

**MONITORING REPORT FORM (CDM-MR) \***  
**Version 01 - in effect as of: 28/09/2010**

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\* as contained within the document entitled "Guidelines for completing the monitoring report form (CDM-MR)" (EB 54 meeting report, annex 34).

## MONITORING REPORT

Version 05; 28/08/2012

**TITLE: “PROJECT FOR THE CATALYTIC REDUCTION OF N<sub>2</sub>O EMISSIONS WITH A SECONDARY CATALYST INSIDE THE AMMONIA REACTOR OF THE NO. 9 NITRIC ACID PLANT AT AFRICAN EXPLOSIVES LTD (“AEL”), SOUTH AFRICA”**

**Reference Number: 1171**

**Monitoring period: No 04, 02/07/2010 – 15/04/2011**

### SECTION A. General description of the project activity

#### A.1. Brief description of the project activity:

##### Purpose of the project activity and measures taken to reduce GHG emissions

The sole purpose of the project activity is to significantly reduce former levels of N<sub>2</sub>O emissions from the production of nitric acid at AEL’s nitric acid plant No. 9 (“AEL-9”) in Modderfontein, South Africa, by implementation of a secondary N<sub>2</sub>O abatement catalyst.

##### Brief description of the installed technology and equipment

The employed secondary N<sub>2</sub>O abatement catalyst technology is supplied by Johnson Matthey PLC. Continuous monitoring of emission reductions is assured by an Automated Measuring System (AMS), consisting of stack gas volume flow meter, N<sub>2</sub>O Analyzer, and respective data logging facilities. The AMS as well as its installation complies with the requirements of the European Standard EN 14181 as required by the methodology.

##### Relevant dates for the project activity

Registration Date: 05/11/2007

Installation of AMS: The N<sub>2</sub>O Analyzer was installed in May 2007. The stack gas flow meter was installed in June 2006

Baseline Campaign: BL – Campaign “H15”<sup>1</sup> 05/09/2007 – 06/11/2007

Installation of secondary catalyst: 09/11/2007

Starting Date of Project Activity: 09/11/2007

Project Campaigns:	1. Campaign	PC1 - 09/11/2007-09/02/2008
	2. Campaign	PC2 - 19/02/2008-12/06/2008
	3. Campaign	PC3 - 08/07/2008-28/07/2008
	4. Campaign	PC4 - 25/02/2009-04/08/2009
	5. Campaign	PC5 – 05/08/2009-01/11/2009
	6. Campaign	PC6 - 30/11/2009-07/03/2010
	7. Campaign	PC7 - 08/04/2010-01/07/2010

Project Campaigns covered by current Monitoring/Verification Period: <sup>2</sup>

8. Campaign	PC8 - 21/09/2010-10/02/2011
9. Campaign	PC9 - 11/02/2011-15/04/2011

##### Total emission reductions achieved in this monitoring period

The total amount of emission reductions achieved in this monitoring period is 41,439 t CO<sub>2</sub>e.

<sup>1</sup> H15 refers to AEL internal designation of the different production campaigns

<sup>2</sup> During this monitoring period one intermediate production campaign without secondary catalyst was performed in the period 02/07/2010 – 21/09/2010. No emission reductions were achieved during this time.

**A.2. Project Participants**

<b>Name of Party involved (host) indicates a Host Party)</b>	<b>Private and/or public entity(ies) project participants (as applicable)</b>	<b>Kindly indicate if the Party involved wishes to be considered as project participant (Yes/No)</b>
South Africa (host)	African Explosives Ltd (“AEL”)	No
United Kingdom of Great Britain and Northern Ireland	N.serve Environmental Services GmbH (“N.serve”)	No
Switzerland	N.serve Environmental Services GmbH, African Explosives Ltd	No

**A.3. Location of the project activity:**

The project activity is located in: Modderfontein (approx. 20 km north-east of Johannesburg). Postal address: PO Modderfontein 1645. Coordinates of the plant are 26°05'26" South and 28°10'17" East.

**A.4. Technical description of the project**

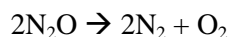
The project activity entails the installation and implementation of the following technical equipment and quality measures:

- 1.) secondary N<sub>2</sub>O abatement technology;
- 2.) Automated Monitoring System (AMS) for continuous N<sub>2</sub>O measurement which is fully in compliance with European Standard EN 14181 (see Section C for more detail); and
- 3.) training of local staff on installation, operation and maintenance of catalyst and monitoring equipment, as well as implementation of quality check and quality assurance measures (see Section C for more detail).

**Catalyst Technology**

AEL has contracted with Johnson Matthey PLC who exclusively markets a secondary catalyst technology that has been developed by YARA International ASA (Norway). AEL installed the YARA 58 Y 1® catalyst system consisting of an additional base metal catalyst that is installed below the standard precious metal gauze pack.

The catalyst has been tried and tested in a number of nitric acid plants in Europe. The abatement efficiency has been shown to be 70 - 90% in the following reaction:



No contamination of the nitric acid with cobalt or any of the other catalyst materials has been observed.

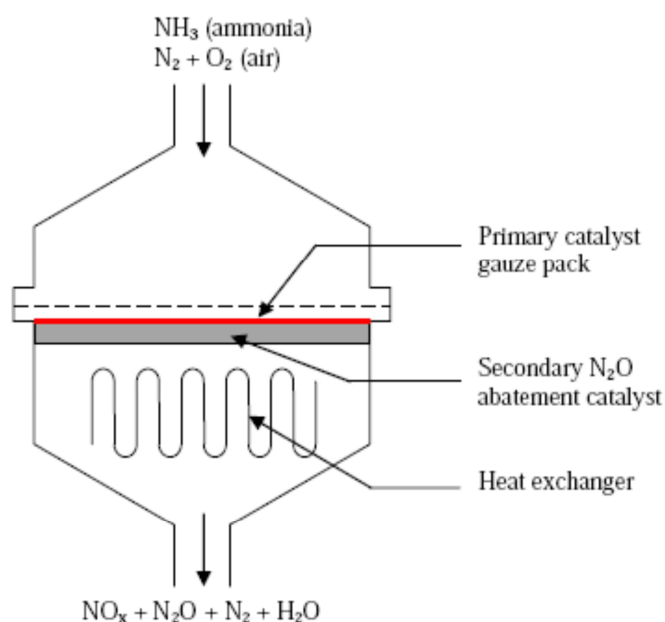
The catalyst does not require additional heat or other energy over and above the temperature that is present inside the Ammonia Oxidation Reactor anyway. There are no additional greenhouse gases or other emissions generated by the reactions on at the N<sub>2</sub>O abatement catalyst.

This technology has been implemented inside the AEL-9 ammonia oxidation reactor.

The precious metal gauze pack – i.e. the primary catalyst required for the actual production of nitric acid – has been supplied to AEL by Heraeus Ltd. for a number of years. The precious metal composition of that gauze pack remains unchanged during the crediting period of the project.

**N<sub>2</sub>O abatement catalyst installation**

The secondary catalyst itself is easily installable during a routine plant shut-down and gauze change. The pellets are poured into the support basket / heat shield arrangement and raked level. The gauze pack is then installed above this bed using the support mechanism provided by the heat shield.



AEL's nitric acid plant No.9 operates at a pressure of around 8.6 -9 bars inside the ammonia oxidation reactor.

**A.5. Title, reference and version of the baseline and monitoring methodology applied to the project activity:**

This project activity is based on Approved Baseline and Monitoring methodologies AM0034 (Version 2): "Catalytic reduction of  $N_2O$  inside the ammonia burner of nitric acid plants". Furthermore, the project draws on approved baseline methodology AM0028 (Version 04.2) for the baseline scenario selection and employs the "Tool for the demonstration and assessment of additionality" (Version 02).

**A.6. Registration date of the project activity:**

Registration Date of project activity: 05/11/2007

**A.7. Crediting period of the project activity and related information (start date and choice of crediting period):**

Crediting period: 10 years; Start date: 05/11/2007-04/11/2017

**A.8. Name of responsible person(s)/entity(ies):**

Contact information of the person(s)/entity(ies) responsible for completing the monitoring report form (CDM-MR).

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## SECTION B. Implementation of the project activity

### B.1. Implementation status of the project activity

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The determination of the permitted operating conditions for operating temperature, operating pressure, maximum ammonia flow rate, maximum ammonia to air ratio, normal gauze supplier and normal gauze composition was undertaken by the validating DOE (as it was clarified by the CDM EB in EB31 meeting that either the validating or verifying DOE could undertake the task of determination of the permitted operating conditions). However, the normal campaign length as well as the determination of the baseline emission factor was in the scope of the verifying DOE. These parameters were determined and verified within the course of the first verification. The baseline campaign was operated from 05/09/2007 until 06/11/2007.

The secondary catalyst was installed on the 09/11/2007, which is the starting date of the project activity. The project was registered by UNFCCC on the 05/11/2007, which is the starting date of the crediting period.

A summary of production campaigns operated in previous monitoring periods as well this monitoring period is given in section A.1. of this monitoring report.

As to the characteristics of this specific project type certain production related events and incidents may affect the performance of the project or influence the monitoring of emission reductions in addition to possible failure of the installed monitoring equipment.

The below table lists all relevant events and incidents related to production and/or emission monitoring which have occurred during actual operation within this specific monitoring period, as well as the measures taken for addressing any resulting problems and issues.

#	Start of the event	End of the event	Campaign		Short description
			AEL designation	Project campaign	
1	02/07/2010 02:00	21/09/2010 01:00	H27	-	Operation of one intermediate campaign without secondary catalyst. Therefore this campaign was excluded from emission reduction calculations and moving average emission factor calculations.
2	21/09/2010 22:00		H28	8	Start of new campaign
3	28/09/2010	30/09/2010	H28	8	Plant tripped on compressor HP vibrations Shutdown
4	17/10/2010	20/10/2010	H28	8	Shutdown
6	30/10/2010	27/01/2011	H28	8	Shutdown
7	27/01/2011		H28	8	Plant trip
8	28/01/2011	29/01/2011	H28	8	Plant trip
9	02/02/2011	10/02/2010	H28	8	Primary gauze torn - leading to higher N <sub>2</sub> O levels
10	10/02/2011		H28	8	Gauze change
11	11/02/2011		H29	9	Start of new campaign
12	15/04/2011		H29	9	Power Failure - Gauze change

***NO events or incidents of any relevance in regard to impacting the applicability of the methodology occurred during this monitoring period.***

*No events or incidents that resulted in AMS downtime occurred during this monitoring period or during the baseline campaign period. Per AM0034 no correction is needed for the plant downtime periods.*

<b>B.2. Revision of the monitoring plan</b>
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The monitoring plan has not been revised.

<b>B.3. Request for deviation applied to this monitoring period</b>
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No deviation was applied to this monitoring period.

<b>B.4. Notification or request of approval of changes</b>
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No notifications or request of approval of changes from the project activity as described in the registered CDM-PDD have been made.

## SECTION C. Description of the monitoring system

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### 1. General Description of the AMS

A complete Automated Monitoring System (AMS) to monitor the mass emissions of  $\text{N}_2\text{O}$  at the stack of AEL's No.9 nitric acid plant was installed and has been operated since 2007. A new stack gas flow meter was installed in June 2006.

### 2. Sample point

The location of the sample point was selected to provide ease of access and a location close to the analyzer. The most suitable position is in tail gas of the plant downstream of all process equipment.

### 3. Sample Conditioning System

The gas sample is continuously taken via a heated probe and filter unit and a heated sample line. Before entering the analyzer the gas is treated by a dryer unit to avoid possible moisture effects.

### 4. Analyzer

The analyzer installed at AEL No. 9 nitric acid plant to continuously monitor  $\text{N}_2\text{O}$  concentration in the stack is an ABB AO2040 Uras 14 NDIR analyzer.

### 5. Flow Meter

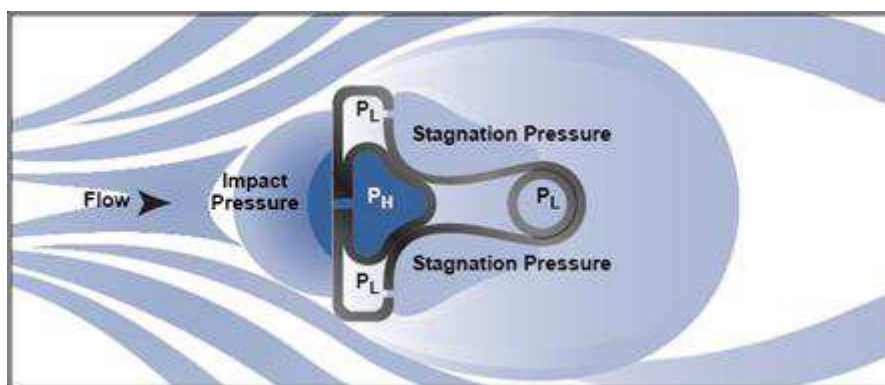
The Emerson Rosemount Flow Meter Annubar®, model no. 485, relies on the Averaging Pitot Tubes (APTs).

The Rosemount Annubar® 485 is a device used to measure the flow-velocity of a liquid, gas or steam fluid that passes through a pipe. It measures by creating a differential pressure (DP) that is proportional to the square of the velocity of the fluid in the pipe, in accordance with Bernoulli's theorem. This DP is measured and converted into a flow rate using a secondary device, such as a DP pressure transmitter.

The Annubar generates a DP by partially blocking the flow. The velocity of the fluid is decreased and stalled as it reaches the upstream surface of the Annubar sensor, thus creating the Impact Pressure. The Rosemount 485 Annubar® senses the impact pressure by utilizing a frontal slot design, which opens into the high pressure chamber.

This high pressure chamber connects directly into the DP transmitter for measurement.

As the fluid continues around the Annubar sensor, it creates a lower velocity profile on the back of the sensor, creating the low/suction pressure downstream. Individual ports, located on the backside of the Annubar sensor measure this low pressure. Working on the same principle as with high pressure, an average low pressure value is obtained in the low pressure chamber that connects directly into the transmitter for measurement. The resulting differential pressure is the difference between the impact (high) pressure reading and the suction (low) pressure reading as seen below.



### 6. Nitric acid production measurement

NAP is continuously measured and determined by a coriolis mass flow meter. The product density and temperature as measured by the mass flow meter are used to calculate the concentration of the nitric acid produced. This value is then used to convert the total mass flow to 100% nitric acid produced. The correct measurement of acid concentration is checked by manual tests.

## **7. Monitoring plan and responsibilities**

The emission reductions achieved by the project activity are monitored based on the approved baseline and monitoring methodology AM0034 (Version 2) “Catalytic reduction of N<sub>2</sub>O inside the ammonia burner of nitric acid plants” as prepared by N.serve Environmental Services GmbH.

AM0034 requires the use of the European Standard EN 14181 (2004) “Stationary source emissions - Quality assurance of automated measuring systems” as a guidance for installing and operating the Automated Monitoring System (AMS) in the nitric acid plants for the monitoring of N<sub>2</sub>O emissions.

As an operator of nitric acid plants since 1932 and of the No. 9 nitric acid plant since 1968, AEL staff in general and its Instrument Department in particular is accustomed to operating technical equipment to a high level of quality standards.

The Production Manager (PM) has the overall responsibility for the ongoing operation of the project.

The Engineering Team Manager Electrical/Instrument (ETM E/I) is responsible for the day-to-day calibration procedure and any adjustments required to the instruments as a result of the calibrations.

The Process Controller (PC) checks the analyzer regularly for any abnormal occurrences. These checks are done using a plausibility checklist, which is filled in and filed, in the control room. If there are any problems the ETM E/I is notified so that the problem can be rectified.

Operation, maintenance, calibration and service intervals are being carried out by staff from the instrumentation department according to the vendor’s specifications.

All monitoring procedures at AEL are also conducted and recorded in accordance with the well established procedures under ISO 9001/14001 which is regularly audited by the South African Bureau of Standards, an independent auditing firm accredited for ISO 9001/14001 certification.

AEL derives hourly averages for all of the monitored parameters and delivers these data to N.serve. Albrecht von Ruffer, Managing Director of N.serve, is responsible for the correct analysis of the delivered data in accordance with the methodology.

## **8. Application of EN 14181 procedures to the project**

In the following, it is described how the procedures given in EN 14181 for QAL1, 2 and 3 have been practically applied at AEL No. 9 plant. QAL 3 procedures are described in section 9 below.

### **QAL1**

In accordance with EN 14181 an AMS shall have been proven suitable for its measuring task (composition of the flue gas) by use of the QAL1 procedure as specified by EN ISO 14956. Using this standard, it shall be proven that the total uncertainty of the results obtained from the AMS meets the specification for uncertainty stated in the applicable regulations. Such suitability testing has to be carried out under specific conditions by an independent third party on a specific testing site. A test institute shall perform all relevant tests on two identical AMS. These two AMS have to be tested in the laboratory and field.

The analyzer installed at AEL No. 9 nitric acid plant to continuously monitor N<sub>2</sub>O concentration in the stack is an ABB AO2040 Uras 14 NDIR analyzer. According to ABB’s own certificate, this analyzer has an accuracy of better than 1% of range. This analyzer has been certified<sup>3</sup> as meeting the requirements (QAL1) of the German emissions standards 17<sup>th</sup> BImSchV and 13<sup>th</sup> BImSchV (waste incineration plants, large furnaces and others) for the components NO, CO and SO<sub>2</sub>. At the time of

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<sup>3</sup> TÜV Süddeutschland Bau und Betrieb GmbH (Report number 170 608), March 2003



commissioning of the AMS by AEL no AMS was available that had been certified according with EN 14181 QAL1 for N<sub>2</sub>O measurements. However, TÜV SÜD conducted and successfully completed the QAL1 tests<sup>4</sup> for the follow-up model of this analyzer module within the same analyzer series (ABB AO2000 Uras 26). Since there are no major technical differences between the two analyzer models it can be assumed that the Analyzer installed at the AEL No. 9 nitric acid plant meets the requirements of the QAL1 test in the same way as the follow-up model.

#### QAL2 and Standard Reference Measurements (SRM)

QAL2 is a procedure for the determination of the calibration function and its variability, and a test of the variability of the measured values of the AMS compared with the uncertainty given by legislation. The QAL2 tests are performed on suitable AMS that have been correctly installed and commissioned on-site (as opposed to QAL 1 which is conducted off-site). QAL2 tests are to be performed at least every 5 years according to EN 14181 but also after major changes to the plant or changes or repairs to the AMS, which will influence the results obtained significantly.

A calibration function is established from the results of a number of parallel measurements performed with a Standard Reference Method (SRM). The variability of the measured values obtained with the AMS is then evaluated against the required uncertainty. According to EN 14181, both the QAL2 procedures and the SRM need to be conducted by an independent “testing house” or laboratory which has to be accredited to EN ISO/IEC 17025.

A series of QAL2 specific reference measurements using the SRM method as per EN 14181 has been carried out at the plant for the above mentioned N<sub>2</sub>O analyzer and stack gas flow meter by an accredited testing house (TÜV SÜD Industrie Service GmbH, Germany) to ensure the AMS’ suitability, establish the calibration curve and test the variability of the measurements. The results of these SRM are available to the DOE as part of the verification process. The AMS calibration function as well as the total uncertainty of the AMS was determined. The results were applied in the calculation of EF<sub>BL</sub> and EF<sub>n</sub>. Moreover the overall uncertainty of the AMS was defined in the QAL2 test and was applied to the calculation of the baseline emission factor in a conservative manner (the baseline emission factor was reduced by the AMS uncertainty).

An annual surveillance test (AST) is used between QAL2 tests to demonstrate that the AMS functions correctly, its performance remains valid and that the calibration function and variability derived during the QAL2 remains as previously determined.

According to the monitoring plan in the PDD it is not necessary to perform an AST by an accredited independent third party. Instead regular QAL3 procedures as periodic zero and span calibrations, checks of the analyzer system and maintenance of the AMS are foreseen in the PDD. However in addition to these calibrations, AEL decided to perform an AST test. At 10/06/2009 – 11/06/2009 and at 06/07/2010 an Annual Surveillance Test (AST) has been successfully performed by an accredited testing house. The test was performed in accordance with EN 14181. The AST test confirmed that the calibration function as determined during QAL2 is still valid and that the requirements for variability are fulfilled.

The AST test was due 10/06/2010 (1 year after last AST). In order to adhere the guidelines for assessing compliance with the calibration frequency requirements as stipulated in EB 52 annex 60 the maximum permissible error of the instruments for NCSG and VSG were applied. The error was applied in a conservative manner for the period between the scheduled AST test and the actual date of the AST test. The error was applied for the period from 10/06/2010 to 01/07/2010 (during the last monitoring period). However, during this monitoring period no corrections were necessary as in the period 02/07/2010 - 21/09/2010 the plant was operated without secondary catalyst and no emission reduction were generated during this period.

## **9. AMS calibration and QA/QC procedures**

AEL is certified according to ISO 9001 and 14001 standards for quality and environmental management respectively. The procedures for monitoring, regular calibrations and QA/QC are fully embedded into the procedures required by ISO 9001/14001 and documented in the applicable ISO handbooks. The South African Bureau of Standards (SABS) is the designated auditor for these standards at AEL.

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<sup>4</sup> TÜV Süd Industrie Service GmbH, München (Report number 821029) June 2006

Therefore, all of the monitoring equipment is subjected to the regular “SABS testing loops” as part of the ISO 9001/14001 procedures.

### QAL3

QAL3 is a procedure which is used to check drift and precision in order to demonstrate that the AMS is in control during its operation so that it continues to function within the required specifications for uncertainty.

This is achieved by conducting periodic zero and span checks on the AMS and then evaluating the results obtained using control charts. Zero and span adjustments or maintenance of the AMS, may be necessary depending on the results of this evaluation.

### Analyzer Zero and Span Calibrations

The N<sub>2</sub>O analyzer is calibrated once per year by external QAL2 or AST test according to EN 14181. In addition according to the QAL 1 reports and manufacturers specifications it is recommended to perform a zero/span calibration once every three weeks for the ABB AO2040 Uras 14 NDIR analyzer, however AEL decided to do it twice per week in order to have a closer control over the instrument. For the zero calibration pure nitrogen is used, for the span calibration a certified calibration gas is used. The results of the calibrations are recorded according to the related CDM procedure.

### Calibration Gas

A certified N<sub>2</sub>O calibration gas (balance being N<sub>2</sub>) with a precision of  $\pm 2\%$  is used in the span calibrations. The calibration gas is certified by an independent laboratory (Modderfontein Laboratory Services).

Modderfontein Laboratory Services (Pty) Ltd. is an independent chemical analysis laboratory which is certified by the South African Bureau of Standards (SABS).

### Flow meter calibration procedures

The flow meter is calibrated once per year by external AST test according to EN 14181. In addition the flow meter is calibrated at least once per year usually every 4 month after each campaign (the plant has to be shut down to conduct calibration) by the Instrument Department of AEL. The pressure transmitter is disconnected from the Annubar and the transmitter is then connected to an absolute pressure simulator that has been approved by the South Africa Bureau of Standards (SABS).

If the deviation exceeds 1% of range, then the pressure transmitter is recalibrated and the previous procedure repeated.

The Annubar itself does not need to be calibrated since it is a physical device which will not have drift. Therefore, it is sufficient to regularly inspect the physical condition of the Annubar. The Annubar is taken out of the stack once per year for physical inspection.

The results of these calibration procedures are then recorded in the Calibration Procedure log sheet.

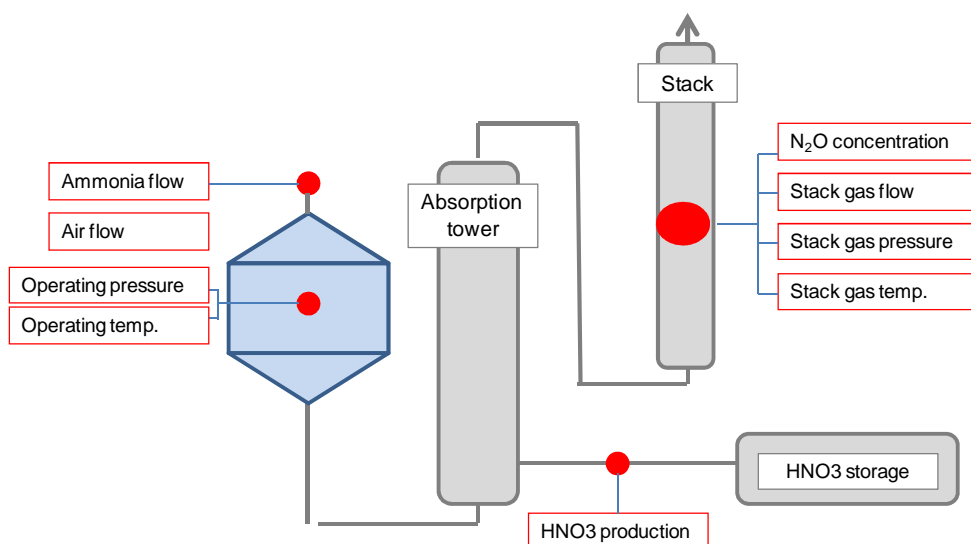


Figure: Monitoring Points for all relevant Parameters (NCSG, VSG, TSG, PSG, NAP, OT<sub>h</sub>, OP<sub>h</sub>, AFR, AIFR)

## Training

Operations staff at the nitric acid plant who are responsible for the operation of the AMS and regular calibrations, visual and physical checks have been trained appropriately by the AMS vendors and AELs' own instrumentation engineers.

### 9.1. Data Acquisition System and Emergency Procedures

The analogue signal (4 to 20 mA) output from the Analyzer and Flow meter are converted by the Programmable Logic Controller (PLC) into a digital signal which is then fed into the SCADA data acquisition and database system.

Each of AEL's two nitric acid plants has its own SCADA system on a dedicated PC near the respective plant itself. However, the two SCADA PCs are directly connected to each other and each of the PCs receives all of the measured data from the AMS and stores them. That way there is a constant redundancy of data acquisition and storage. In addition, the instrumentation engineer transfers the data at least once a week into AEL's main IT system as well as making a complete copy of that weeks data (2-second, hourly and daily averages) onto an external disc drive. That way there are already four copies of the original and unchanged data stored in four different locations. In addition, the hourly data are sent to N.serve on a regular basis (e. g. after each campaign) where they are also stored.

The SCADA system automatically produces comma separated files stored in Microsoft Excel of the 2-second values and it also automatically produces hourly and daily average values for each of the measured parameters. The hourly averages are the basis of the analysis of the data for the purpose of the calculation of the emissions factors for the baseline and for the project campaigns. These are then extracted and converted into excel files which can then be imported into the N.serve Database Management System (N.DBMS).

#### N.serve Database Management System (N.DBMS)

All data necessary for the monitoring and verification procedures related to the project activity are transferred from the nitric acid plant's data acquisition system into N.serve's dedicated relational database management system ("N.DBMS") based on Microsoft Access 2002. Database management systems are designed for a structured storage of large amounts of data providing for minimum redundancy and maximum flexibility to allow best practice data analysis.

The N.DBMS is designed to conduct all the calculation steps required by the methodology in order to derive the baseline and project emissions factors and to calculate the amount of emission reductions resulting from the project activity.

The use of the N.DBMS system is described in the PDD and therefore part of the validated monitoring plan. For the purpose of plausibility checks and for transparency reasons all calculations are also provided in an EXCEL calculation sheet. This EXCEL calculation sheet will be submitted in addition to the N.DBMS documentation sheet along with the request for issuance to allow easy crosschecks and recalculations.

## SECTION D. Data and parameters

### D.1. Data and parameters determined at registration and not monitored during the monitoring period, including default values and factors

<b>Data / Parameter:</b>	<b>B.1 NCSG<sub>BC</sub></b>
Data unit:	<b>mg/Nm<sup>3</sup></b>
Description:	N <sub>2</sub> O concentration in the stack gas during the baseline campaign.
Source of data used:	ABB AO2040 URAS 14 Continuous Emissions Analyzer
Value(s) :	Value applicable for <b>regular project campaigns</b> exceeding CL <sub>normal</sub> or CL <sub>BL</sub> : <b>1,764.44</b>  Value applicable for Project Campaign 8 : <b>1,725.20</b> Value applicable for Project Campaign 9 : <b>1,764.44</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission calculations
Additional comment:	<p>A complete QAL2 audit in accordance with EN 14181 was conducted on the AMS in February 2008. During the QAL2 reference measurements it was determined that the analyzer consistently overestimates the N<sub>2</sub>O concentration in the stack. As a result from the QAL2 calibration curve, it was determined that a correction factor of 0.97 will have to be applied to all NCSG measurements. Therefore, the mean NCSG value will be multiplied by 0.97 before going into the calculation of BE<sub>BC</sub>.</p> <p>Calibration information: During Baseline period 05/09/2007 – 06/11/2007:</p> <p>Bi-weekly Zero and span check and calibration in case of deviation &gt;1% of range of analyzer against zero gas and certified calibration gas cylinder (internal calibration by AEL) Documentation in form of calibration reports and Shewart charts.</p> <p>First check for baseline period: 04/09/2007 During the baseline period: check performed twice per week Last check for baseline period: 05/11/2007 Next check after baseline period: 08/11/2007</p> <p>Date of last external calibration: QAL2 Test – 07/02/2008 - 13/02/2008 valid until 06/02/2013 The calibration error as determined during the QAL2 test was retroactively applied to the NCSG results for the baseline period in a conservative manner. Moreover the overall uncertainty of the AMS was applied in a conservative manner to the results of baseline emissions.</p>

<b>Data / Parameter:</b>	<b>B.2 VSG<sub>BC</sub></b>
Data unit:	<b>Nm<sup>3</sup>/h</b>
Description:	Normal gas volume flow rate of the stack gas during the baseline campaign.
Source of data used:	Gas Volume Flow meter, Emerson Rosemount Annubar® Model 485 combined with pressure transmitter Rosemount 3051S
Value(s) :	<b>42,983</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission calculations.

Additional comment:	<p>The QAL2 test as well as the AST test, performed by an independent 3rd party laboratory with EN ISO/IEC 17025 accreditation, include the test of the correct measurement of stack gas temperature and stack gas pressure by comparison of the AMS results of these parameters with the results of the reference measurement instruments of the testing laboratory. Moreover during the QAL2 and AST tests the correct normalization of the stack gas flow (VSG) to standard conditions is verified by comparison of the AMS results for normalized flow with the reference measurement results for normalized flow.</p> <p>During the QAL2 reference measurements it was determined that the flow meter consistently overestimates the total gas volume flow in the stack. As a result from the QAL2 calibration curve, it was determined that a correction factor of 0.962 will have to be applied to all VSG measurements. Therefore, the result of the above statistical analysis, i.e. the mean VSG value will be multiplied by 0.962 before going into the calculation of <math>BE_{BC}</math>.</p> <p>Calibration information: During Baseline period 05/09/2007 – 06/11/2007:</p> <p>Internal calibrations: after each campaign (usually every 4 month) Date of internal calibration :08/2007*) Date of internal calibration :11/2007*)</p> <p>*) exact dates not available only month and year noted on calibration document</p> <p>Date of last external calibration: QAL2 Test – 07/02/2008 - 13/02/2008 valid until 06/02/2013</p> <p>The calibration error as determined during the QAL2 test was retroactively applied to the NCSG results for the baseline period in a conservative manner. Moreover the overall uncertainty of the AMS was applied in a conservative manner to the results of baseline emissions.</p>
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<b>Data / Parameter:</b>	<b>B.3 <math>BE_{BC}</math></b>
Data unit:	<b>tN<sub>2</sub>O</b>
Description:	Total N <sub>2</sub> O mass flow during baseline campaign
Source of data used:	Calculation from measured data.
Value(s) :	Value applicable for <b>regular project campaigns</b> exceeding $CL_{normal}$ or $CL_{BL}$ : <b>104.315</b>  Value applicable for Project Campaign 8: <b>101.995</b> Value applicable for Project Campaign 9: <b>104.315</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission calculations.
Additional comment:	None

<b>Data / Parameter:</b>	<b>B.4 <math>OH_{BC}</math></b>
Data unit:	<b>hours</b>
Description:	Operating hours

Source of data used:	Production log
Value(s) :	<b>1,474</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission calculations.
Additional comment:	None

<b>Data / Parameter:</b>	<b>B.5 NAP<sub>BC</sub></b>
Data unit:	<b>tHNO<sub>3</sub></b>
Description:	Metric tonnes of 100% concentrated nitric acid produced during the baseline campaign.
Source of data used:	Nitric acid flow meter Manufacturer: EMERSON, Type: Coriolis mass flow meter CMF 200 Laboratory results for verification purposes
Value(s) :	<b>17,718</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission calculations.
Additional comment:	The nitric acid flow meter is subject to external calibration procedures every 3 years. Calibration information During Baseline period 05/09/2007 – 06/11/2007:  External calibration by: ALPRET Controls Specialists Date 04/01/2007 and 11/04/2008; although the calibration is valid for 3 years, it is done more frequently

<b>Data / Parameter:</b>	<b>B.6 TSG</b>
Data unit:	<b>°C</b>
Description:	Temperature in the stack gas
Source of data used:	Stack temperature probe as part of the VSG flow meter.
Value(s) :	<b>Not applicable</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission calculations.
Additional comment:	The TSG result is automatically applied for calculating VSG at standard conditions Calibration information During Baseline period 05/09/2007 – 06/11/2007:  Internal calibrations: after each campaign (usually every 4 month), validity of calibration 1 year Date of internal calibration: 08/2007*) Date of internal calibration: 11/2007*)  *) exact dates not available only month and year noted on calibration document  Date of last external calibration: QAL2 Test – 07/02/2008 - 13/02/2008 valid until 06/02/2013

<b>Data / Parameter:</b>	<b>B.7 PSG</b>
Data unit:	<b>mbar (absolute)</b>
Description:	Pressure in the stack
Source of data used:	Stack pressure as part of the VSG flow meter.
Value(s) :	<b>Not applicable</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission calculations.
Additional comment:	<p>The PSG result is automatically applied for calculating VSG at standard conditions.</p> <p>Calibration information: During Baseline period 05/09/2007 – 06/11/2007:</p> <p>Internal calibrations: after each campaign (usually every 4 month) validity of calibration 1 year Date of internal calibration: 08/2007*) Date of internal calibration: 11/2007*)</p> <p>*) exact dates not available only month and year noted on calibration document</p> <p>Date of last external calibration: QAL2 Test – 07/02/2008 - 13/02/2008 valid until 06/02/2013</p>

<b>Data / Parameter:</b>	<b>B.8 EF<sub>BL</sub></b>
Data unit:	<b>tN<sub>2</sub>O/tHNO<sub>3</sub></b>
Description:	Emissions factor for baseline period
Source of data used:	Calculated from measured data (tonnes of N <sub>2</sub> O emitted / tonnes of nitric acid produced)
Value(s) :	<p>Value applicable for <b>regular project campaigns</b> exceeding CL<sub>normal</sub> or CL<sub>BL</sub>: <b>0.00564</b></p> <p>Value applicable for Project Campaign 8: <b>0.00551</b> Value applicable for Project Campaign 9: <b>0.00564</b></p>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission calculations.
Additional comment:	None

<b>Data / Parameter:</b>	<b>B.9 UNC</b>
Data unit:	<b>%</b>
Description:	Calculated overall uncertainty of the Automated Monitoring System (AMS)
Source of data used:	UNC is determined by conducting reference measurements by an independent testing laboratory with EN ISO/IEC 17025 accreditation (QAL2).
Value(s) :	<b>4.20</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission calculations.



Additional comment:	None
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<b>Data / Parameter:</b>	<b>B.10 AFR</b>
Data unit:	<b>tNH<sub>3</sub>/h</b>
Description:	Ammonia gas flow rate to the ammonia oxidation reactor
Source of data used:	Differential pressure measurement (orifice plate) Type: D/P
Value(s) :	Not applicable, monitored data of AFR will be used to determine if plant was operating outside of AFR <sub>max</sub> .
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission calculations.
Additional comment:	Calibration information During Baseline period 05/09/2007 – 06/11/2007 : Calibration frequency: Once every six months. (only during plant shutdown between campaigns) Date of last calibrations: 04/09/2007, 10/02/2008

Data / Parameter:	B.11 AFR <sub>max</sub>																																			
Data unit:	tNH <sub>3</sub> /h (converted from originally measured Nm <sup>3</sup> /h)																																			
Description:	Maximum Ammonia gas flow rate to the ammonia oxidation reactor																																			
Source of data used:	AFR data																																			
Value(s) :	<p><b>3.877</b></p> <p>Historic data of daily NH<sub>3</sub> consumption was used to obtain determine the range of AFR for the five historic campaigns.</p> <p>Table: Maximum NH<sub>3</sub> gas flow to the AOR</p> <table><tr><th>Campaign No.</th><th>Start Date</th><th>End date</th><th>Total NH<sub>3</sub> consumed</th><th>Maximum NH<sub>3</sub> consumed per day</th></tr><tr><td></td><td></td><td></td><td>tonnes</td><td>tonnes</td></tr><tr><td>H6</td><td>04/06/2004</td><td>16/09/2004</td><td>7,448.377</td><td>93.131</td></tr><tr><td>H7</td><td>24/09/2004</td><td>27/12/2004</td><td>7,372.149</td><td>89.508</td></tr><tr><td>H8</td><td>14/03/2005</td><td>21/06/2005</td><td>7,828.5427</td><td>92.187</td></tr><tr><td>H9</td><td>23/09/2005</td><td>20/12/2005</td><td>6,838.168</td><td>90.425</td></tr><tr><td>H10</td><td>17/02/2006</td><td>20/07/2006</td><td>6,907.924</td><td>91.204</td></tr></table> <p>After removing the top 2.5 percentile values the maximum daily flow rate was 93.037 tons. This corresponds to an hourly flow rate of 3,877kg/h or 5,110 Nm<sup>3</sup>/h. The ammonia flow in Nm<sup>3</sup>/hr is used in the ratio calculation.</p>	Campaign No.	Start Date	End date	Total NH <sub>3</sub> consumed	Maximum NH <sub>3</sub> consumed per day				tonnes	tonnes	H6	04/06/2004	16/09/2004	7,448.377	93.131	H7	24/09/2004	27/12/2004	7,372.149	89.508	H8	14/03/2005	21/06/2005	7,828.5427	92.187	H9	23/09/2005	20/12/2005	6,838.168	90.425	H10	17/02/2006	20/07/2006	6,907.924	91.204
Campaign No.	Start Date	End date	Total NH <sub>3</sub> consumed	Maximum NH <sub>3</sub> consumed per day																																
			tonnes	tonnes																																
H6	04/06/2004	16/09/2004	7,448.377	93.131																																
H7	24/09/2004	27/12/2004	7,372.149	89.508																																
H8	14/03/2005	21/06/2005	7,828.5427	92.187																																
H9	23/09/2005	20/12/2005	6,838.168	90.425																																
H10	17/02/2006	20/07/2006	6,907.924	91.204																																
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission calculations.																																			
Additional comment:	None																																			

<b>Data / Parameter:</b>	<b>B.12 AIFR</b>
Data unit:	<b>% v/v</b>
Description:	Ammonia to air ratio into the ammonia oxidation reactor
Source of data used:	Measurements of AFR and primary air flow rates (measured by differential pressure measurement).
Value(s) :	<b>Not applicable, monitored data of AIFR will be used to determine if plant was operating outside of AIFR<sub>max</sub>.</b>

Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission calculations.
Additional comment:	Calibration information During Baseline period 05/09/2007 – 06/11/2007 : Calibration frequency: Once every six months. (only during plant shutdown between campaigns) Date of last calibrations: 04/09/2007, 10/02/2008

<b>Data / Parameter:</b>	<b>B.13 CL<sub>BL</sub></b>
Data unit:	<b>tHNO<sub>3</sub></b>
Description:	Length of the baseline campaign measured in metric tonnes of 100% concentrated nitric acid produced during that baseline campaign.
Source of data used:	NAP <sub>BC</sub>
Value(s) :	<b>17,718</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission calculations.
Additional comment:	None

Data / Parameter:	B.14 CL <sub>normal</sub>																																
Data unit:	tHNO <sub>3</sub>																																
Description:	Average length of the historic campaigns measured in metric tonnes of 100% concentrated nitric acid produced during the historic campaigns.																																
Source of data used:	Flow meter measurements as described in NAP.																																
Value(s) :	<div>24,026.2</div> <div>During the five historic campaigns, the following amounts of metric tonnes of 100% concentrated nitric acid have been produced:</div> <table><thead><tr><th>Campaign No.</th><th>Start Date</th><th>End date</th><th>Production (tHNO<sub>3</sub>)</th></tr></thead><tbody><tr><td></td><td></td><td></td><td>tonnes</td></tr><tr><td>H6</td><td>04/06/2004</td><td>16/09/2004</td><td>24,443.3</td></tr><tr><td>H7</td><td>24/09/2004</td><td>27/12/2004</td><td>24,041.6</td></tr><tr><td>H8</td><td>14/03/2005</td><td>21/06/2005</td><td>26,945.1</td></tr><tr><td>H9</td><td>23/09/2005</td><td>20/12/2005</td><td>24,326.1</td></tr><tr><td>H10</td><td>17/02/2006</td><td>20/07/2006</td><td>20,374.6</td></tr><tr><td>Mean</td><td></td><td></td><td>24,026.2</td></tr></tbody></table> <div>Therefore, the average historic campaign length (CL<sub>normal</sub>) is 24,026.2 tonnes of 100% concentrated nitric acid.</div>	Campaign No.	Start Date	End date	Production (tHNO <sub>3</sub> )				tonnes	H6	04/06/2004	16/09/2004	24,443.3	H7	24/09/2004	27/12/2004	24,041.6	H8	14/03/2005	21/06/2005	26,945.1	H9	23/09/2005	20/12/2005	24,326.1	H10	17/02/2006	20/07/2006	20,374.6	Mean			24,026.2
Campaign No.	Start Date	End date	Production (tHNO <sub>3</sub> )																														
			tonnes																														
H6	04/06/2004	16/09/2004	24,443.3																														
H7	24/09/2004	27/12/2004	24,041.6																														
H8	14/03/2005	21/06/2005	26,945.1																														
H9	23/09/2005	20/12/2005	24,326.1																														
H10	17/02/2006	20/07/2006	20,374.6																														
Mean			24,026.2																														
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline / Project emission calculations.																																
Additional comment:	None																																

<b>Data / Parameter:</b>	<b>B. 15 AIFR<sub>max</sub></b>
Data unit:	% v/v
Description:	Maximum Ammonia to air ratio into the ammonia oxidation reactor.
Source of data used:	AIFR Data
Value(s) :	<b>11.5</b>  Since no historical data were recorded and available, the allowable NH <sub>3</sub> to Air ratio is taken from the controller data sheet (No 9 Ratio Controller, August 1997). The range is 8.4% v/v - 11.5% v/v, therefore the maximum ammonia to air ratio is 11.5%.
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission calculations.
Additional comment:	None

<b>Data / Parameter:</b>	<b>B.16 OT<sub>h</sub></b>
Data unit:	°C
Description:	Oxidation temperature for each hour during the baseline campaign
Source of data used:	Monitoring results of a thermocouple inside the ammonia oxidation reactor.
Value(s) :	<b>Not applicable</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission calculations.
Additional comment:	Calibration information During Baseline period 05/09/2007 – 06/11/2007: Calibration frequency: Once every campaign (only during plant shutdown between campaigns) Date of last calibrations: 04/09/2007, 10/02/2008

<b>Data / Parameter:</b>	<b>B.17 OT<sub>normal</sub></b>
Data unit:	°C (min and max)
Description:	Normal range operating temperature
Source of data used:	Design specifications and operating manual of the No. 9 nitric acid plant (Technical Manual (TM24 June 1977, p94).
Value(s) :	<b>810 to 915</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission calculations.
Additional comment:	None

<b>Data / Parameter:</b>	<b>B.18 OP<sub>h</sub></b>
Data unit:	kPa (gauge)
Description:	Oxidation Pressure for each hour during the baseline campaign
Source of data used:	Monitoring results of a pressure transmitter on the ammonia oxidation reactor (ammonia to air mixer).
Value(s) :	<b>Not applicable.</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission calculations.
Additional comment:	Calibration information

	<p>During Baseline period 05/09/2007 – 06/11/2007:  Calibration frequency: Once every six month (only during plant shutdown between campaigns)  Date of last calibrations: 04/09/2007, 10/02/2008</p>
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<b>Data / Parameter:</b>	<b>B.19 OP<sub>normal</sub></b>
Data unit:	<b>kPa (gauge) min and max</b>
Description:	Normal range of operating pressure in the ammonia oxidation reactor as determined during the historic campaigns analysis.
Source of data used:	Design specifications and operating manual of the No. 9 nitric acid plant (Technical Manual (TM24 June 1977, p94).
Value(s) :	<b>860 to 910</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission calculations.
Additional comment:	None

<b>Data / Parameter:</b>	<b>B.20 GS<sub>normal</sub></b>
Data unit:	<b>Name of Supplier</b>
Description:	Gauze supplier for the operating condition (i.e. historic) campaigns
Source of data used:	Monitored / Invoices
Value(s) :	<b>W.C. Heraeus</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission calculations.
Additional comment:	None

<b>Data / Parameter:</b>	<b>B.21 GS<sub>BL</sub></b>
Data unit:	<b>Name of Supplier</b>
Description:	Gauze supplier for the baseline condition campaign
Source of data used:	Monitored / Invoices
Value(s) :	<b>W.C. Heraeus</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission calculations.
Additional comment:	None

Data / Parameter:	B.23 GC <sub>normal</sub>			
Data unit:	%			
Description:	Gauze composition during the historic operating campaigns expressed as percentage by weight of the precious metals Platinum, Rhodium and, if applicable, Palladium comprising the Ammonia Oxidation Catalyst gauzes.			
Source of data used:	Monitored / Gauze supplier invoices			
Value(s) :	<b>Platinum (Pt) 59; Rhodium (Rh) 4; Palladium (Pd) 37</b>			
	Record of Gauze compositions installed during the historic campaigns <sup>5</sup> :			
	Campaign	Gauze Supplier	Gauze Composition	
			Pt (%)	Rh (%)

<sup>5</sup> The figures shown here are rounded figures. More exact figures are commercially sensitive information but can be inspected by the DOE during the site visit and can be made available to the CDM EB upon request.

	H6	Heraeus	59	4	37	
	H7	Heraeus	59	4	37	
	H8	Heraeus	59	4	37	
	H9	Heraeus	59	4	37	
	H10	Heraeus	59	4	37	
	Average		59	4	37	
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline emission calculations.					
Additional comment:	None					

<b>Data / Parameter:</b>	<b>B.24 GC<sub>BL</sub></b>
Data unit:	%
Description:	Gauze composition during the baseline campaign expressed as percentage by weight of the precious metals Platinum, Rhodium and, if applicable, Palladium comprising the Ammonia Oxidation Catalyst gauzes.
Source of data used:	Monitored / Gauze supplier invoices
Value(s) :	<b>Platinum (Pt) 59; Rhodium (Rh) 4; Palladium (Pd) 37</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline / Project emission calculations.
Additional comment:	None

<b>Data / Parameter:</b>	<b>B.26 EF<sub>reg</sub></b>
Data unit:	tN <sub>2</sub> O/tHNO <sub>3</sub>
Description:	Emissions cap for N <sub>2</sub> O from nitric acid production set by government regulation
Source of data used:	Department of Environmental Affairs and Tourism
Value(s) :	<b>None</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Baseline / Project emission calculations.
Additional comment:	None.

## D.2. Data and parameters monitored

<b>Data / Parameter:</b>	<b>NCSG</b>
Data unit:	<b>mg/m<sup>3</sup></b> (convertible from ppmv, if required)
Description:	N <sub>2</sub> O concentration in the stack gas during each project campaign.
Measured /Calculated /Default:	Measured/Calculated - every 2 sec. used for calculation of campaign mean (average, after exclusion of extreme values and outliers)
Source of data:	ABB AO2040 URAS 14 Continuous Emissions Analyzernalyzer
Value(s) of monitored parameter:	Value applicable for Project Campaign 8: <b>84.08</b> Value applicable for Project Campaign 9: <b>113.25</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project emission calculations.
Monitoring equipment (type, accuracy class, serial	Type: <i>ABB AO2040 URAS 14 Continuous Emissions Analyzer, non-dispersive infrared analyzer</i>

number, calibration frequency, date of last calibration, validity)	<p>Measurement accuracy (for N<sub>2</sub>O): 2.69 % (per QAL 2 test)</p> <p>Serial Number: 3.346854.7</p> <p>Calibration frequency:</p> <ul style="list-style-type: none"> <li>- External calibration: QAL2 every 5 years;</li> <li>- External calibration: AST every year;</li> <li>- Internal check: twice per week manual check with test gas</li> </ul> <p>Bi-weekly Zero and span check and calibration in case of deviation &gt;1% of range of analyzer against zero gas and certified calibration gas cylinder (internal calibration by AEL) Documentation in form of calibration reports and Shewart charts.</p> <p>First check for monitoring period: 01/07/2010</p> <p>During the monitoring period: check performed twice per week</p> <p>Last check for monitoring period: 14/04/2011</p> <p>Next check after monitoring period: 18/04/2011</p> <p>Date of last external calibration:</p> <p style="margin-left: 40px;"><i>QAL2 Test – 07/02/2008 - 13/02/2008 valid until 06/02/2013</i></p> <p style="margin-left: 40px;"><i>AST – 10/06/2009 - 11/06/2009 valid until 09/06/2010</i></p> <p style="margin-left: 40px;"><i>AST - 06/07/2010 valid until 05/07/2011</i></p>
Measuring/ Reading/ Recording frequency:	Continuously (every 2 seconds)
Calculation method (if applicable):	<p>AM0034 requires the determination of the concentration of N<sub>2</sub>O in the stack gas. NCSG is continuously monitored with an NDIR gas analyzer and monitoring results are taken and recorded for every two seconds of plant operation. Hourly means for NCSG are derived by the data acquisition system. NCSG data taken during times when the plant was out of operation were eliminated. Also readings that were taken during malfunction of the monitoring system were eliminated. The remaining hourly average values were subjected to the following statistical analysis:</p> <ol style="list-style-type: none"> <li>a) Calculate the sample mean (x)</li> <li>b) Calculate the sample standard deviation (s)</li> <li>c) Calculate the 95% confidence interval (equal to 1.96 times the standard deviation)</li> <li>d) Eliminate all data that lie outside the 95% confidence interval</li> <li>e) Calculate the new sample mean from the remaining NCSG values</li> </ol> <p>During the QAL2 reference measurements it was determined that the analyzer consistently overestimates the N<sub>2</sub>O concentration in the stack. As a result from the QAL2 calibration curve, it was determined that a correction factor of 0.97 will have to be applied to all NCSG measurements. Therefore, the result of the above statistical analysis, i.e. the mean NCSG value will be multiplied by 0.97 before going into the calculation of PE<sub>n</sub>.</p>
QA/QC procedures applied:	<p>Bi-weekly Zero and span check and calibration in case of deviation &gt;1% of range of analyzer against zero gas and certified calibration gas cylinder (internal calibration by AEL ) Documentation in form of calibration reports and Shewart charts.</p> <p>First check for monitoring period: 01/07/2010</p> <p>During the monitoring period: check performed twice per week</p>

	<p>Last check for monitoring period: 14/04/2011 Next check after monitoring period: 18/04/2011</p> <p>every 5 years QAL2 test (including AST) according to EN 14181 (External by qualified institute)</p> <p>yearly AST test according to EN 14181 (External by qualified institute)</p> <p>Date of last external calibration:  <i>QAL2 Test – 07/02/2008 - 13/02/2008 valid until 06/02/2013</i>  <i>AST – 10/06/2009 - 11/06/2009 valid until 09/06/2010</i>  <i>AST - 06/07/2010 valid until 05/07/2011</i></p> <p>Calibration delay: The AST was due 10/06/2010 (1 year after the last AST). In order to adhere the guidelines for assessing compliance with the calibration frequency requirements as stipulated in EB 52 annex 60 the maximum permissible error of the instruments for NCSG and VSG were applied. The error was applied in a conservative manner for the period between the scheduled AST and the actual date of the AST. The error was applied for the period from 10/06/2010 to 01/07/2010 (during the last monitoring period). However, during this monitoring period no corrections were necessary as in the period 02/07/2010 - 21/09/2010 the plant was operated without secondary catalyst and no emission reduction were generated during this period.</p>
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<b>Data / Parameter:</b>	<b>VSG</b>
Data unit:	<b>Nm<sup>3</sup>/h</b>
Description:	Normal gas volume flow rate of the stack gas during each project campaign.
Measured /Calculated /Default:	Measured/Calculated - every <b>2</b> sec. used for calculation of campaign mean (average, after exclusion of extreme values and outliers)
Source of data:	Gas Volume Flow meter, Emerson Rosemount Annubar® Model 485 combined with pressure transmitter Rosemount 3051S
Value(s) of monitored parameter:	Value applicable for Project Campaign 8: <b>41,780</b> Value applicable for Project Campaign 9: 42,261
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project emission calculations.
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	<p>Type: Emerson Rosemount Annubar® Model 485 combined with pressure transmitter Rosemount 3051S Overall measurement accuracy: 2.65% (<i>accuracy for the flowmeter per QAL 2 test, before correction of the result to standard conditions by TSG and PSG</i>) combined uncertainty after normalisation by PSG and TSG is 3.22%</p> <p>Serial Number: 0305RT32A11B3 Calibration frequency:  - External calibration: QAL2 every 5 years; External calibration: AST every year;  - Internal calibration: after each campaign (usually every 4 month)</p>

	<p><i>Date of internal calibration: 19/07/2010</i>  <i>Date of internal calibration: 24/11/2010</i>  <i>Date of internal calibration: 10/02/2011</i>  <i>Date of internal calibration: 15/06/2011</i></p> <p>Date of last external calibration:  <i>QAL2 Test – 07/02/2008 - 13/02/2008 valid until 06/02/2013</i>  <i>AST – 10/06/2009 - 11/06/2009 valid until 09/06/2010</i>  <i>AST - 06/07/2010 valid until 05/07/2011</i></p>
Measuring/ Reading/ Recording frequency:	Continuously (every 2 seconds).
Calculation method (if applicable):	<p>AM0034 requires the determination of the gas volume flow (VSG) in the stack. VSG is continuously monitored with a flow meter and monitoring results are taken and recorded for every two seconds of plant operation. Hourly means for VSG are derived by the data acquisition system. Temperature and pressure is also continuously measured in the stack and the VSG values subsequently adjusted to derive the VSG at normal conditions (i.e. standard pressure and temperature).</p> <p>VSG data taken during times when the plant was out of operation were eliminated.</p> <p>The resulting hourly average VSG values are now expressed in Nm<sup>3</sup>/h as required by AM0034 and where subsequently subjected to the following statistical analysis:</p> <ol style="list-style-type: none"> <li>Calculate the sample mean (x)</li> <li>Calculate the sample standard deviation (s)</li> <li>Calculate the 95% confidence interval (equal to 1.96 times the standard deviation)</li> <li>Eliminate all data that lie outside the 95% confidence interval</li> <li>Calculate the new sample mean from the remaining VSG values</li> </ol> <p>During the QAL2 reference measurements it was determined that the flow meter consistently overestimates the total gas volume flow in the stack. As a result from the QAL2 calibration curve, it was determined that a correction factor of 0.962 will have to be applied to all VSG measurements. Therefore, the result of the above statistical analysis, i.e. the mean VSG value will be multiplied by 0.962 before going into the calculation of PE<sub>n</sub>.</p>
QA/QC procedures applied:	<p>Internal calibration at least once per year usually every 4 month after each campaign (the plant has to be shut down to conduct calibration) by the Instrument Department of AEL.</p> <p><i>Date of internal calibration: 19/07/2010</i>  <i>Date of internal calibration: 24/11/2010</i>  <i>Date of internal calibration: 10/02/2011</i>  <i>Date of internal calibration: 15/06/2011</i></p> <p>every 5 years QAL2 test (including AST) according to EN 14181 (External by qualified institute)</p> <p>yearly AST test according to EN 14181 (External by qualified</p>



	<p>institute)</p> <p>Date of last external calibration:  <i>QAL2 Test – 07/02/2008 - 13/02/2008 valid until 06/02/2013</i>  <i>AST – 10/06/2009 - 11/06/2009 valid until 09/06/2010</i>  <i>AST - 06/07/2010 valid until 05/07/2011</i></p> <p>Calibration delay: The AST was due 10/06/2010 (1 year after the last AST). In order to adhere the guidelines for assessing compliance with the calibration frequency requirements as stipulated in EB 52 annex 60 the maximum permissible error of the instruments for NCSG and VSG were applied. The error was applied in a conservative manner for the period between the scheduled AST and the actual date of the AST. The error was applied for the period from 10/06/2010 to 01/07/2010 (during the last monitoring period). However, during this monitoring period no corrections were necessary as in the period 02/07/2010 - 21/09/2010 the plant was operated without secondary catalyst and no emission reduction were generated during this period.</p>
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<b>Data / Parameter:</b>	<b>PE<sub>n</sub></b>
Data unit:	<b>tN<sub>2</sub>O</b>
Description:	Total mass N <sub>2</sub> O emissions in each project campaign.
Measured /Calculated /Default:	Calculated.
Source of data:	Calculated from measured values.
Value(s) of monitored parameter:	Value applicable for Project Campaign 8: <b>3.701</b> Value applicable for Project Campaign 9: <b>6.811</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project emission calculations.
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Not applicable.
Measuring/ Reading/ Recording frequency:	Not applicable.
Calculation method (if applicable):	$PE_n = VSG * NCSG * 10^{-9} * OH$ <p>QAL2 factors have been applied to NCSG and VSG values. These correction factors were determined during the QAL2 test according to EN 14181.</p>
QA/QC procedures applied:	Not applicable.

<b>Data / Parameter:</b>	<b>OH<sub>n</sub></b>
Data unit:	<b>Hours</b>
Description:	Total operating hours during each project campaign
Measured /Calculated /Default:	Measured.
Source of data:	Production log and continuous monitoring.
Value(s) of monitored	Value applicable for Project Campaign 8: <b>1,129</b>

parameter:	Value applicable for Project Campaign 9: <b>1,525</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project emission calculations.
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Not applicable.
Measuring/ Reading/ Recording frequency:	The total operating hours are logged continuously.
Calculation method (if applicable):	Since the design plant operating temperature is between 800 °C and 915 °C, by definition the plant is offline if the temperature recorded is at or below 800 °C. For practical purposes, each hour for which the ammonia oxidation temperature (OT <sub>h</sub> ) was recorded to be below 810 °C is excluded from the determination of OH.
QA/QC procedures applied:	The production logging process is subject to ISO 9001 procedures

<b>Data / Parameter:</b>	<b>NAP</b>
Data unit:	<b>tHNO<sub>3</sub></b>
Description:	Metric tonnes of 100% concentrated nitric acid during each project campaign.
Measured /Calculated /Default:	Measured / Calculated.
Source of data:	Nitric acid flow meter Emerson Coriolis mass flow meter Laboratory results.
Value(s) of monitored parameter:	Value applicable for Project Campaign 8: <b>13,855</b> Value applicable for Project Campaign 9: <b>18,596</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project emission calculations.
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Emerson coriolis mass flow meter CMF 200 Overall measurement accuracy: $\leq 0.1\%$ Serial Number: 12032709 Calibration frequency: every 3 years Date of last calibrations: 24/02/2009 valid until 23/02/2012 24/11/2010 valid until 23/11/2013
Measuring/ Reading/ Recording frequency:	NAP is determined by continuous measurement of the HNO <sub>3</sub> production and concentration
Calculation method (if applicable):	NAP is determined by a mass flow meter according to the following procedures:  The density and temperature as measured by the mass flow meter is used to calculate the concentration of the nitric acid produced. This value is then used to convert the total mass flow to 100% nitric acid produced. The correct measurement of acid concentration is checked by manual tests.
QA/QC procedures applied:	The mass flow meter is calibrated in regular intervals.

<b>Data / Parameter:</b>	<b>TSG</b>
Data unit:	°C
Description:	Temperature in the stack gas
Measured /Calculated /Default:	Measured.
Source of data:	Stack temperature probe situated directly next to the volume flow meter;
Value(s) of monitored parameter:	Not applicable, directly used for normalization of tail gas volume flow measurement.
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project emission calculations.
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	<p>Type: PT 100_385 3-wire RTD - part of the Gas Volume Flow meter  Overall measurement accuracy: 2.55% (<i>per QAL2 test</i>)  Serial Number: <i>not available</i>  Calibration frequency:  - <i>External calibration: QAL2 every 5 years;</i>  - <i>External calibration: AST every year;</i>  - <i>Internal calibration: after each campaign (usually every 4 month) validity 1 year</i></p> <p><i>Date of internal calibration: 19/07/2010</i>  <i>Date of internal calibration: 24/11/2010</i>  <i>Date of internal calibration: 10/02/2011</i>  <i>Date of internal calibration: 15/06/2011</i></p> <p>Date of last external calibration:  <i>QAL2 Test – 07/02/2008 - 13/02/2008 valid until 06/02/2013</i>  <i>AST – 10/06/2009 - 11/06/2009 valid until 09/06/2010</i>  <i>AST - 06/07/2010 valid until 05/07/2011</i></p>
Measuring/ Reading/ Recording frequency:	Continuously (every 2 seconds)
Calculation method (if applicable):	AM0034 requires the determination of gas volume flow at normal conditions in the stack. In order to calculate from the measured VSG values to VSG at normal conditions, the actual temperature in the stack is measured by a temperature probe as part of the flow meter. The resulting measurements are transferred to the data acquisition system and are applied to each VSG value for calculation of normal volume flow.
QA/QC procedures applied:	<p>Internal calibration at least once per year usually every 4 month after each campaign (the plant has to be shut down to conduct calibration) by the Instrument Department of AEL.</p> <p><i>Date of internal calibration: 19/07/2010</i>  <i>Date of internal calibration: 24/11/2010</i>  <i>Date of internal calibration: 10/02/2011</i>  <i>Date of internal calibration: 15/06/2011</i></p> <p>every 5 years QAL2 test (including AST) according to EN 14181 (External by qualified institute)</p>

	<p>yearly AST according to EN 14181 (External by qualified institute)</p> <p>Date of last external calibration:</p> <p style="padding-left: 40px;"><i>QAL2 Test – 07/02/2008 - 13/02/2008 valid until 06/02/2013</i></p> <p style="padding-left: 40px;"><i>AST – 10/06/2009 - 11/06/2009 valid until 09/06/2010</i></p> <p style="padding-left: 40px;"><i>AST - 06/07/2010 valid until 05/07/2011</i></p>
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<b>Data / Parameter:</b>	<b>PSG</b>
Data unit:	<b>Pa (absolute)</b>
Description:	Pressure in the stack
Measured /Calculated /Default:	Measured.
Source of data:	Stack pressure probe situated directly next to the volume flow meter.
Value(s) of monitored parameter:	Not applicable, directly used for normalization of tail gas volume flow measurement.
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project emission calculations.
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	<p>Type: part of the Gas Volume Flow meter, Rosemount 3051TA1A2B21BB4I1M5Q4</p> <p>Overall measurement accuracy: 0.7% (<i>per QAL2 test</i>)</p> <p>Serial Number: 338640.1.1</p> <p>Calibration frequency:</p> <ul style="list-style-type: none"> <li>- <i>External calibration: QAL2 every 5 years;</i></li> <li>- <i>External calibration: AST every year;</i></li> <li>- <i>Internal calibration: after each campaign (usually every 4 month) validity 1 year</i></li> </ul> <p><i>Date of internal calibration: 19/07/2010</i></p> <p><i>Date of internal calibration: 24/11/2010</i></p> <p><i>Date of internal calibration: 10/02/2011</i></p> <p><i>Date of internal calibration: 15/06/2011</i></p> <p>Date of last external calibration:</p> <p style="padding-left: 40px;"><i>QAL2 Test –07/02/2008 - 13/02/2008 valid until 06/02/2013</i></p> <p style="padding-left: 40px;"><i>AST – 10/06/2009 - 11/06/2009 valid until 09/06/2010</i></p> <p style="padding-left: 40px;"><i>AST - 06/07/2010 valid until 05/07/2011</i></p>
Measuring/ Reading/ Recording frequency:	Continuously (every 2 seconds).
Calculation method (if applicable):	AM0034 requires the determination of gas volume flow at normal conditions in the stack. In order to calculate from the measured VSG values to VSG at normal conditions, the actual pressure in the stack has to be determined and transferred to the DURAG system and applied to each VSG value for calculation of normal volume flow.
QA/QC procedures applied:	Internal calibration at least once per year usually every 4 month after each campaign (the plant has to be shut down to conduct calibration)

	<p>by the Instrument Department of AEL.</p> <p><i>Date of internal calibration: 19/07/2010</i>  <i>Date of internal calibration: 24/11/2010</i>  <i>Date of internal calibration: 10/02/2011</i>  <i>Date of internal calibration: 15/06/2011</i></p> <p>every 5 years QAL2 test (including AST) according to EN 14181 (External by qualified institute)</p> <p>yearly AST test according to EN 14181 (External by qualified institute)</p> <p>Date of last external calibration:  <i>QAL2 Test – 07/02/2008 - 13/02/2008 valid until 06/02/2013</i>  <i>AST – 10/06/2009 - 11.06.2009 valid until 09/06/2010</i>  <i>AST - 06/07/2010 valid until 05/07/2011</i></p>
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<b>Data / Parameter:</b>	<b>EF<sub>n</sub></b>
Data unit:	<b>tN<sub>2</sub>O/tHNO<sub>3</sub></b>
Description:	Emissions factor for campaign n.
Measured /Calculated /Default:	Calculated.
Source of data:	Calculation from total mass N <sub>2</sub> O emissions of campaign n (PE <sub>n</sub> ) and total nitric acid production (NAP <sub>n</sub> )
Value(s) of monitored parameter:	Value applicable for Project Campaign 8: <b>0.00027</b> Value applicable for Project Campaign 9: <b>0.00037</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project emission calculations.
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Not applicable.
Measuring/ Reading/ Recording frequency:	Not applicable.
Calculation method (if applicable):	The campaign specific emissions factor for each campaign during the project's crediting period is calculated by dividing the total mass of N <sub>2</sub> O emissions during that campaign by the total production of 100% concentrated nitric acid during that same campaign. For campaign <i>n</i> the campaign specific emission factor is: $EF_n = PE_n / NAP_n$
QA/QC procedures applied:	Not applicable.

<b>Data / Parameter:</b>	<b>EF<sub>ma,n</sub></b>
Data unit:	<b>tN<sub>2</sub>O/tHNO<sub>3</sub></b>
Description:	Moving average emissions factor derived over time from campaign specific emissions factors.
Measured /Calculated /Default:	Calculated.

Source of data:	Calculation from campaign specific emissions factors ( $EF_n$ )
Value(s) of monitored parameter:	Value applicable for Project Campaign 8 : <b>0.00154</b> Value applicable for Project Campaign 9 : <b>0.00141</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project emission calculations.
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Not applicable.
Measuring/ Reading/ Recording frequency:	Not applicable.
Calculation method (if applicable):	In order to take into account possible long-term emissions trends over the duration of the project activity and to take a conservative approach the moving average emission factor is determined as follows:  $EF_{ma,n} = (EF_1 + EF_2 + \dots + EF_n) / n$ <p>This process is repeated for each campaign such that a moving average, <math>EF_{ma,n}</math> is established over time, becoming more representative and precise with each additional campaign.</p>
QA/QC procedures applied:	Not applicable.

<b>Data / Parameter:</b>	<b><math>EF_p</math></b>
Data unit:	<b><math>tN_2O/tHNO_3</math></b>
Description:	Emissions factor used for the specific campaign n to determine the emission reductions of that campaign
Measured /Calculated /Default:	Calculated.
Source of data:	Calculation of $EF_n$ and $EF_{ma,n}$ .
Value(s) of monitored parameter:	Value applicable for Project Campaign 8 : <b>0.00154</b> Value applicable for Project Campaign 9 : <b>0.00141</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project emission calculations.
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Not applicable.
Measuring/ Reading/ Recording frequency:	Not applicable.
Calculation method (if applicable):	To calculate the total emission reductions achieved in a campaign, the higher of the two values $EF_{ma,n}$ and $EF_n$ shall be applied as the emission factor relevant for the particular campaign to be used to calculate emissions reductions ( $EF_p$ ). Thus:  If $EF_{ma,n} > EF_n$ then $EF_p = EF_{ma,n}$ If $EF_{ma,n} < EF_n$ then $EF_p = EF_n$
QA/QC procedures applied:	Not applicable.

<b>Data / Parameter:</b>	<b><math>EF_{min}</math></b>
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Data unit:	<b>tN<sub>2</sub>O/tHNO<sub>3</sub></b>
Description:	EF <sub>min</sub> is equal to the lowest EF <sub>n</sub> observed during the first 10 campaigns of the project crediting period.
Measured /Calculated /Default:	Calculated.
Source of data:	EF <sub>n</sub>
Value(s) of monitored parameter:	<b>Not applicable, will be calculated after 10 project campaigns</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project emission calculations.
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Not applicable.
Measuring/ Reading/ Recording frequency:	Not applicable.
Calculation method (if applicable):	A campaign-specific emissions factor shall be used to cap any potential long-term trend towards decreasing N <sub>2</sub> O emissions that may result from a potential built up of platinum deposits. After the first ten campaigns of the crediting period of the project, the lowest EF <sub>n</sub> observed during those campaigns will be adopted as a minimum (EF <sub>min</sub> ). If any of the later project campaigns results in an EF <sub>n</sub> that is lower than EF <sub>min</sub> , the calculation of the emission reductions for that particular campaign shall use EF <sub>min</sub> and not EF <sub>n</sub> .
QA/QC procedures applied:	Not applicable.

<b>Data / Parameter:</b>	<b>CL<sub>n</sub></b>
Data unit:	<b>tHNO<sub>3</sub></b>
Description:	Length of each project campaign measured in metric tonnes of 100% concentrated nitric acid produced during that campaign.
Measured /Calculated /Default:	Measured.
Source of data:	NAP
Value(s) of monitored parameter:	Value applicable for Project Campaign 8: <b>13,855</b> Value applicable for Project Campaign 9: <b>18,596</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Project emission calculations.
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	See comments for NAP above
Measuring/ Reading/ Recording frequency:	See comments for NAP above
Calculation method (if applicable):	In accordance with AM0034 the project length (CL <sub>n</sub> ) has to be compared to the established average historic campaign length (CL <sub>normal</sub> ); and if the length of each individual project campaign CL <sub>n</sub> is longer than or equal to the average historic campaign length CL <sub>normal</sub> , then all N <sub>2</sub> O values measured during the baseline campaign can be

	used for the calculation of EF (subject to the elimination of data from the operational parameters analysis). If $CL_n < CL_{normal}$ , recalculate $EF_{BL}$ by eliminating those $N_2O$ values that were obtained during the production of tonnes of nitric acid beyond the $CL_n$ (i.e. the last tonnes produced) from the calculation of $EF_n$ .
QA/QC procedures applied:	See comments for NAP above

<b>Data / Parameter:</b>	<b>OP<sub>h</sub></b>
Data unit:	<b>kPa (gauge)</b>
Description:	Oxidation Pressure for each hour
Measured /Calculated /Default:	Measured.
Source of data:	Monitoring results of a pressure transmitter on the ammonia oxidation reactor (ammonia to air mixer).
Value(s) of monitored parameter:	<b>Not applicable. Used to determine when plant is operating outside of permitted range during baseline campaign or if the plant is out of operation.</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Not applicable.
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Type: Yokogawa Press Tx – pressure transmitter Overall measurement accuracy: 1.7 % Serial Number: 12C805780329 Calibration frequency: Once every six months. (only during plant shutdown between campaigns) Date of last calibration: 04/05/2010, 28/08/2010, 04/11/2010, 22/07/2011
Measuring/ Reading/ Recording frequency:	The measurement results are taken by the data acquisition and evaluation system. The system directly calculates hourly averages.
Calculation method (if applicable):	See above
QA/QC procedures applied:	The instrument is subject to yearly internal calibrations. The QA/QC procedures are part of the ISO 9001 procedures.

<b>Data / Parameter:</b>	<b>OT<sub>h</sub></b>
Data unit:	<b>°C</b>
Description:	Oxidation temperature in the ammonia oxidation reactor (AOR) for each hour.
Measured /Calculated /Default:	Measured.
Source of data:	Thermocouples inside the ammonia oxidation reactor
Value(s) of monitored parameter:	<b>Not applicable. Used to determine when plant is operating outside of permitted range during baseline campaign or if the plant is out of operation.</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Not applicable.
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Type: Thermocouple products; K-6 Multipoints Thermocouple Assembly Overall measurement accuracy: 1 % Serial Number: TP3138 Calibration frequency: Once every campaign (only during plant



	shutdown between campaigns) Date of last calibration: 04/05/2010, 28/08/2010, 04/11/2010, 25/07/2011
Measuring/ Reading/ Recording frequency:	The measurement results are taken by the data acquisition and evaluation system. The system directly calculates hourly averages.
Calculation method (if applicable):	See above.
QA/QC procedures applied:	The instrument is subject to yearly internal calibrations, which are part of the ISO 9001 procedures.

<b>Data / Parameter:</b>	<b>AFR</b>
Data unit:	<b>tNH<sub>3</sub>/h</b>
Description:	Ammonia gas flow rate to the ammonia oxidation reactor.
Measured /Calculated /Default:	Measured.
Source of data:	Differential pressure measurement (orifice plate) Type: D/P
Value(s) of monitored parameter:	<b>Not applicable, monitored data of AFR will be used to determine if the plant operating outside of AFR<sub>max</sub> during the baseline campaign or for plausibility checks</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Not applicable.
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Type: Yokogawa Orifice plate with D.P. transmitter Overall measurement accuracy: 1.25 % Serial Number: 91H520733822 Calibration frequency: Once every six months. (only during plant shutdown between campaigns) Date of last calibration: 04/05/2010, 28/08/2010, 04/11/2010, 22/07/2011
Measuring/ Reading/ Recording frequency:	The measurement results are taken by the data acquisition and evaluation system. The system directly calculates hourly averages.
Calculation method (if applicable):	See above
QA/QC procedures applied:	The instrument is subject to yearly internal calibrations, which are part of the ISO 9001 procedures.

<b>Data / Parameter:</b>	<b>AIFR</b>
Data unit:	<b>% v/v</b>
Description:	Ammonia to air ratio into the ammonia oxidation reactor
Measured /Calculated /Default:	Calculated (primary air flow measured as basis for AIFR).
Source of data:	Calculation for each hour of plant operation based on measurements of AFR and primary air flow rates.
Value(s) of monitored parameter:	<b>Not applicable, monitored data of AIFR will be used to determine if the plant operating outside of AIFR<sub>max</sub> during the baseline campaign or for plausibility checks</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Not applicable.
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last	Equipment for Air Flow-rate to AOR: Type: Yokogawa Orifice plate with D.P. transmitter Overall measurement accuracy: 1,66% Serial Number: F570EK384627

calibration, validity)	Calibration frequency: Once every six months. (only during plant shutdown between campaigns) Date of last calibration: 04/05/2010, 28/08/2010, 04/11/2010, 22/07/2011
Measuring/ Reading/ Recording frequency:	The measurement results are taken by the data acquisition and evaluation system. The system directly calculates hourly averages.
Calculation method (if applicable):	The calculation of AIFR is based on the measurement of AFR and primary air flow-rate. The AFR measurement is described in section AFR above. The measurement of primary air flow-rate to AOR is based on differential pressure measurement principle.
QA/QC procedures applied:	Not applicable.

<b>Data / Parameter:</b>	<b>GS<sub>project</sub></b>
Data unit:	<b>Name of Supplier</b>
Description:	Gauze supplier for the project campaign
Measured /Calculated /Default:	Not applicable.
Source of data:	Monitored / Invoices
Value(s) of monitored parameter:	<b>W.C. Heraeus</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Not applicable.
Monitoring equipment (type, accuracy class, serial number, calibration frequency, date of last calibration, validity)	Not applicable.
Measuring/ Reading/ Recording frequency:	Not applicable.
Calculation method (if applicable):	Not applicable.
QA/QC procedures applied:	Not applicable.

<b>Data / Parameter:</b>	<b>GC<sub>project</sub></b>
Data unit:	<b>%</b>
Description:	Gauze composition during the project campaign expressed as % by weight of the precious metals Platinum, Rhodium and, if applicable, Palladium comprising the Ammonia Oxidation Catalyst gauzes.
Measured /Calculated /Default:	Not applicable.
Source of data:	Monitored / Gauze supplier invoices
Value(s) of monitored parameter:	<b>Project campaign 8: Platinum (Pt) 60.1; Rhodium (Rh) 3.9, Palladium (Pd) 36.0</b>  <b>Project campaign 9: Platinum (Pt) 59.9; Rhodium (Rh) 3.9, Palladium (Pd) 36.2</b>
Indicate what the data are used for (Baseline/ Project/ Leakage emission calculations)	Not applicable.
Monitoring equipment (type, accuracy class, serial number, calibration	Not applicable.

frequency, date of last calibration, validity)	
Measuring/ Reading/ Recording frequency:	Not applicable.
Calculation method (if applicable):	Not applicable.
QA/QC procedures applied:	Not applicable.

## SECTION E. Emission reductions calculation

### E.1. Baseline emissions calculation

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N.serve Database Management System (N.DBMS)

All data necessary for the monitoring and verification procedures related to the project activity are transferred from the nitric acid plant's data acquisition system into N.serve's dedicated relational database management system ("N.DBMS") based on Microsoft Access 2002. Database management systems are designed for a structured storage of large amounts of data providing for minimum redundancy and maximum flexibility to allow best practice data analysis.

The N.DBMS is designed to conduct all the calculation steps required by the methodology in order to derive the baseline and project emissions factors and to calculate the amount of emission reductions resulting from the project activity.

The use of the N.DBMS system is described in the PDD and therefore part of the validated monitoring plan. For the purpose of plausibility checks and for transparency reasons all calculations are also provided in an EXCEL calculation sheet. This EXCEL calculation sheet will be submitted in addition to the N.DBMS documentation sheet along with the request for issuance to allow easy crosschecks and recalculations.

#### Analysis of Historical campaign data

The monitoring results for Oxidation Temperature and Pressure have been routinely discarded in the past and are therefore not available to establish the normal range. As a substitute, the technical manuals of the No. 9 nitric acid plant were used to derive these normal ranges. See Annex 1 for details.

Historic data of daily  $\text{NH}_3$  consumption was used to determine the range of AFR for the five historic campaigns (excluding abnormal campaigns). After removing the top 2.5 percentile values the maximum daily flow rate was derived which was then converted into an hourly Ammonia flow rate, which was used to determine AIFR.

The following data was established from the above mentioned sources as permitted operating conditions:

Oxidation temperature (min – max): 810 °C – 915 °C  
Oxidation pressure (min – max): 860,000 Pa – 910,000 Pa or 860 kPa – 910 kPa  
Maximum ammonia flow rate: 3.877 t/h  
Maximum ammonia to air ratio: 0,115 or 11,5%  
 $\text{CL}_{\text{normal}}$ : 24,026.2 t  $\text{HNO}_3$

#### Analysis of Baseline campaign data

As the baseline campaign for AEL No. 9 the campaign AEL No 9 H15 was used. The baseline campaign was in operation in the period 05/09/2007 – 06/11/2007. The baseline monitoring data, baseline calculation and baseline results were determined during the first verification and were verified by the DOE during the first verification.

The results are as follows:

$\text{NCSG}_{\text{BL}}$	mg/Nm <sup>3</sup>	1764.44
QAL2 NCSG		0.97
$\text{VSG}_{\text{BL}}$	Nm <sup>3</sup> /h	42983
QAL2 VSG		0.962

OH <sub>BL</sub>	h	1,474
NAP <sub>BL</sub>	t HNO <sub>3</sub>	17718.00
BE	t N <sub>2</sub> O	104.315
UNC		4.20
<b>EF<sub>BL</sub></b>	<b>kg N<sub>2</sub>O/t HNO<sub>3</sub></b>	<b>5.64</b>

#### **Adjustment of Baseline Emission Factor if $CL_n < CL_{normal}$**

If the length of an individual project campaign  $CL_n$  is longer than or equal to the average historic campaign length  $CL_{normal}$ , then all N<sub>2</sub>O values measured during the baseline campaign can be used for the calculation of EF<sub>BL</sub>. If  $CL_n < CL_{normal}$ , EF<sub>BL</sub> has to be recalculated by eliminating those N<sub>2</sub>O values that were obtained during the production of tonnes of nitric acid beyond the  $CL_n$  (i.e. the last tonnes produced) from the calculation of EF<sub>BL</sub>.

**For the project campaign 9 the  $CL_n$  is longer than  $CL_{BL}$ , therefore no adjustment of the Baseline emissions factor EF<sub>BL</sub> is necessary.**

#### **New calculation of Baseline emissions factor due to $CL_n < CL_{BL}$**

Since for the project campaign 8 (PC8)  $CL_n < CL_{BL}$ , EF<sub>BL</sub> is recalculated by eliminating those N<sub>2</sub>O values that were obtained during the production of tonnes of nitric acid beyond the  $CL_{BL}$  (i.e. the last tonnes produced) from the calculation of EF<sub>BL</sub>.

The results of the baseline recalculation for project campaign 8 (PC8) are as follows:

NCSG <sub>BL</sub>	mg/Nm <sup>3</sup>	1,725.20
QAL2 NCSG		0.97
VSG <sub>BL</sub>	Nm <sup>3</sup> /h	42,983
QAL2 VSG		0.962
OH <sub>BL</sub>	h	1,474
NAP <sub>BL</sub>	t HNO <sub>3</sub>	17,718
BE	t N <sub>2</sub> O	101.995
UNC		4.20
<b>EF<sub>BL</sub></b>	<b>kg N<sub>2</sub>O/t HNO<sub>3</sub></b>	<b>5.51</b>

As a result of this recalculation the new EF<sub>BL</sub> to be applied for project campaign 8 (PC8) is 5.51 kgN<sub>2</sub>O/tHNO<sub>3</sub>

#### **Adjustment of Baseline emissions factor due to EF<sub>reg</sub>**

Should N<sub>2</sub>O emissions regulations that apply to nitric acid plants be introduced in the host country or jurisdiction covering the location of the project activity, such regulations shall be compared to the calculated baseline emission factor for the project (EF<sub>BL</sub>). If the regulatory limit is lower than the baseline factor determined for the project, the regulatory limit shall serve as the new baseline emission factor, that is:

if  $EF_{BL} > EF_{reg}$ ,

then the baseline N<sub>2</sub>O emission factor shall be EF<sub>reg</sub> for all calculations.

where:

#### Variable Definition

$EF_{BL}$  Baseline emissions factor ( $tN_2O/tHNO_3$ )

$EF_{reg}$  Emissions level set by newly introduced policies or regulations ( $tN_2O/tHNO_3$ ).

Such  $EF_{reg}$  shall be determined according to the nature of the regulation (e.g. in terms of absolute emission, by-product rate, concentration in stack gas), as described in the approved methodology AM0028.

**There is currently no  $N_2O$  regulation for nitric acid plants in South Africa therefore no adjustment of the Baseline emissions factor  $EF_{BL}$  is necessary.**

### E.2. Project emissions calculation

>>

Project emissions are calculated according to the following formula:

$$PE_n = VSG * NCSG * 10^{-9} * OH$$

Variable	Definition
VSG	Mean stack gas volume flow rate for the project campaign ( $m^3/h$ )
NCSG	Mean concentration of $N_2O$ in the stack gas for the project campaign ( $mgN_2O/m^3$ )
$PE_n$	Total $N_2O$ emissions of the $n^{th}$ project campaign ( $tN_2O$ )
OH	Is the number of hours of operation in the specific monitoring period (h)

Based on the total  $N_2O$  emissions of each project campaign the specific project campaign emission factor is calculated as:

$$EF_n = PE_n / NAP_n$$

Where:

Variable	Definition
$EF_n$	Project Emission Factor for $n^{th}$ project campaign ( $kgN_2O/tHNO_3$ )
$PE_n$	Total $N_2O$ emissions of the $n^{th}$ project campaign ( $tN_2O$ or $kgN_2O$ )
$NAP_n$	Campaign length of the $n^{th}$ project campaign ( $tHNO_3$ )

Before calculation of the Project Emissions (PE) the same statistical analysis as for the calculation of the baseline emission factor ( $EF_{BL}$ ) is applied to the monitoring raw data (hourly average values) of each project campaign.

The respective correction functions for NCSG and VSG as determined during the relevant QAL2 test are applied within the calculation.

#### Analysis of Project campaign data

##### *Query 1 (Raw data): Analysis of the raw campaign data*

This set of data shows a summary of the collected raw data for the complete project campaign.

N.DBMS Project Campaign Calculation Project: AEL No. 9, Johannesburg, South Africa Campaign: H 28 21.09.10 - 10.02.11									
Project campaign 8 Query 1: Without parameter limits 148									
Parameter	OH	AFR	AIFR	Oph	OTh	NCSG	VSG	NAP	
Unit	h	t NH3 / h	ratio	Pa	°C	mg N2O / Nm3	Nm3 / h	t HNO3	
Count	1,314	1,314	1,314	1,314	1,314	1,314	1,314		
Minimum		0.00	0.00	351.00	800	0.00	1,065		
Maximum		3.49	0.8	907,766.0	901	1,221	43,558		
Mean		2.80	0.11	867,703.1	883	192	36,678		
Standard deviation		1.135	0.06	160,426.08	34	324	12,675		
95% confidence level (1.96 * Std.dev.)		2.22	0.12	314,435.11	66	635	24,842		
Sum	1,314								13,855
Limits acc. to consistency check									
Lower limit									
Upper limit									

According to this Query 1, the NAP value of Project campaign 8 is 13,855 t of nitric acid

N.DBMS Project Campaign Calculation Project: AEL No. 9, Johannesburg, South Africa Campaign: H 29 11.02.11 - 15.04.11									
Project campaign 9 Query 1: Without parameter limits 168									
Parameter	OH	AFR	AIFR	Oph	OTh	NCSG	VSG	NAP	
Unit	h	t NH3 / h	ratio	Pa	°C	mg N2O / Nm3	Nm3 / h	t HNO3	
Count	1,536	1,536	1,536	1,536	1,536	1,536	1,536		
Minimum		0.02	0.00	358.00	801	0.00	2,318		
Maximum		3.34	0.4	914,145.0	902	354	43,036		
Mean		3.16	0.10	889,847.4	900	117	41,991		
Standard deviation		0.273	0.01	73,765.38	9	34	3,063		
95% confidence level (1.96 * Std.dev.)		0.54	0.02	144,580.15	17	67	6,003		
Sum	1,536								18,596
Limits acc. to consistency check									
Lower limit									
Upper limit									

According to this Query 1, the NAP value of Project campaign 9 is 18,596 t of nitric acid

### Query 2: Elimination of faulty data outside operational limits

In this query (Query 2), the operational limits of the plant are applied. Lines of data in which at least one value indicates that the plant is out of operation (trip values) are completely eliminated from further analysis. The design “trip” temperature, i.e. the temperature inside the ammonia oxidation reactor below which the plant shuts down automatically has been applied to exclude such lines of data. During the project, the “trip temperature” of 810 °C will be applied as the exclusion criterion for determining those hours during which the plant was offline during a campaign.

N.DBMS Project Campaign Calculation Project: AEL No. 9, Johannesburg, South Africa Campaign: H 28 21.09.10 - 10.02.11									
Project campaign 8 Query 2: With operational limits 152									
Parameter	OH	AFR	AIFR	Oph	OTh	NCSG	VSG	NAP	
Unit	h	t NH3 / h	ratio	Pa	°C	mg N2O / Nm3	Nm3 / h	t HNO3	
Count	1,129	1,129	1,129	1,129	1,129	1,129	1,129		
Remaining share of data sets	85.9%	85.9%	85.9%	85.9%	85.9%	85.9%	85.9%		
Minimum		0.72	0.06	317,891.00	817	0	12,514		
Maximum		3.49	0.11	907,766.0	901	1,221	43,558		
Mean		3.26	0.10	897,507.4	896	223	41,667		
Standard deviation		0.173	0.004	32,618.710	5.9	340	1,656		
95% confidence level (1.96 * Std.dev.)		0.339	0.008	63,932.671	11.6	666	3,247		
Sum	1,129								13,855
Limits acc. to consistency check									
Lower limit					810				
Upper limit									

As a result of this query the number of operation hours OH of Project campaign 8 is 1,129 h.

N.DBMS Project Campaign Calculation Project: AEL No. 9, Johannesburg, South Africa Campaign: H 29 11.02.11 - 15.04.11									
Project campaign 9 Query 2: With operational limits 172									
Parameter	OH	AFR	AIFR	Oph	OTh	NCSG	VSG	NAP	
Unit	h	t NH3 / h	ratio	Pa	°C	mg N2O / Nm3	Nm3 / h	t HNO3	
Count	1,525	1,525	1,525	1,525	1,525	1,525	1,525		
Remaining share of data sets	99.3%	99.3%	99.3%	99.3%	99.3%	99.3%	99.3%		
Minimum		1.24	0.10	362,460.00	836	53	19,252		
Maximum		3.34	0.10	914,145.0	902	354	43,036		
Mean		3.19	0.10	895,883.6	901	118	42,238		
Standard deviation		0.062	0.001	18,727.250	2.3	33	738		
95% confidence level (1.96 * Std.dev.)		0.122	0.002	36,705.411	4.5	65	1,447		
Sum	1,525								18,596
Limits acc. to consistency check									
Lower limit					810				
Upper limit									

As a result of this query the number of operation hours OH of Project campaign 9 is 1,525 h.

### Query 6: application of confidence interval to eliminate outliers

The 95% confidence interval for NCSG and VSG values is derived and the outliers excluded individually for VSG and NCSG. Hence, the remaining number of data sets may differ between NCSG and VSG.

N.DBMS Project Campaign Calculation Project: AEL No. 9, Johannesburg, South Africa Campaign: H 28 21.09.10 - 10.02.11									
Project campaign 8 Q6: Q2 + confidence levels									
Parameter	OH	AFR	AIFR	Oph	OTh	NCSG	VSG	NAP	
Unit	h	t NH3 / h	ratio	Pa	°C	mg N2O / Nm3	Nm3 / h	t HNO3	
Count						959	1,121		
Remaining share of data sets									
Minimum		0.715	0.06	317,891.00	817	0	38,592		
Maximum		3.49	0.11	907,766.0	901	881	43,558		
Mean		3.26	0.10	897,507.4	896	84.08	41,780		
Standard deviation		0.173	0.004	32,618.710	5.9	90	740		
95% confidence level (1.96 * Std.dev.)		0.339	0.008	63,932.671	11.6	177	1,451		
Sum	1,129								13,855
Limits acc. to consistency check									
Lower limit					810	0.00	38,421		
Upper limit						888.88	44,914		
						0.9700	0.9620		
Campaign emissions	PE						t N2O		3.701
Emission factor	EF_n						kg N2O / t HNO3		0.27

As a result of this query the mean NCSG value for Project campaign 8 is 84.08 mg N2O / Nm3

As a result of this query the mean VSG value for Project campaign 8 is 41,780 Nm3 / h

As a result of this query the result for EFn for Project campaign 8 is 0.27 kg N2O / t HNO3

N.DBMS Project Campaign Calculation Project: AEL No. 9, Johannesburg, South Africa Campaign: H 29 11.02.11 - 15.04.11									
Project campaign 9 Q6: Q2 + confidence levels									
Parameter	OH	AFR	AIFR	Oph	OTh	NCSG	VSG	NAP	
Unit	h	t NH3 / h	ratio	Pa	°C	mg N2O / Nm3	Nm3 / h	t HNO3	
Count						1,453	1,522		
Remaining share of data sets									
Minimum		1.236	0.10	362,460.00	836	53	40,987		
Maximum		3.34	0.10	914,145.0	902	182	43,036		
Mean		3.19	0.10	895,883.6	901	113.25	42,261		
Standard deviation		0.062	0.001	18,727.250	2.3	26	368		
95% confidence level (1.96 * Std.dev.)		0.122	0.002	36,705.411	4.5	52	721		
Sum	1,525								18,596
Limits acc. to consistency check									
Lower limit					810	52.89	40,792		
Upper limit						182.65	43,685		
						0.9700	0.9620		
Campaign emissions	PE						t N2O		6.811
Emission factor	EF_n						kg N2O / t HNO3		0.37

As a result of this query the mean NCSG value for Project campaign 9 is 113.25 mg N2O / Nm3

As a result of this query the mean VSG value for Project campaign 9 is 42,261 Nm3 / h

As a result of this query the result for EFn for Project campaign 9 is 0.37 kg N2O / t HNO3

### Relevant Project Emissions (PE<sub>n</sub>) and respective Project Emission Factors (EF<sub>n</sub>)

The resulting project emissions (PE<sub>n</sub>) and project emission factor (EF<sub>n</sub>) for the project campaigns covered by this monitoring report are:

Campaign	PE	EF <sub>n</sub>
Project Campaign 8 (PC8)	3.701 tN2O	0.27 kgN <sub>2</sub> O/tHNO <sub>3</sub>
Project Campaign 9 (PC9)	6.811 tN2O	0.37 kgN <sub>2</sub> O/tHNO <sub>3</sub>

### Project Campaign Length

If the length of each individual project campaign CL<sub>n</sub> is longer than or equal to the average historic campaign length CL<sub>normal</sub> or to the baseline campaign length whichever is shorter, then all N<sub>2</sub>O values



measured during the baseline campaign can be used for the calculation of EF (subject to the elimination of data from the operational limits analysis, see above under recalculation of Baseline Emission factor).

For the project campaign 9 the  $CL_n$  is longer than  $CL_{BL}$ , therefore no adjustment of the Baseline emissions factor  $EF_{BL}$  is necessary.

Since for the project campaign 8 (PC8)  $CL_n < CL_{BL}$ ,  $EF_{BL}$  is recalculated by eliminating those  $N_2O$  values that were obtained during the production of tonnes of nitric acid beyond the  $CL_{BL}$  (i.e. the last tonnes produced) from the calculation of  $EF_{BL}$ . See section: *New calculation of Baseline emissions factor due to  $CL_n < CL_{BL}$*  above.

### E.3. Leakage calculation

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No leakage occurs under this project type.

### E.4. Emission reductions calculation / table

>>

#### Emission reductions

A *moving average emissions factor* must be calculated at the end of a campaign n as follows:

$$EF_{ma,n} = (EF_1 + EF_2 + \dots + EF_n) / n$$

This process is repeated for each campaign such that a moving average,  $EF_{ma,n}$ , is established over time, becoming more representative and precise with each additional campaign.

To calculate the total emission reductions achieved in a campaign according to the formula below, the higher of the two values  $EF_{ma,n}$  and  $EF_n$  shall be applied as the emission factor relevant for the particular campaign to be used to calculate emissions reductions ( $EF_p$ ). Thus:

If  $EF_{ma,n} > EF_n$  then  $EF_p = EF_{ma,n}$

If  $EF_{ma,n} < EF_n$  then  $EF_p = EF_n$

In addition a campaign-specific *minimum emissions factor* ( $EF_{min}$ ) shall be used to cap any potential long-term trend towards decreasing  $N_2O$  emissions that may result from a potential built up of platinum deposits. After the first ten campaigns of the crediting period of the project, the lowest  $EF_n$  observed during those campaigns will be adopted as a minimum emission factor ( $EF_{min}$ ). If any of the later project campaigns results in a  $EF_n$  that is lower than  $EF_{min}$ , the calculation of the emission reductions for that particular campaign shall use  $EF_{min}$  and not  $EF_n$ . As this project campaign of this current monitoring period is only the 8th project campaign consideration of  $EF_{min}$  is not yet of relevance.

The emission reductions for the project activity during this monitoring period are determined by deducting the campaign-specific emission factor from the baseline emission factor and multiplying the result by the production output of 100% concentrated nitric acid over the campaign period and the GWP of  $N_2O$  according to:

$$ER = (EF_{BL} - EF_p) * NAP * GWP_{N_2O} (tCO_2e)$$

Where:

Variable	Definition
ER	Emission reductions of the project for the specific campaign (tCO <sub>2</sub> e)
NAP	Nitric acid production for the project campaign (tHNO <sub>3</sub> ). The maximum value of NAP shall not exceed the design capacity.
$EF_{BL}$	Baseline emissions factor (kgN <sub>2</sub> O/tHNO <sub>3</sub> )
$EF_p$	Emissions factor used to calculate the emissions from this particular campaign (i.e. the higher of $EF_{ma,n}$ and $EF_n$ ) (kgN <sub>2</sub> O/tHNO <sub>3</sub> )
$GWP_{N_2O}$	Global Warming Potential of N <sub>2</sub> O (310 tCO <sub>2</sub> e/tN <sub>2</sub> O)

The resulting emission reductions (ER) for each of the project campaigns covered by this monitoring report and all relevant monitoring results are summarized in the table below:

		<b>Project campaign 8 (PC8): 21/09/2010 - 10/02/2011</b>	<b>Project campaign 9 (PC9): 11/02/2011 - 15/04/2011</b>
NCSG <sub>BL</sub>	mg/Nm <sup>3</sup>	1,725.20	1,764.44
QAL2 NCSG		0.97	0.97
VSG <sub>BL</sub>	Nm <sup>3</sup> /h	42,983	42,983
QAL2 VSG		0.962	0.962
OH <sub>BL</sub>	h	1,474	1,474
NAP <sub>BL</sub>	t HNO <sub>3</sub>	17,718	17,718
BE	t N <sub>2</sub> O	101.995	104.315
UNC		4.20	4.20
<b>EF<sub>BL</sub></b>	<b>kg N<sub>2</sub>O/t HNO<sub>3</sub></b>	<b>5.51</b>	<b>5.64</b>
NCSG <sub>n</sub>	mg/Nm <sup>3</sup>	84.08	113.25
QAL2 NCSG		0.97	0.97
VSG <sub>n</sub>	Nm <sup>3</sup> /h	41,780	42,261
QAL2 VSG		0.962	0.962
OH <sub>n</sub>	h	1,129	1,525
NAP <sub>n</sub>	t HNO <sub>3</sub>	13,855	18,596
PE <sub>n</sub>	t N <sub>2</sub> O	3.701	6.811
EF <sub>n</sub>	kg N <sub>2</sub> O/t HNO <sub>3</sub>	0.27	0.37
EF <sub>ma,n</sub>	kg N <sub>2</sub> O/t HNO <sub>3</sub>	1.54	1.41
EF <sub>min</sub>	kg N <sub>2</sub> O/t HNO <sub>3</sub>	n/a	n/a
<b>EF<sub>p</sub></b>	<b>kg N<sub>2</sub>O/t HNO<sub>3</sub></b>	<b>1.54</b>	<b>1.41</b>
GWP	tCO <sub>2</sub> e/tN <sub>2</sub> O	310.00	310.00
<b>ER</b>	<b>tCO<sub>2</sub>e</b>	<b>17,062</b>	<b>24,377</b>
<b>Total ER for the monitoring period</b>		<b>41,439</b>	

#### Comparison of design capacity and actually achieved production during this monitoring period

The design capacity of the plant is 292.112 metric tonnes per day, operating 365 days per year. This equals a total production of 84,128 tonnes for a period of 288 days. Therefore the factual production of 32,451 tonnes during the two production campaigns of this monitoring period is below the design capacity of the plant.

#### E.5. Comparison of actual emission reductions with estimates in the CDM-PDD

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This section shall include a comparison of actual values of the emission reductions achieved during the monitoring period with the estimations in the registered CDM-PDD.

<b>Item</b>	<b>Values applied in ex-ante calculation of the registered CDM-PDD</b>	<b>Actual values reached during the monitoring period</b>
<b>Emission reductions (tCO<sub>2</sub>e)</b>	<b>116,779 tonnes CO<sub>2</sub>e per year i. e 92,143 for a period of 288 days</b>	<b>41,439 tonnes CO<sub>2</sub>e during the monitoring period (288 days)</b>

<b>E.6. Remarks on difference from estimated value in the PDD</b>
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The achieved amount of emission reductions during this monitoring period is 41,439 tonnes of CO<sub>2</sub>e and therefore lower than the estimated amount according to the PDD. The reason for this is a considerably lower nitric acid production compared to the estimations in the PDD. Secondly the nitric acid plant was operated without secondary catalyst for one production campaign (02/07/20102 – 21/09/2010). Therefore no emission reductions were achieved during that time. period. Moreover, the baseline emission factors for the project campaigns (0.00551 tN<sub>2</sub>O/tHNO<sub>3</sub> for campaign PC8 and 0.00564 tN<sub>2</sub>O/ tHNO<sub>3</sub> for campaign PC9) were lower than the estimated value that was given in the registered PDD (0.00601 tN<sub>2</sub>O/tHNO<sub>3</sub>).

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**History of the document**

Version	Date	Nature of revision
01	EB 54, Annex 34 28 May 2010	Initial adoption.
<b>Decision Class:</b> Regulatory <b>Document Type:</b> Guideline, Form <b>Business Function:</b> Issuance		