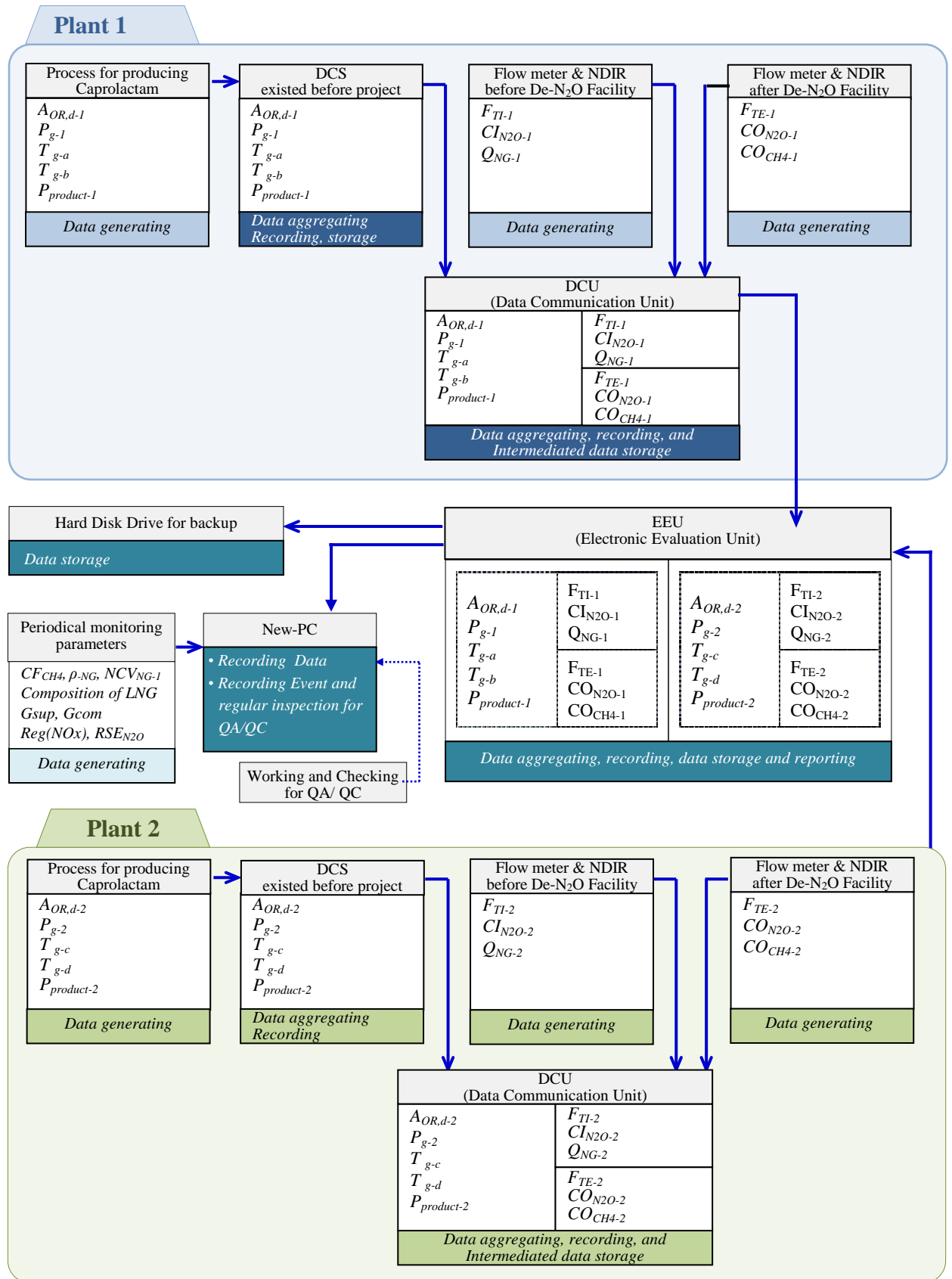


Figure C.3 Data Collecting Flow

3. Organization Structure, roles and responsibilities of personnel

3.1 Organization Structure

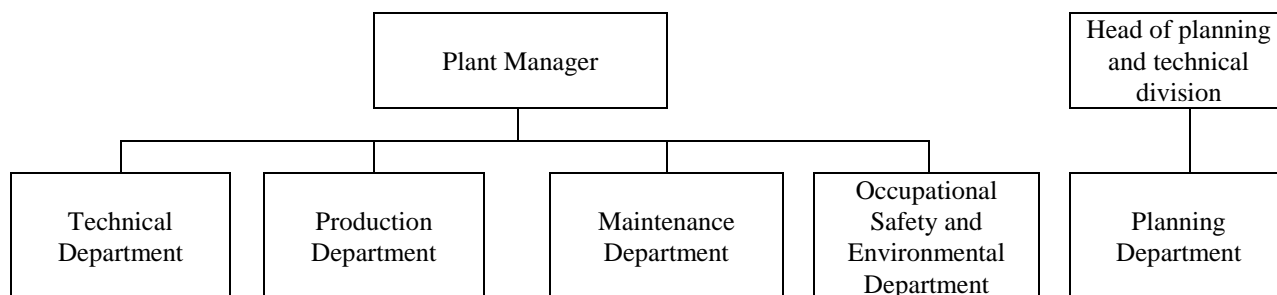


Figure C.4 The scheme of the operational and management structure

3.2 Roles and responsibilities of personnel

• Plant Manager

The Plant Manager takes overall responsibility for the operation and maintenance of the N₂O monitoring system. In addition, the Plant Manager has authority to approve monitoring report provided by the Technical Department.

• Production Department

The responsible Production Engineers in Production Department are in charge of the operation and supervision of N₂O monitoring system that will be implemented to record plant operation data.

• Technical Department

Monitoring engineers in Technical Department are responsible for collecting, validating and processing the data to determine GHG emission reduction and making report periodically. Moreover, the monitoring engineer is in charge of archiving the data as well. The monitoring engineers archive all required data and reports for verification.

• Maintenance Department

Maintenance Department is responsible for maintaining and repairing the instrument associated with this project. Calibration for instruments is concerned by maintenance department as well.

• Occupational Safety and Environment Department

The OSHES Department plays a role for indicating the direction and managing according to the monitoring plan.

• Planning Department

Planning Department conducts the internal audit of N₂O monitoring system periodically.

4. Emergency Procedures for the Monitoring system

In case of the data deviation, following procedures are taken.

- Production Engineer in Production Department identifies whether the deviation results from processing or other factors such as temperature and pressures.
- Production engineer compares the deviated data with other parameter data if the deviation results from processing.

- (c) If the reason for the data deviation is not identified, production engineer informs Maintenance Department to correct the error after inspecting all gauges and analysers.

If the data deviation is not covered by procedures above, Technical Department makes the decision to correct figures or to abandon the data. In addition, any data correction is in compliance with the applied methodology and done in a conservative bias

When the malfunction of measuring instruments is occurred, following procedures are taken.

- (a) If production engineer recognizes the malfunction of measuring instruments, he informs person in Maintenance Department of this abnormal situation.
- (b) Maintenance Department estimates whether performing repairing action to solve problem is appropriate or not.
- (c) If it is decided that self-repairing by Maintenance Department is appropriate, self-repairing is carried out. However, if the instrument is out of repair, Maintenance Department requests external institution specialized in repairing to have it serviced.

If measuring devices have to be replaced, related supporting evidences should be checked and kept by Maintenance Department, in order to demonstrate that the quality of the replaced measuring devices is the same as the quality grade of existed devices, before the copies of the supporting evidences to replaced devices should be delivered to and kept in the Technical Department.

Specially, if any malfunction situation of the measuring devices composing AMS(Automated measuring system) is continued during the 8hrs after it is detected, Maintenance Department should request the service of official measuring agency to measuring the N₂O concentration or flow rate at the monitoring points of inlet and outlet of N₂O decomposition system. If the services by the official measuring agency cannot be taken for some unavoidable reason, it will be taken instead of measuring by the external official measuring agency that the AMS data measured at the most similar operating condition among those of the recent 1 month just before the abnormal situation is happen, with the conservative understanding of that the N₂O concentration of inlet is replaced with the lowest number, and that of outlet is with highest one.

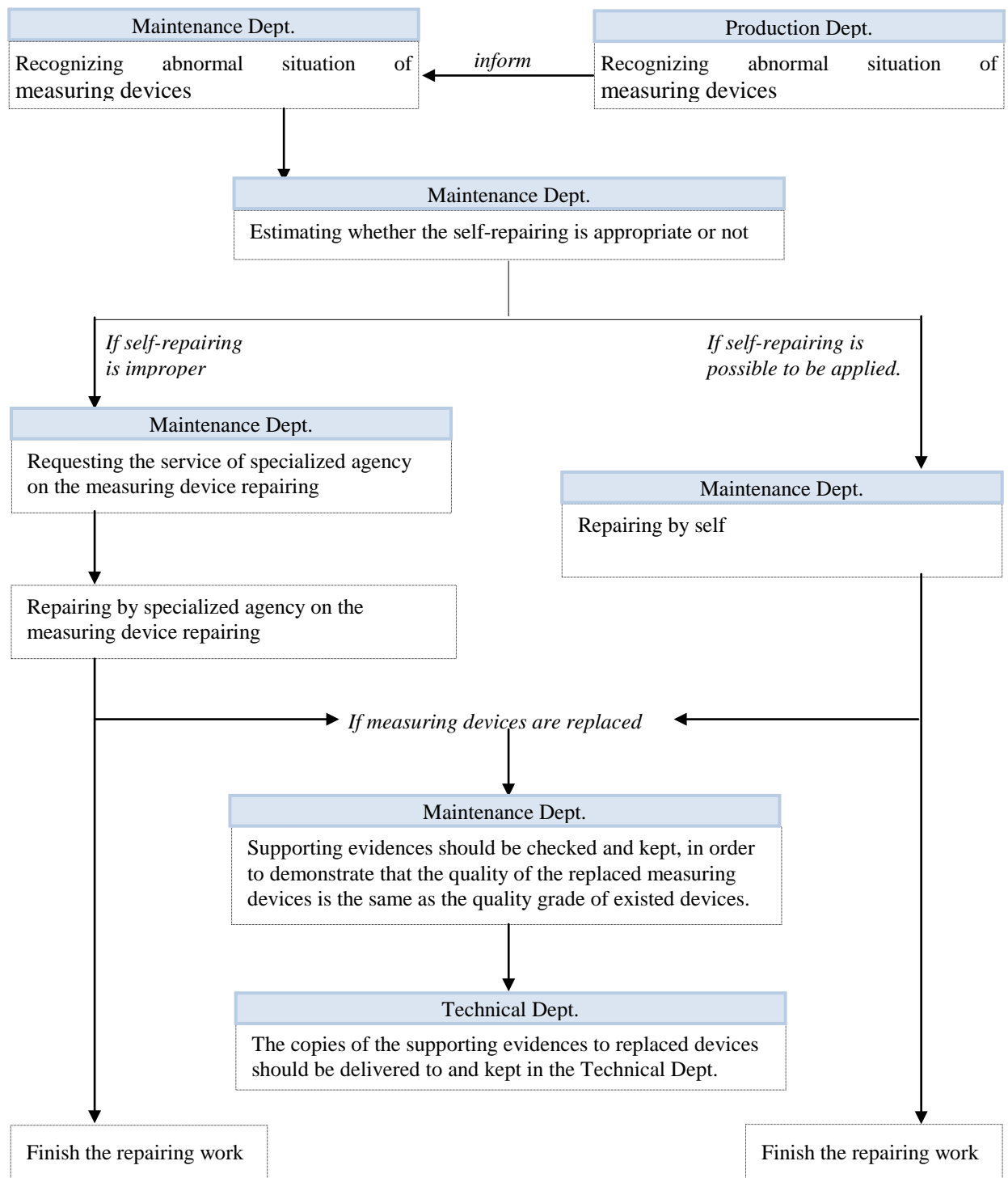


Figure C.5 Emergency Procedures for malfunctions of measuring devices in general

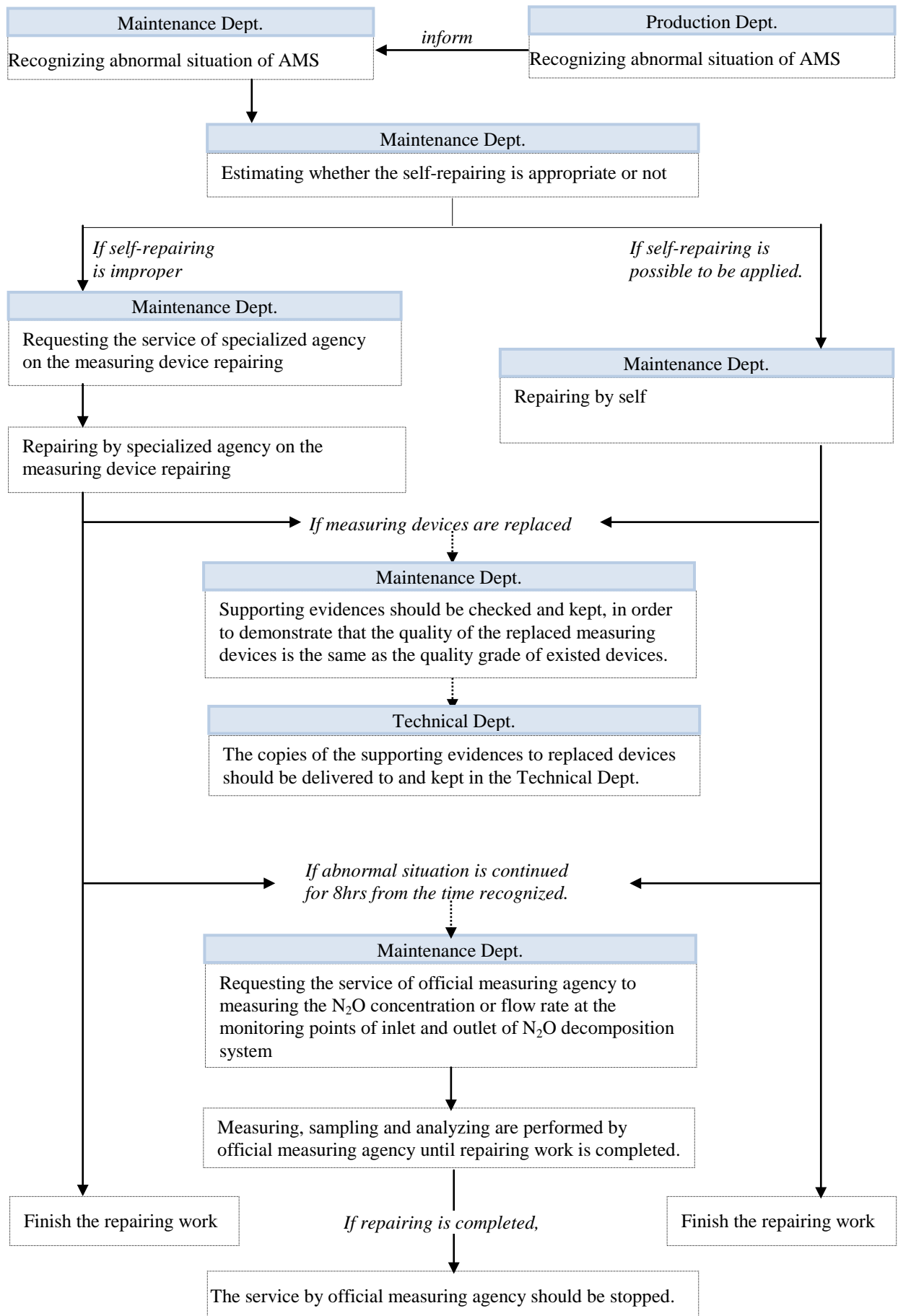


Figure C.6 Emergency Procedures for malfunction of AMS

5. Reporting

- **Daily report** consists of the parts printed out from EEU and from New-PC. EEU report is to show the data generated by AMS and related to the AOR operation condition and to the productivity of caprolactam. Daily value of each parameter is calculated based on hourly average or hourly total value on the EEU report. The situation of the AMS failure is also documented on the EEU report. The other hand, new-PC daily report is about checking and maintaining the measuring device and N₂O abatement system, and about monitoring events.
- **Monthly report** integrates the data and information in daily reports. LNG information is also reported monthly. Periodical monitoring parameters such as the composition and supplier of AOR catalysts, the national regulation on NO_x and N₂O are checked by monthly report too.
- **Annual report** is a bunch of monthly report files. However there is no annual report, because the this period is first and the length of the periods is just 84 days.

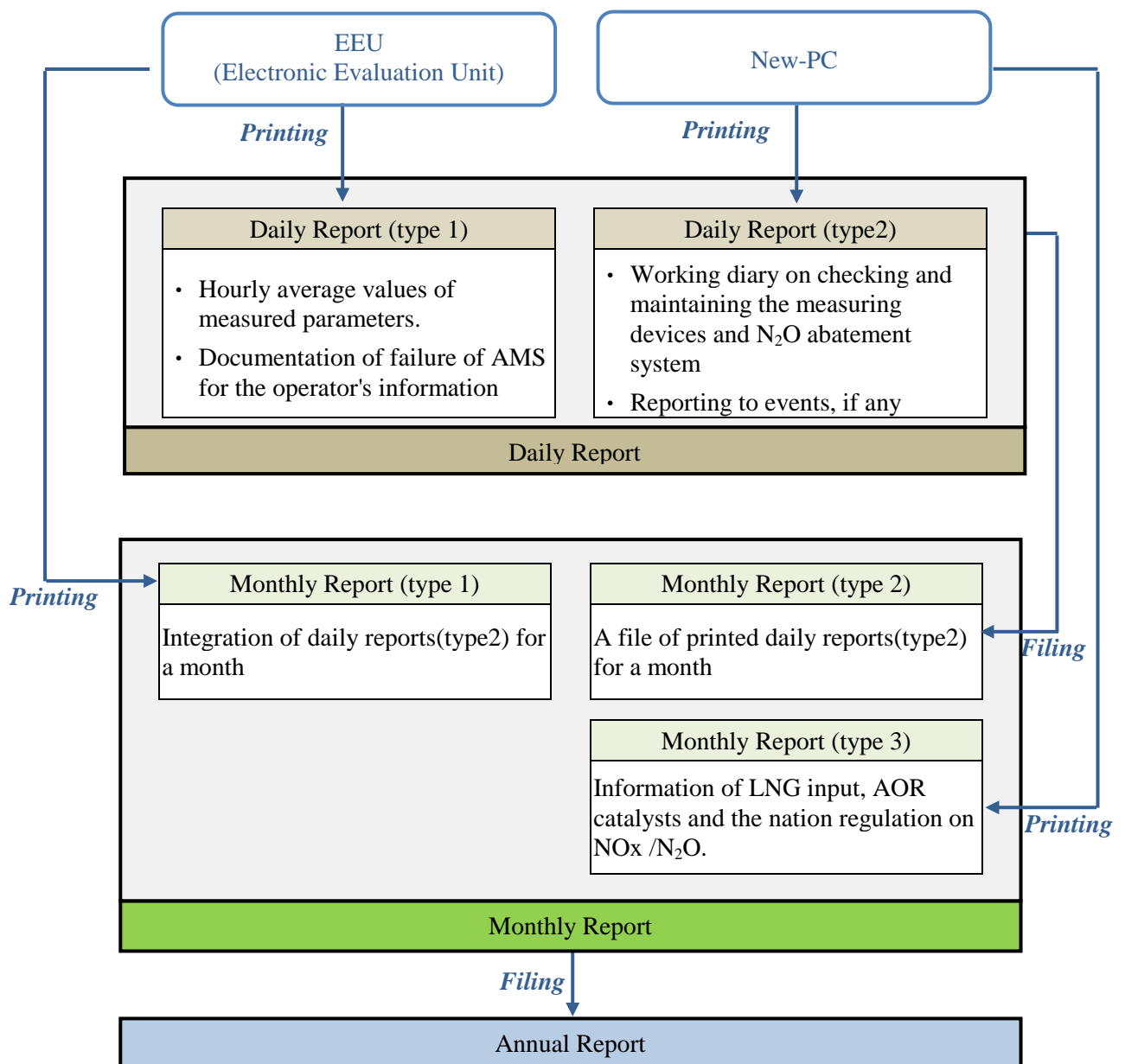


Figure C.7 The consists of the periodical reports

6. Quality Assurance of AMS(Automated measuring system)

AMS(Automated measuring system) has been applied to measure the amount of N₂O emission at the two monitoring points of the inlet and outlet of N₂O destruction facility of each plant involved in this project. By AMS, the concentration of N₂O and the volume flow rate of tail gas are measured simultaneously(F_{Ti}, CI_{N2O}, and F_{TE}, CO_{N2O}) at same basis (wet or dry), and these values are expressed on the same basis (wet or dry) with correcting to normal conditions (101.324kPa, 0deg C) through the algorithm based on procedures of EN14181.

“European Norm EN14181: Quality assurance of automated measuring systems, 2004” is selected as a guidance document to the Quality Assurance and Control procedure of the AMS for this project. This means that the three levels of quality assurance tests(QAL1, QAL2 and QAL3) and one annual functional test must be carried out regarding the selection, installation, and operation of AMS under the monitoring methodology in AM0028(ver.05).

Quality assurance of tested AMS (:QAL1)

The quality assurance of tested AMS was accomplished with that the flow meters and N₂O gas analyzers having the performance certificate with calculation uncertainty were selected as summarized in following tables.

Quality assurance of installation and calibration of AMS (:QAL2)

QAL 2 has been performed two times according to the Standard Reference Measurement Method (23/05/2011~27/05/2011 and 26/09/2011~29/09/2011) by AIR-TEC, which is the one of the organizations having an accredited quality assurance system on ISO/IEC 17025.

The results to the tests for QAL2 were summarized on the QAL 2 reports in the major items following:

- (a) Section of the location of measurement
- (b) Duly installation of the monitoring equipment
- (c) Correct choice of measurement range
- (d) Calibration of AMS using the standard-Reference-Method(SRM) as guidance
- (e) Calibration curve either as linear regression or as straight line from absolute zero to centre of a scatter-plot
- (f) Calibration of the standard deviation at the 95% confidence interval

Continuous quality Assurance through the local operator/manager (:QAL3)

QAL 3 has been implemented since the project start up. This includes:

- Permanent quality assurance during the plant operation by the operating staff
- Assurance of reliable and correct operation of the monitoring equipment
- Regular controls : zero point, span, drift, meet schedule of manufacturer maintenance intervals

Annual Surveillance test (AST)

Annual Surveillance test has not been carried out yet, because only 84 days have passed since the crediting period was started.

Table C.2 (a) Information of the quality assurance of tested AMS located in Plant I

Location	Parameters	Type	model	serial number	Standard for Performance certification	Certificate No.	The date of Certificate Issued (dd/mm/yyyy)	Approved methods to calculate of uncertainty
Inlet	F_{TE-1}	Ultrasonic flow meter	D-FL 200 System	HEAD A: 1217007 HEAD B: 1217008 EVALUATION UNIT : 1216861 CASE OF EVALUATION : 1216999	MCERTS	Sira MC 060072/01	22/05/2007	
	CI_{N2O-1}	Non-dispersion infrared absorption analyzer (NDIR)	ULTRAMAT 6	AO-748	TUV	Report Nr. 1290727	May 2009	
					TUV	BB-EG1-KAR Gr02X	29/07/2003	EN 50016 EN 60079-14 Guidelines for explosion protection of GB Chemie(GRG 104)
					FM Approvals	3016050	15/07/2003	
					CSA INTERNATIONAL	1431560	17/04/2003	
Outlet	F_{TE-1}	Ultrasonic flow meter	D-FL 200 System	HEAD A: 1217009 HEAD B: 1217010 EVALUATION UNIT : 1216862 CASE OF EVALUATION : 1217001	MCERTS	Sira MC 060072/01	22/05/2007	
	CO_{N2O-1}	NDIR	ULTRAMAT 6	AO-750	TUV	Report Nr. 1290727	May 2009	
					TUV	BB-EG1-KAR Gr02X	29/09/2003	EN 50016 EN 60079-14 Guidelines for explosion protection of GB Chemie(GRG 104)
					FM Approvals	3016050	15/07/2003	
					CSA INTERNATIONAL	1431560	17/04/2003	

Table C.2 (b) Information of the quality assurance of tested AMS located in Plant II

Location	Parameters	Type	model	serial number	Standard for Performance certification	Certificate No.	The date of Certificate Issued (dd/mm/yyyy)	Approved methods to calculate of uncertainty
Inlet	F_{TI-2}	Ultrasonic Flow meter	D-FL 200 System	HEAD A: 1217011 HEAD B: 1217012 EVALUATION UNIT : 1216866 CASE OF EVALUATION : 1217002	MCERTS	Sira MC 060072/01	22/05/2007	
	CI_{N2O-2}	NDIR	ULTRAMAT 6	AO-749	TUV	Report Nr. 1290727	May 2009	
					TUV	BB-EG1-KAR Gr02X	29/09/2003	EN 50016 EN 60079-14 Guidelines for explosion protection of GB Chemie(GRG 104)
					FM Approvals	3016050	15/07/2003	
					CSA INTERNATIONAL	1431560	17/04/2003	
Outlet	F_{TE-2}	Ultrasonic Flow meter	D-FL 200 System	HEAD A: 1217013 HEAD B: 1217014 EVALUATION UNIT : 1216867 CASE OF EVALUATION : 1217003	MCERTS	Sira MC 060072/01	22/05/2007	
	CO_{N2O-2}	NDIR	ULTRAMAT 6	AO-751	TUV	Report Nr. 1290727	May 2009	
					TUV	BB-EG1-KAR Gr02X	29/09/2003	EN 50016 EN 60079-14 Guidelines for explosion protection of GB Chemie(GRG 104)
					FM Approvals	3016050	15/07/2003	
					CSA INTERNATIONAL	1431560	17/04/2003	

7. Conservative calculation on tail gas flow

Measurement value by a flow meter at inlet of destruction facility (F_{TI}) and Measurement value by a flow meter at outlet of destruction facility (F_{TE}), both parameters shall be cross checked to ensure that no leak of N_2O is taking place, and in case of discrepancy, conservative calculation of emission reduction is provided. In order to achieve conservative approach, the measured inlet flow (F_{TI}) would be adjusted to the value (F_{TI}^*) by the below equation.

$$F_{TI}^* = \min \left[F_{TI} ; \left(\frac{F_{TE}}{1+VEF} - Q_{NG} \times \frac{Q_{NG \text{ combustion gas}}}{Q_{NG}} \right) \right]$$

Where:

- F_{TI}^* : Conservative volume flow at the inlet of destruction facility used for emission reduction calculation (Nm^3/h)
- F_{TI} : Measurement value by a flow meter at inlet of destruction facility (Nm^3/h)
- F_{TE} : Measurement value by a flow meter at outlet of destruction facility (Nm^3/h)
- Q_{NG} : Natural gas input for re-heating the tail gas (Nm^3/h)
- $Q_{NG \text{ combustion gas}}$: Combustion gas of natural gas (Nm^3/h)
- VEF : Volumetric Expansion Factor

For monitoring, the gas generated by combusting natural gas ($Q_{NG \text{ combustion gas}}$) has been estimated on the supposition that air input according to the theoretical oxygen demand on the natural gas composition which information is provided by the natural gas supplier for Capro (Kyung Dong city gas CO., Ltd).

And for the conservative approach, any volume change from De- NO_x and/or De- N_2O system will be considered by the Volumetric Expansion Factor (VEF). Before the first monitoring period, the Volumetric Expansion Factor (VEF) was determined as 0.001 which was provided by CRI, N_2O abatement catalysts supplier. This value of VEF is applied as a fixed official value.

8. Training

The supplier of the NDIR system provided complete training to the monitoring engineers in charge of operation and maintenance of the monitoring system. The provider of the De- N_2O system, (Hyosung Ebara Engineering Co., Ltd.) initiated the operation technique for the system to the staff in the Technical department of Capro.

SECTION D. Data and parameters

D.1. Data and parameters determined at registration and not monitored during the monitoring period, including default values and factors

Data / Parameter:	GWP_{N_2O}
Data unit:	Not applicable
Description:	Global warming potential of the nitrous oxide
Source of data used:	IPCC, The Second Assessment Report
Value(s) :	310
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline Emission / Project Emission
Additional comment:	Not applicable

Data / Parameter:	GWP_{CH_4}
Data unit:	Not applicable
Description:	Global warming potential of the methane
Source of data used:	IPCC, The Second Assessment Report

Value(s) :	21
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project Emission Calculation
Additional comment:	Not applicable

Data / Parameter:	$P_{product, max}$
Data unit:	t Caprolactam /yr
Description:	Design capacity of caprolactam production of the targeted line
Source of data used:	PDD
Value(s) :	$P_{product1, max}$: 63,307 ton/yr (design capacity in Plant I) for 363 days $P_{product2, max}$: 64,965 ton/yr (design capacity in Plant II) for 355 days Each plant has an individual design capacity.
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline Emission Calculation
Additional comment:	Not applicable

Data / Parameter:	$A_{OR, hist}$
Data unit:	tNH ₃ /day
Description:	Maximum of historical ammonia flow rate of the ammonia oxidation reactor (AOR)
Source of data used:	PDD
Value(s) :	$A_{OR, hist-1}$: 42.250tNH ₃ /d (total flow rate for AOR-a and AOR-b in Plant I) $A_{OR, hist-2}$: 44.557tNH ₃ /d (total flow rate for AOR-c and AOR-d in Plant II)
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline Emission Calculation
Additional comment:	Not applicable

Data / Parameter:	$T_{g, hist}$
Data unit:	°C
Description:	Historical operating temperature range of the ammonia oxidation reactor
Source of data used:	PDD
Value(s) :	$T_{g, hist-a}$: 656.57– 731.66°C (for AOR-a in Plant I) $T_{g, hist-b}$: 662.08–743.92 °C (for AOR-b in Plant I) $T_{g, hist-c}$: 738.95– 774.85°C (for AOR-c in Plant II) $T_{g, hist-d}$: 734.53– 770.57°C (for AOR-d in Plant II)
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline Emission Calculation
Additional comment:	Not applicable

Data / Parameter:	$P_{g, hist}$
Data unit:	Pa gauge
Description:	Historical operating pressure range of the ammonia oxidation reactor
Source of data used:	PDD
Value(s) :	$P_{g, hist-1}$: 43,320– 98,564 Pa gauge (for AOR-a and AOR-b in Plant I) $P_{g, hist-2}$: 79,317– 96,381 Pa gauge (for AOR-c and AOR-d in Plant II)

Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline Emission Calculation
Additional comment:	Not applicable

Data / Parameter:	$G_{sup,hist}$
Data unit:	-
Description:	Historical supplier of the ammonia oxidation catalyst
Source of data used:	PDD
Value(s) :	Name of the supplier: Johnson Matthey
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline Emission Calculation
Additional comment:	Not applicable

Data / Parameter:	$G_{com,hist}$
Data unit:	%
Description:	Historical composition of the ammonia oxidation catalyst
Source of data used:	PDD
Value(s) :	Pt (90%): Rh (10%)
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline Emission Calculation
Additional comment:	Not applicable

Data / Parameter:	$OXID_{HC}$
Data unit:	%
Description:	Oxidation factor of natural gas, with two or more molecules of carbon
Source of data used:	PDD
Value(s) :	100%
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project Emission Calculation
Additional comment:	Not applicable

Data / Parameter:	EF_{CH_4}
Data unit:	tCO ₂ /tCH ₄
Description:	Emission factor of methane
Source of data used:	PDD
Value(s) :	2.75(tCO ₂ /tCH ₄)
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project Emission Calculation
Additional comment:	Not applicable

Data / Parameter:	ρ_{CH_4}
Data unit:	t/m ³
Description:	Density of methane
Source of data used:	Tool to determine project emissions from flaring gases containing methane

Value(s) :	0.000716 t/m ³ (0°C, 1atm)
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project Emission Calculation
Additional comment:	Not applicable

Data / Parameter:	M_i
Data unit:	hour
Description:	Length of measuring interval
Source of data used:	AMS
Value(s) :	1 hour (to be measured continuously for 24 hours)
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline Emission Calculation / Project Emission Calculation
Additional comment:	Not applicable

Data / Parameter:	Reg_{NOx}
Data unit:	tNO _x /Nm ³
Description:	National regulation on NO _x emissions
Source of data used:	The “Clean Air Conservation Act”, one of the National environmental legislation, Ministry of Environment
Value(s) :	4.10714×10 ⁻⁷ tNO _x /Nm ³ (as a NO ₂ concentration)
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Not applicable
Additional comment:	Not applicable

D.2. Data and parameters monitored			
Data / Parameter:	$F_{TI,i}$		
Data unit:	Nm ³ /hr		
Description:	Volume flow rate at the inlet of the destruction facility		
Measured /Calculated/Default:	Measured		
Source of data:	Flow meter with normalizing functions		
Value(s) of monitored parameter:	For this period, the average values of F_{TI} :		
		Plant I ($F_{TI,1}$)	Plant II($F_{TI,2}$)
	F_{TI} (Nm ³ /hr) average	40,035.48	37,668.26
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline Emission Calculation		

Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)			
		Plant I ($F_{TI,1}$)	Plant II ($F_{TI,2}$)
	Type	Ultrasonic flow meter	Ultrasonic flow meter
	Accuracy class	< 2%	< 2%
	Serial No.	<ul style="list-style-type: none"> • HEAD A: 1217007 • HEAD B: 1217008 • Evaluation Unit :1216861 • Case of Evaluation : 1216999 	<ul style="list-style-type: none"> • HEAD A: 1217011 • HEAD B: 1217012 • Evaluation Unit :1216866 • Case of Evaluation : 1217002
	Calibration frequency	Every day by Auto calibration manner	Every day by Auto calibration manner
	Date of last calibration	31/08/2011	31/08/2011
	Validity	Yes	Yes
Measuring/ Reading/ Recording frequency:	<ul style="list-style-type: none"> •Measuring period : Continuously •Recording frequency : Hourly 		
Calculation method (if applicable):	Not applicable		
QA/QC procedures applied:	QAL 1, 2,3 and AST for AMS		

Data / Parameter:	$F_{TE,i}$		
Data unit:	Nm ³ /hr		
Description:	Volume flow rate at the exit of the destruction facility		
Measured /Calculated/Default:	Measured		
Source of data:	Flow meter with normalizing functions		
Value(s) of monitored parameter:	For this period, the average values of F_{TE}		
		Plant I ($F_{TE,1}$)	Plant II ($F_{TE,2}$)
	F_{TE} as Nm ³ /hr in average	44,414.55	46,001.72
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project Emission Calculation		
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)		Plant I ($F_{TE,1}$)	Plant II ($F_{TE,2}$)
	Type	Ultrasonic flow meter	Ultrasonic flow meter
	Accuracy class	< 2%	< 2%
	Serial No.	<ul style="list-style-type: none"> •HEAD A: 1217009 •HEAD B: 1217010 • Evaluation Unit : 1216862 • Case of Evaluation : 1217001 	<ul style="list-style-type: none"> •HEAD A: 1217013 •HEAD B: 1217014 • Evaluation Unit : 1216867 • Case of Evaluation : 1217003
	Calibration frequency	Every day by Auto calibration manner	Every day by Auto calibration manner
	Date of last calibration	31/08/2011	31/08/2011

	Validity	Yes	Yes
Measuring/ Reading/ Recording frequency:	•Measuring period : Continuously •Recording frequency : Hourly		
Calculation method (if applicable):	Not applicable		
QA/QC procedures applied:	QAL 1, 2,3 and AST for AMS		

Data / Parameter:	CI _{N2O,i}																							
Data unit:	tN ₂ O/Nm ³																							
Description:	N ₂ O concentration at destruction facility inlet																							
Measured /Calculated/Default:	Measured																							
Source of data:	Non-dispersion infrared absorption analyzer (NDIR)																							
Value(s) of monitored parameter:	For this period, the average values of CI _{N2O} : <table><tr><td></td><td>Plant I(CI_{N2O-1})</td><td>Plant II(CI_{N2O-2})</td></tr><tr><td>CI_{N2O,i} as tN₂O/Nm³</td><td>3.92561×10⁻⁶</td><td>3.06045×10⁻⁶</td></tr></table>				Plant I(CI _{N2O-1})	Plant II(CI _{N2O-2})	CI _{N2O,i} as tN ₂ O/Nm ³	3.92561×10 ⁻⁶	3.06045×10 ⁻⁶															
	Plant I(CI _{N2O-1})	Plant II(CI _{N2O-2})																						
CI _{N2O,i} as tN ₂ O/Nm ³	3.92561×10 ⁻⁶	3.06045×10 ⁻⁶																						
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline Emission Calculation																							
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	<table><tr><td></td><td>Plant I(CI_{N2O-1})</td><td>Plant II(CI_{N2O-2})</td></tr><tr><td>Type</td><td>NDIR</td><td>NDIR</td></tr><tr><td>Accuracy class (repeatability)</td><td>>95%</td><td>>95%</td></tr><tr><td>Serial No.</td><td>AO-748</td><td>AO-749</td></tr><tr><td>Calibration frequency</td><td>Every 2weeks</td><td>Every 2weeks</td></tr><tr><td>Date of last calibration</td><td>25/08/2011</td><td>25/08/2011</td></tr><tr><td>Validity</td><td>Yes</td><td>Yes</td></tr></table>				Plant I(CI _{N2O-1})	Plant II(CI _{N2O-2})	Type	NDIR	NDIR	Accuracy class (repeatability)	>95%	>95%	Serial No.	AO-748	AO-749	Calibration frequency	Every 2weeks	Every 2weeks	Date of last calibration	25/08/2011	25/08/2011	Validity	Yes	Yes
	Plant I(CI _{N2O-1})	Plant II(CI _{N2O-2})																						
Type	NDIR	NDIR																						
Accuracy class (repeatability)	>95%	>95%																						
Serial No.	AO-748	AO-749																						
Calibration frequency	Every 2weeks	Every 2weeks																						
Date of last calibration	25/08/2011	25/08/2011																						
Validity	Yes	Yes																						
Measuring/ Reading/ Recording frequency:	•Measuring period : Continuously •Recording frequency : Hourly																							
Calculation method (if applicable):	Not applicable																							
QA/QC procedures applied:	QAL 1, 2,3 and AST for AMS																							

Data / Parameter:	$CO_{N2O,i}$
Data unit:	tN ₂ O/Nm ³
Description:	N ₂ O concentration at destruction facility outlet

Measured /Calculated/Default:	Measured		
Source of data:	Non-dispersion infrared absorption analyzer (NDIR)		
Value(s) of monitored parameter:	For this period, the average values of CO_{N2O}		
		Plant I(CO_{N2O-1})	Plant II(CO_{N2O-2})
	$CO_{N2O,i}$ as tN ₂ O/Nm ³	3.81066×10 ⁻⁷	2.7285×10 ⁻⁷
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project Emission Calculation		
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)		Plant I(CO_{N2O-1})	Plant II(CO_{N2O-2})
	Type	NDIR	NDIR
	Accuracy class (repeatability)	>95%	>95%
	Serial No.	AO-750	AO-751
	Calibration frequency	Every 2weeks	Every 2weeks
	Date of last calibration	25/08/2011	25/08/2011
	Validity	Yes	Yes
Measuring/ Reading/ Recording frequency:	•Measuring period : Continuously •Recording frequency : Hourly		
Calculation method (if applicable):	Not applicable		
QA/QC procedures applied:	QAL 1, 2,3 and AST for AMS		

Data / Parameter:	$P_{product,y}$								
Data unit:	t Caprolactam/yr								
Description:	Plant output of caprolactam								
Measured /Calculated/Default:	Measured								
Source of data:	The value measured by Mass flow meter								
Value(s) of monitored parameter:	<table><tr><td></td><td>Plant I ($P_{product-1}$)</td><td>Plant II($P_{product-2}$)</td></tr><tr><td>$P_{product, period}$ (ton/period)</td><td>13,764</td><td>14,416</td></tr></table>				Plant I ($P_{product-1}$)	Plant II($P_{product-2}$)	$P_{product, period}$ (ton/period)	13,764	14,416
	Plant I ($P_{product-1}$)	Plant II($P_{product-2}$)							
$P_{product, period}$ (ton/period)	13,764	14,416							
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline Calculation								

Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)		Plant I ($P_{product-1}$)	Plant II ($P_{product-2}$)
	Type	Mass flow meter	Mass flow meter
	Accuracy class	$\pm 0.1\%$	$\pm 0.15\%$
	Serial No.	6T 681125	28 529138
	Calibration frequency	Every 2years	Every 2years
	Date of last calibration	07/10/2010	07/10/2010
	Validity	Yes	Yes
Measuring/ Reading/ Recording frequency:	•Measuring period : Continuously •Recording frequency : Hourly		
Calculation method (if applicable):	Not applicable		
QA/QC procedures applied:	Cross-check of amount of the produced caprolactam is performed on the basis of stock change data and weighbridge data.		

Data / Parameter:	$T_{g,d}$			
Data unit:	°C			
Description:	Actual daily (d) operating temperature of the ammonia oxidation reactor			
Measured /Calculated /Default:	Measured			
Source of data:	Thermocouple			
Value(s) of monitored parameter:	Average daily temperature (°C) of AOR in period #1			
	Plant I		Plant II	
	$T_{g,a}$ (°C)	$T_{g,b}$ (°C)	$T_{g,c}$ (°C)	$T_{g,d}$ (°C)
	712.79	739.33	758.77	757.36
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline Calculation			
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	The measuring instrument for T_{g-a} which is indicated in the registered PDD was replaced on May 2011. Even though the model number and Maker of the new measuring equipment are different from past one described in PDD, the type and the accuracy class of the equipment are the same.			
	Plant I	T_{g-a}		T_{g-b}
	Type	Thermocouple K		Thermocouple K
	Accuracy class (Maximum error)	300°C	+0.00°C	± 0.75°C
		500°C	+0.35°C	
		700°C	+0.98°C	
	Serial No.	2170447		09002677
	Calibration frequency	2 years		2 years
	Date of last calibration	13/05/2011		13/05/2011
	Validity	Yes		Yes
	Plant II	T_{g-c}		T_{g-d}

	Type	Thermocouple K		Thermocouple K	
	Accuracy class (Maximum error)	300°C	-0.7°C	300°C	-0.7°C
		500°C	-0.1°C	500°C	-0.1°C
		700°C	-0.7°C	700°C	-0.7°C
	Serial No.	24001		24002	
	Calibration frequency	Every 2 years		Every 2 years	
	Date of last calibration	23/05/2011		23/05/2011	
Validity	Yes		Yes		
Measuring/ Reading/ Recording frequency:	•Measuring period : Continuously •Recording frequency : Hourly				
Calculation method (if applicable):	Not applicable				
QA/QC procedures applied:	Every two years, the measuring instrument is calibrated by the authorized organization providing the calibration service on the basis of the national standard. Otherwise, the measuring instrument is replaced with new instrument calibrated according to the national standard.				

Data / Parameter:	$P_{g,d}$		
Data unit:	Pa gauge		
Description:	Actual operating pressure of the ammonia oxidation reactor on day d		
Measured /Calculated /Default:	Measured		
Source of data:	Pressure gauge		
Value(s) of monitored parameter:	Average daily Pressure (Pa/day) of AOR in period #1		
		Plant I (P_{g-1})	Plant II (P_{g-2})
	$P_{g,d}$ (Pa/day)	85,967	84,949
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline Calculation		
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)			
	Type	Plant I (P_{g-1})	Plant II (P_{g-2})
		Gauge Pressure	Gauge Pressure
	Accuracy class	$\pm 0.1\%$	$\pm 0.1\%$
	Serial No.	10530360183	10530360212
	Calibration frequency	Every 2 years	Every 2 years
	Date of last calibration	11/01/2010	11/03/2010
	Validity	Yes	Yes
Measuring/ Reading/ Recording frequency:	•Measuring period : Continuously •Recording frequency : Hourly		
Calculation method (if applicable):	Not applicable		
QA/QC procedures applied:	Every two years, the measuring instrument is calibrated by the		

	authorized organization providing the calibration service on the basis of the national standard. Otherwise, the measuring instrument is replaced with new instrument calibrated according to the national standard.
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Data / Parameter:	$A_{OR,d}$																							
Data unit:	tNH ₃ /day																							
Description:	Actual ammonia flow rate to the ammonia oxidation reactor (AOR)																							
Measured /Calculated /Default:	Measured																							
Source of data:	Differential pressure transmitter with normalizing functions																							
Value(s) of monitored parameter:	Average ammonia flow rate a day (tNH ₃ /day) of AOR in period #1																							
		Plant I($A_{OR,d-1}$)	Plant II($A_{OR,d-2}$)																					
	$A_{OR,d}$ (tNH ₃ /day)	38.98	42.10																					
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline Calculation																							
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	<table><tr><td></td><td>Plant I($A_{OR,d-1}$)</td><td>Plant II($A_{OR,d-2}$)</td></tr><tr><td>Type</td><td>Differential Pressure</td><td>Differential Pressure</td></tr><tr><td>Accuracy class</td><td>± 0.1%</td><td>± 0.1%</td></tr><tr><td>Serial No.</td><td>10530360038</td><td>10530360080</td></tr><tr><td>Calibration frequency</td><td>Every 2 years</td><td>Every 2 years</td></tr><tr><td>Date of last calibration</td><td>11/01/2010</td><td>11/03/2010</td></tr><tr><td>Validity</td><td>Yes</td><td>Yes</td></tr></table>				Plant I($A_{OR,d-1}$)	Plant II($A_{OR,d-2}$)	Type	Differential Pressure	Differential Pressure	Accuracy class	± 0.1%	± 0.1%	Serial No.	10530360038	10530360080	Calibration frequency	Every 2 years	Every 2 years	Date of last calibration	11/01/2010	11/03/2010	Validity	Yes	Yes
	Plant I($A_{OR,d-1}$)	Plant II($A_{OR,d-2}$)																						
Type	Differential Pressure	Differential Pressure																						
Accuracy class	± 0.1%	± 0.1%																						
Serial No.	10530360038	10530360080																						
Calibration frequency	Every 2 years	Every 2 years																						
Date of last calibration	11/01/2010	11/03/2010																						
Validity	Yes	Yes																						
Measuring/ Reading/ Recording frequency:	•Measuring period : Continuously •Recording frequency : Hourly																							
Calculation method (if applicable):	Since this parameter is measured																							
QA/QC procedures applied:	Every two years, the measuring instrument is calibrated by the authorized organization providing the calibration service on the basis of the national standard. Otherwise, the measuring instrument is replaced with new instrument calibrated according to the national standard.																							

Data / Parameter:	G_{sup}
Data unit:	Not applicable
Description:	Supplier of the ammonia oxidation catalyst
Measured /Calculated/Default:	Not applicable
Source of data:	Supplier information on catalyst delivery confirmation document
Value(s) of monitored parameter:	Johnson Matthey

Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline Calculation
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Not applicable
Measuring/ Reading/ Recording frequency:	Recording frequency : Date of changing catalyst
Calculation method (if applicable):	Not applicable
QA/QC procedures applied:	Not applicable

Data / Parameter:	G_{com}
Data unit:	%
Description:	Composition of the ammonia oxidation catalyst
Measured/Calculated/Default:	Not applicable
Source of data:	Supplier information on catalyst delivery confirmation document
Value(s) of monitored parameter:	Pt (90)% : Rh(10)%
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline Calculation
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Not applicable
Measuring/ Reading/ Recording frequency:	Recording frequency : Date of changing catalyst
Calculation method (if applicable):	Not applicable
QA/QC procedures applied:	Not applicable

Data / Parameter:	$Type_{HC}$
Data unit:	Not applicable
Description:	Type of hydrocarbon / Natural gas
Measured/Calculated/Default:	Not applicable
Source of data:	Natural gas supplier : KyungDong city gas CO., Ltd. This company is one of the city gas companies in the Republic of Korea. The most of natural gas supplied by KyungDong city gas CO., Ltd. is provided from Korea Gas Corporation (hereafter, KOGAS), which imports natural gas from around the world and supplies it to power generation plants, gas-utility companies and city gas companies throughout the country.
Value(s) of monitored parameter:	Natural Gas
Indicate what the data are used	Project emission

for (Baseline/ Project/ Leakage emission calculations)	
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Not applicable
Measuring/ Reading/ Recording frequency:	Monthly
Calculation method (if applicable):	Not applicable
QA/QC procedures applied:	Not applicable

Data / Parameter:	CF_{CH4}				
Data unit:	-				
Description:	Methane content of hydrocarbon, natural gas				
Measured /Calculated /Default:	Not applicable				
Source of data:	Information provided by the natural gas supplier				
Value(s) of monitored parameter:	The same kinds of natural gas are supplied to the Plant I and Plant II.				
	Date	June, 2011	July, 2011	August, 2011	Period1
	CF_{CH4}	0.9152	0.9158	0.9138	0.9149
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project Emission				
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Not applicable				
Measuring/ Reading/ Recording frequency:	Recording frequency : Monthly				
Calculation method (if applicable):	Not applicable				
QA/QC procedures applied:	Not applicable				

Data / Parameter:	$Q_{NG,y}$		
Data unit:	Nm^3		
Description:	Natural gas input for re-heating the tail gas		
Measured /Calculated/Default:	Measured		
Source of data:	Flow meter with normalizing functions		
Value(s) of monitored parameter:	Average daily value of Q_{NG} (Nm^3/day) in period #1		
		Plant I ($Q_{NG,1}$)	Plant II($Q_{NG,2}$)
	Q_{NG} (Nm^3/day)	473.34	847.02
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project emission		

Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)		Plant I ($Q_{NG,1}$)	Plant II ($Q_{NG,2}$)
	Type	Orifice	Orifice
	Accuracy class	$\pm 0.90\%$	$\pm 0.90\%$
	Serial No.	02319622	02319623
	Calibration frequency	Every 2 years	Every 2 years
	Date of last calibration	12/03/2010	12/03/2010
	Validity	Yes	Yes
Measuring/ Reading/ Recording frequency:	•Measuring period : Continuously •Recording frequency : Hourly		
Calculation method (if applicable):	Not applicable		
QA/QC procedures applied:	Every two years, the measuring instrument is calibrated by the authorized organization providing the calibration service on the basis of the national standard. Otherwise, the measuring instrument is replaced with new instrument calibrated according to the national standard.		

Data / Parameter:	$Q_{CH_4,y}$		
Data unit:	Nm^3/yr		
Description:	Methane part of the natural gas used.		
Measured /Calculated /Default:	Calculated		
Source of data:	Information provided by the natural gas supplier		
Value(s) of monitored parameter:	Average values of daily used ($Q_{CH_4,d}$)		
		Plant I	Plant II
	$Q_{CH_4,d}$ (Nm^3/day)	419.74	742.26
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project emission		
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Not applicable		
Measuring/ Reading/ Recording frequency:	Not applicable		
Calculation method (if applicable):	$Q_{CH_4,y} = Q_{NG,y} \times CF_{CH_4}$		
QA/QC procedures applied:	Not applicable		

Data / Parameter:	$Q_{HC,y}$
Data unit:	Nm^3 / yr
Description:	The hydrocarbon with two or more molecules of carbon in natural gas

Measured /Calculated /Default:	Calculated		
Source of data:	Information provided by the natural gas supplier		
Value(s) of monitored parameter:	Average values of daily used ($Q_{HC,d}$)		
		Plant I	Plant II
	$Q_{HC,d}$ (Nm ³ /day)	39.04	69.04
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project Emission		
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Not applicable		
Measuring/ Reading/ Recording frequency:	Not applicable		
Calculation method (if applicable):	$Q_{HC,y} = Q_{NG,y} \times (1 - CF_{CH4})$		
QA/QC procedures applied:	Not applicable		

Data / Parameter:	ρ_{NG}				
Data unit:	t/Nm ³				
Description:	Density of the natural gas				
Measured /Calculated /Default:	Not applicable				
Source of data:	Monthly report provided by the fuel supplier				
Value(s) of monitored parameter:		June, 2011	July, 2011	August□ 2011	Period 1
	ρ_{NG} (t/Nm ³)	□ 0.0007968	0.0007966	0.0007962	0.0007965
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project Emission				
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Not applicable				
Measuring/ Reading/ Recording frequency:	Recording frequency : Monthly				
Calculation method (if applicable):	Not applicable				
QA/QC procedures applied:	Not applicable				

Data / Parameter:	ρ_{HC}
Data unit:	t/m ³
Description:	Density of the hydrocarbon with two or more molecules of carbon in natural gas

Measured /Calculated /Default:	Calculated														
Source of data:	Information provided by the natural gas supplier														
Value(s) of monitored parameter:	<table><tr><td></td><td>June, 2011</td><td>July, 2011</td><td>August, 2011</td><td>Period 1</td></tr><tr><td>$\rho_{HC}(t/Nm^3)$</td><td>0.0016688</td><td>0.0016732</td><td>0.0016464</td><td>0.0016628</td></tr></table>						June, 2011	July, 2011	August, 2011	Period 1	$\rho_{HC}(t/Nm^3)$	0.0016688	0.0016732	0.0016464	0.0016628
	June, 2011	July, 2011	August, 2011	Period 1											
$\rho_{HC}(t/Nm^3)$	0.0016688	0.0016732	0.0016464	0.0016628											
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project emission														
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Not applicable														
Measuring/ Reading/ Recording frequency:	Not applicable														
Calculation method (if applicable):	$\rho_{HC} = (\rho_{NG} - \rho_{CH_4} \times CF_{CH_4}) / (1 - CF_{CH_4})$														
QA/QC procedures applied:	Not applicable														

Data / Parameter:	EF _{NG}				
Data unit:	tCO ₂ /tNG				
Description:	Emission factor of the natural gas				
Measured /Calculated /Default:	Calculated				
Source of data:	Information provided by the natural gas supplier				
Value(s) of monitored parameter:		June, 2011	July, 2011	Aug. 2011	Period 1
	EF _{NG}	2.7695	2.7701	2.7712	2.7703
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project emission				
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Not applicable				
Measuring/ Reading/ Recording frequency:	Not applicable				
Calculation method (if applicable):	$EF_{NG} = COEF_{NG} \times NCV_{NG} / \rho_{NG} \times 44/12$ Where $COEF_{NG}$: Carbon Emission factor of natural gas [tC/TJ] 15.3[tC/TJ] is applied to this project as Ex-ante value by IPCC DEFAULT VALUES OF CARBON CONTENT of “Natural Gas” in TABLE 1.3 (2006 IPCC Guidelines for National Greenhouse Gas Inventories Volume 2, Energy) NCV_{NG} : Net calorific value of the natural gas [TJ/Nm ³] For this project, NCV_{NG} is offered by KOGAS.				

	ρ_{NG} : Density of the natural gas[t/Nm ³] For this project, based on data source by natural gas supplier.
QA/QC procedures applied:	Not applicable

Data / Parameter:	EF_{HC}				
Data unit:	tCO ₂ /tHC				
Description:	Emission factor of the hydrocarbon with two or more molecular of carbon, which is existed as a contents of the natural gas				
Measured /Calculated/Default:	Calculated				
Source of data:	Calculated based on the followings: Methane content offered by the fuel supplier ; The density of the natural gas provided by the fuel supplier ; Estimated emission factor of the natural gas, and Specified methane density				
Value(s) of monitored parameter:		June, 2011	July, 2011	August, 2011	Period 1
	EF_{HC}	2.8598	2.8634	2.8690	2.8640
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project emission				
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Not applicable				
Measuring/ Reading/ Recording frequency:	Not applicable				
Calculation method (if applicable):	$EF_{HC} = (EF_{NG} \times \rho_{NG} - EF_{CH4} \times \rho_{CH4} \times CF_{CH4}) / (1 - CF_{CH4}) / \rho_{HC}$ Where EF_{NG} : CO ₂ emission factor of NG[tCO ₂ /tNG ρ_{NG} : Density of natural gas (tNG/m ³) EF_{CH4} : CO ₂ emission factor of CH ₄ (tCO ₂ /tCH ₄). ρ_{CH4} : Density of methane (tCH ₄ / m ³). CF_{CH4} : Methane fraction in the natural gas				
QA/QC procedures applied:	Not applicable				

Data / Parameter:	SE_{N2O}
Data unit:	kgN ₂ O/tCaprolactam
Description:	N ₂ O emission rate per ton of caprolactam

Measured /Calculated /Default:	Calculated								
Source of data:	Baseline and Monitoring Methodology (AM28 ver05)								
Value(s) of monitored parameter:	<div>Average:<table><tr><td></td><td>Plant I</td><td>Plant II</td></tr><tr><td>$SE_{N2O, period}$(kgN₂O/tCaprolactam)</td><td>22.0</td><td>15.39</td></tr></table></div>				Plant I	Plant II	$SE_{N2O, period}$ (kgN ₂ O/tCaprolactam)	22.0	15.39
	Plant I	Plant II							
$SE_{N2O, period}$ (kgN ₂ O/tCaprolactam)	22.0	15.39							
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission								
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Not applicable								
asuring/ Reading/ Recording frequency:	Not applicable								
Calculation method (if applicable):	$SE_{N2O, period} = QI_{N2O, period} / P_{product, period} \times 1000$ Where, $QI_{N2O, y}$ means Quantity of N ₂ O emissions at the inlet of the destruction facility (t N ₂ O)								
QA/QC procedures applied:	Not applicable								

Data / Parameter:	OXIDCH4								
Data unit:	%								
Description:	Oxidation factor of CH4 in natural gas for re-heating tail gas								
Measured /Calculated/Default:	Calculated								
Source of data:	Not applicable								
Value(s) of monitored parameter:	Average: <table><tr><td></td><td>Period 1</td><td>Plant II</td></tr><tr><td>OXIDCH4</td><td>93.64</td><td>98.16</td></tr></table>				Period 1	Plant II	OXIDCH4	93.64	98.16
	Period 1	Plant II							
OXIDCH4	93.64	98.16							
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project emission								
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Not applicable								
Measuring/ Reading/ Recording frequency:	Not applicable								
Calculation method (if applicable):	OXIDCH4={ QCH4 -(∑i^n FTE,i × COCH4,i × 10^-6) } / QCH4 × 100								
QA/QC procedures applied:	Not applicable								

Data / Parameter:	CO_{CH_4}		
Data unit:	ppm (v)		
Description:	Methane concentration at destruction facility outlet.		
Measured /Calculated /Default:	Measured		

Source of data:	Non-dispersion infrared absorption analyzer with dual-channel as a gas path		
Value(s) of monitored parameter:	Average:		
	CO_{CH4} (ppm)	Period 1	
	Plant I (CO_{CH4-1})	25.65	
	Plant II (CO_{CH4-2})	13.06	
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project emission		
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)		Plant I (CO_{CH4-1})	Plant II(CO_{CH4-2})
	Type	NDIR	NDIR
	Accuracy class	>95%	>95%
	Serial No.	AO-750	AO-751
	Calibration frequency	Every 2weeks	Every 2weeks
	Date of last calibration	25/08/2011	25/08/2011
	Validity	Yes	Yes
	Model	ULTRAMAT 6	ULTRAMAT 6
Measuring/ Reading/ Recording frequency:	•Measuring period : Continuously •Recording frequency : Hourly		
Calculation method (if applicable):	Not applicable		
QA/QC procedures applied:	Every two years, the measuring instrument is calibrated by the authorized organization providing the calibration service on the basis of the national standard. Otherwise, the measuring instrument is replaced with new instrument calibrated according to the national standard.		

Data / Parameter:	<i>Reg_{NOx}</i>
Data unit:	tNO _x /Nm ³
Description:	National regulation on NO _x emissions
Measured /Calculated/Default:	Not applicable
Source of data:	The “Clean Air Conservation Act”, one of the National environmental legislation, Ministry of Environment
Value(s) of monitored parameter:	4.10714×10^{-7} tNO _x /Nm ³ (as a NO ₂ concentration)
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Not applicable
Measuring/ Reading/ Recording frequency:	Not applicable

Calculation method (if applicable):	Recording frequency : Date of Regulation
QA/QC procedures applied:	Not applicable

Data / Parameter:	$RSE_{N_2O,y}$
Data unit:	tN ₂ O/tCaprolactam
Description:	Regulatory limit of N ₂ O emissions per unit of outlet of caprolactam (tN ₂ O/t caprolactam)
Measured /Calculated /Default:	Not applicable
Source of data:	National legislation in Republic of Korea. (That may be mostly like environmental regulation.)
Value(s) of monitored parameter:	Not applicable
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Not applicable
Measuring/ Reading/ Recording frequency:	Not applicable
Calculation method (if applicable):	Recording frequency : Date of Regulation
QA/QC procedures applied:	Not applicable

SECTION E. Emission reductions calculation

E.1. Baseline emissions calculation

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Based on the production of caprolactam during this first monitoring period, it is not available to be decided whether the yearly production ($P_{product,y}$) exceeds the design capacity ($P_{product,max}$). The actual daily Product is lower than suggested the daily of Product in PDD (page 80). Reference ER sheet AD line. Therefore on the assumption $P_{product,y} < P_{product,max}$, baseline emissions (BE) for this period are given by following equation :

$$BE_{period} = \left(\sum_i^n F_{TL,i} \times CI_{N_2O,i} \times M_i \right) \times GWP_{N_2O}$$

Where

M_i	Length of Measuring Interval (hr), (1hr : set value at instrument for this project)
GWP_{N_2O}	Global warming potential of the N ₂ O, (310: default value).
n	Number of intervals during this period
$F_{TL,i}$	Volume flow rate at the inlet of the DF during interval (Nm ³ /hr)
$CI_{N_2O,i}$	N ₂ O concentration in the tail gas of the DF inlet during interval (tN ₂ O/ Nm ³)

If the actual average daily operating temperature and/or pressure in the ammonia oxidation reactor (T_g

and P_g) are outside a “permitted range” of operating temperatures and/or pressures ($T_{g,hist}$ and $P_{g,hist}$), the baseline emission is integrated of the daily baseline emission($BE_{daily, out of permit range}$) for the respective day in which AOR operation conditions were outside of “permitted range”. The daily baseline emission is calculated for the respective time period as follows:

$$BE_{daily, out of permit range} = P_{product, day} \times EF_{N_2O} \times GWP_{N_2O} / 1000$$

Where

$BE_{daily, out of permit range}$	The daily daseline emission for the respective day in which AOR operation conditions were outside of “permitted range (tonCO ₂ /day)
$P_{product, day}$	The daily output of caprolactam for the respective day in which AOR operation conditions were outside of permitted range (ton caprolactam/day)
EF_{N_2O}	N ₂ O Emission factor to the process of caprolactam production (kgN ₂ O/ton caprolactam)

Emission factor of N₂O(EF_{N_2O}) is the lowest value among (a) $EF_{N_2O,IPCC}$, (b) $SE_{N_2O,y}$ and (c) any related value as a result of legal regulation(e.g. $RSE_{N_2O,y}$). In Republic of Korea, there is no mandatory regulation for N₂O emission. Therefore, actually EF of N₂O is the lower value between (a) $F_{N_2O,IPCC}$ and (b) $SE_{N_2O,y}$. $F_{N_2O,IPCC}$ means Conservative IPCC default value of the latest IPCC GHG Inventory Guidelines accepted by the IPCC for the equivalent N₂O emission process. At this time, $EF_{N_2O,IPCC}$ is 5.4kgN₂O/tonne of caprolactam.

$SE_{N_2O,y}$ is the specific N₂O emission per unit of output of caprolactam defined as :

$$SE_{N_2O,y} = QI_{N_2O,y} / P_{product,y} \times 1000$$

Where, $QI_{N_2O,y}$ means Quantity of N₂O emissions at the inlet of the destruction facility in year, y (t N₂O) given by :

$$QI_{N_2O,y} = \sum_i^n F_{TI,i} \times CI_{N_2O,i} \times M_i$$

For this period, $SE_{N_2O,y}$ should be converted as $SE_{N_2O,period}$ as follows :

$$SE_{N_2O,period} = QI_{N_2O, period} / P_{product,period}$$

On condition of that the actual daily ammonia flow rate exceeds the (upper) limit on maximum historical daily permitted ammonia flow rate, the baseline N₂O emissions for this operating day are capped at conservative IPCC default values. Where, the upper limit on ammonia flow should be determined based on “the historical operating data on maximum daily average ammonia flow”.

1. Plant I

BE in Plant I with AOR operation conditions within “permitted range”

Hourly BE (BE_{hr-l}) calculated on hourly integrated measured values of $F_{TI,i-l}$ and $CI_{N_2O,-li}$ are aggregated to the daily BE(BE_{day-l}), and total BE on the period ($BE_{period-l}$) are estimate as sum of BE_{day-l} . BE calculated on hourly input data is explained in detail on the emission reductions calculation spreadsheet

BE in case of AOR operation conditions outside of “permitted range”.

In case of Plant I, permit range of AOR operation condition has been kept for period 1. Therefore it is not necessary that the baseline emission calculation for period 1 depending on IPCC default values or ($SE_{N_2O,y}$) the specific N₂O emission per unit of output of caprolactam.

2. Plant II

BE by Plant 2 with AOR operation conditions outside of “permitted range”

Hourly BE (BE_{hr-2}) calculated on hourly integrated measured values of F_{Ti-2} and $CI_{N2O,i-2}$ are aggregated to the daily BE (BE_{day-2}), and total BE on the period ($BE_{period-2}$) are estimate as sum of BE_{day-2} . BE calculated on hourly input data is explained in detail on the emission reductions calculation spreadsheet.

Except 1day (4 July, 2011), all of daily average values of the AOR operation condition parameters have been kept within permit range. So, it is excluded for calculation that measured values of relevant parameters with BE calculation ($F_{Ti,2}$, and $CI_{N2O,i}$) of the day in which AOR was operated outside of permit range.

BE in case of AOR operation conditions outside of “permitted range”.

In order to determined the daily BE (BE_{day-2}) to the day in which AOR was operated outside of permit range, EF_{N2O} is determined to 5.4 kgN₂O/tCaprolactam because that it the the lower value between (a) $F_{N2O,IPCC}$ and (b) $SE_{N2O,period}$ as below table. The RSE_{N2O} is no mandatory regulation for N₂O emission in the Republic of Korea at present. Change in N₂O regulation will automatically cause a re-assessment of the baseline scenario.

Table E.1 $SE_{N2O,period}$ of period 1 of Plant II on 4 July, 2011

EF_{N2O}	Value	Unit	Note		
$EF_{N2O,IPCC}$	5.4	kgN ₂ O/tCaprolactam	parameter	Values	Unit
$SE_{N2O,period}$	15.39	kgN ₂ O/tCaprolactam	$QI_{N2O,period.2}$ (total)	221.82	ton N ₂ O/period
			$P_{product,period,-2}$	14415.80	ton/period

Table E.2 BE in Plant 2 with AOR operation conditions outside of “permitted range”

No. of times	Date (dd~dd/mm/yyyy)	$P_{product, day, out of permit range}$ (t Caprolactam/day)	$BE_{daily, out of permit range}$ (tonCO ₂ /day)
1	04/07/2011	170.77	285.87 285.869
Period Total of $BE_{periodout of permit range}$ (tonCO ₂ /period)			285.87 285.869

3. The total BE of Period 1

Eventually, Total BE in this period is ~~162,628~~162,628.267ton CO₂ as shown below table

Table E.3 BE in Period#1

		BE _{period-1} (ton CO ₂ /period)	
		BE _{period-1} in Plant I	BE _{period-1} in Plant II
BE_{period} on AOR condition	within “permitted range	93,882 93,881.790	68,461 68,460.608
	Outside “permitted range	0	285.87 285.869
BE_{period} total	BE _{period} for plant	93,882 93,881.790	68,746 68,746.477
	BE _{period}	162,628 162,628.267	

E.2. Project emissions calculation

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The emission due to the project activity are composed of (a) the emissions of not destroyed N₂O, (b) on-site emissions due to the hydrocarbons (; Natural Gas) use as input to the N₂O destruction facility, and (c) the emissions from the operation of the destruction facility.

Hydrocarbons can be used as reducing agent and/or re-heating the tail gas to enhance the catalytic N₂O reduction efficiency. In this project, natural gas is used for re-heating the tail gas to enhance the catalytic N₂O reduction efficiency

$$PE_{period} = \left(\sum_i^n F_{TE,i} \times CO_{N_2O,i} \times M_i \right) \times GWP_{N_2O} \\ + [(\rho_{HC} \times Q_{HC,y} \times EF_{HC} \times OXID_{HC}/100) + (\rho_{CH_4} \times Q_{CH_4,y} \times EF_{CH_4} \times OXID_{CH_4}/100)] \\ + [\rho_{CH_4} \times Q_{CH_4,y} \times GWP_{CH_4} \times (1-OXID_{CH_4}/100)]$$

- n : Number of intervals during the year (period⁻¹)
- M_i : Length of Measuring Interval (hr), (1hr : set value at instrument for this project)
- $F_{TE,i}$: Volume flow rate at the exit of the DF during interval i (Nm³/hr)
- $CO_{N_2O,i}$: N₂O concentration in the tail gas of the DF exit during interval i (tN₂O/ m³)
- GWP_{CH_4} : Global warming potential of CH₄, 21 (: default value)
- GWP_{N_2O} : Global warming potential of the nitrous oxide, 310 (: default value)
- ρ_{CH_4} : Density of methane (tCH₄/m³), 0.000716
- ρ_{HC} : Density of HC (tHC/m³)
- EF_{CH_4} : CO₂ emission factor of CH₄ (tCO₂e/tCH₄), 2.75
- EF_{HC} : CO₂ emission factor of HC with two or more carbon molecule in natural gas (tCO₂e/tHC)
- $Q_{CH_4,y}$: Methane used in period (Nm³/period)
- $Q_{HC,y}$: HC with two or more carbon molecule in natural gas used in period (Nm³/period)
- $OXID_{CH_4}$: Oxidation factor of methane (%)
- $OXID_{HC}$: Oxidation factor of HC(%), 100% (Fixed value)

Hourly calculated PE (PE_{hr}) are aggregated into the daily PE(PE_{day}), and total PE on the period (PE_{period}) are estimated as sum of PE_{day} . ER calculation sheet for each plant which daily measured and calculated results were integrated into is in detail on the mission reductions calculation spreadsheet

E.3. Leakage calculation

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The installation of the N₂O destruction facility doesn't result in significant additional energy consumption at the caprolactam production plant. In conclusion, no leakage is expected at this project as per the registered PDD.

The emission by leakage is accounted as zero ($LE_y = 0$)

E.4. Emission reductions calculation / table

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The emission reduction ER_{period} by the project activity during a given year y is the difference between the baseline emissions (BE_{period}) and project emissions (PE_{period}), as follows:

$$ER_{period} = BE_{period} - PE_{period} - LE_{period}$$

Therefore ER_{period} can be estimated upon the values of BE_{period} , PE_{period} and LE_{period} those are calculated as mentioned above.

Table E.4 ER in Period#1

	BE_{period}	PE_{period}	LE_{period}	ER_{period}
Plant I	<u>93,882</u> <u>93,881.790</u>	<u>10,182</u> <u>10,223.506</u>	0	<u>83,700</u> <u>83,658.284</u>
Plant II	<u>68,746</u> <u>68,746.477</u>	<u>7,577</u> <u>7,653.747</u>	0	<u>61,169</u> <u>61,092.730</u>
Period Total	<u>162,628</u> <u>162,628.267</u>	<u>17,759</u> <u>17,877.253</u>	0	<u>144,869</u> <u>144,751</u>

Also, these values of ER_{period} in Table E.9 are the same as the integrated values of ER_{day} for each plant during this period. Refer to Table S.1 and Table S.3 in the spread sheets named "1.5 Period1-Plant1-ER(IC)" and "2.5 Period1-Plant2-ER(IC)".

E.5. Comparison of actual emission reductions with estimates in the CDM-PDD

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Below table is to show comparison of actual values of the emission reductions achieved during the monitoring period with the estimations in the registered CDM-PDD.

Table E.5 Comparison of actual emission reductions with estimates in the CDM-PDD

Item	Values applied in ex-ante calculation of the registered CDM-PDD	Actual values reached during the monitoring period
Emission reductions (tCO ₂ e)	660,995	<u>144,869</u> <u>144,751</u>
Days	365	84
Daily average(tCO ₂ e/day)	1,811	<u>1,725</u> <u>1,723</u>

The actual value is lower than the ex-ante calculated value of the registered CDM-PDD.

E.6. Remarks on difference from estimated value in the PDD

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Not applicable

History of the document

Version	Date	Nature of revision
01	EB 54, Annex 34 28 May 2010	Initial adoption.
Decision Class: Regulatory Document Type: Guideline, Form Business Function: Issuance		