

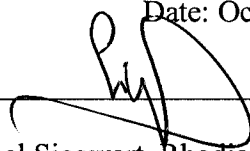


**CDM  
MONITORING REPORT #1  
of  
“N2O Emission Reduction in Onsan,  
Republic of Korea”  
UNFCCC 0099**

**From: Sep. 1, 2006  
To: Oct. 22, 2006**

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## 1 Introduction

The purpose of this monitoring report is to calculate and clarify GHG emission reduction quantity achieved by this project for periodic verification.

This monitoring report covers the activity from September 1<sup>st</sup> 2006 to October 22<sup>nd</sup> 2006 as the 1<sup>st</sup> period.

Duration of the project activity period

The starting date of the project as well as the starting date of the crediting period is defined as 01/09/2006.

## 2. Reference

### **Approved Baseline methodology :**

Baseline Methodology for decomposition of N<sub>2</sub>O from existing adipic acid production plants (AM0021)

### **Approved Monitoring methodology :**

Monitoring Methodology for decomposition of N<sub>2</sub>O from existing adipic acid production plants (AM0021)

### **Project Design Document :**

N<sub>2</sub>O Emission Reduction in Onsan, Republic of Korea.

Version number of the document : 8

Date : September, 1<sup>st</sup> 2005

### **CDM registration number :**

“N<sub>2</sub>O Emission Reduction in Onsan, Republic of Korea” – UNFCCC ref number 0099

## 3. Definition

- y : Monitoring period (in this report, September 1<sup>st</sup> 2006 to October 22<sup>nd</sup> 2006.)
- PDD : Project Design Document of this project “N<sub>2</sub>O Emission Reduction in Onsan, Republic of Korea.” Version number of the document: 8, issued on September, 1<sup>st</sup> 2005



#### 4. General description of project

##### Project activity

Nitrous oxide (N<sub>2</sub>O) is a by-product of adipic acid production. It is of low toxicity but is a greenhouse gas (GHG), whose GWP is large (GWP=310 in the IPCC 2nd Assessment Report). Emissions of N<sub>2</sub>O will be controlled under the Kyoto Protocol. As far as we are aware, there are however no national or regional regulations or restrictions on the emission of N<sub>2</sub>O in South Korea. There are in fact no governmental regulations with quantified emission limits in any non-Annex I countries at this point.

In this project, Rhodia Polyamide Co. Ltd additionally installed N<sub>2</sub>O collection and a thermal decomposition process equipment to the currently operating adipic acid manufacturing plant. This installation reduces the GHG emissions, which would otherwise be released to the atmosphere if the project was not implemented.

The decomposition facilities was installed in the factory site of Onsan Rhodia Polyamide Co., Ltd. in May 2006 and destruction of N<sub>2</sub>O was started in September 2006.

The starting date of the project as well as the starting date of the crediting period is defined as 01/09/2006.

This project activity was registered at UNFCCC on November 27<sup>th</sup> 2005 with the number 0099.

##### Technical description of the project

##### **Location of the project activity**

The decomposition facilities were installed in the factory site of Onsan Rhodia Polyamide Co. Ltd, in May 2006. The surrounding area is the Onsan industrial estate.

##### **Technology to be employed by the project activity**

A thermal oxidizer with 2 chambers is the technology used to decompose N<sub>2</sub>O.

Natural gas is fed with the off gas adipic acid production containing N<sub>2</sub>O and some air in a reduction chamber, where it burns (oxidizes) to carbon dioxide CO<sub>2</sub> and water vapour. N<sub>2</sub>O is used as an oxidizer. Being oxygen deficient, the oxidation is not complete and carbon monoxide and hydrogen are present.

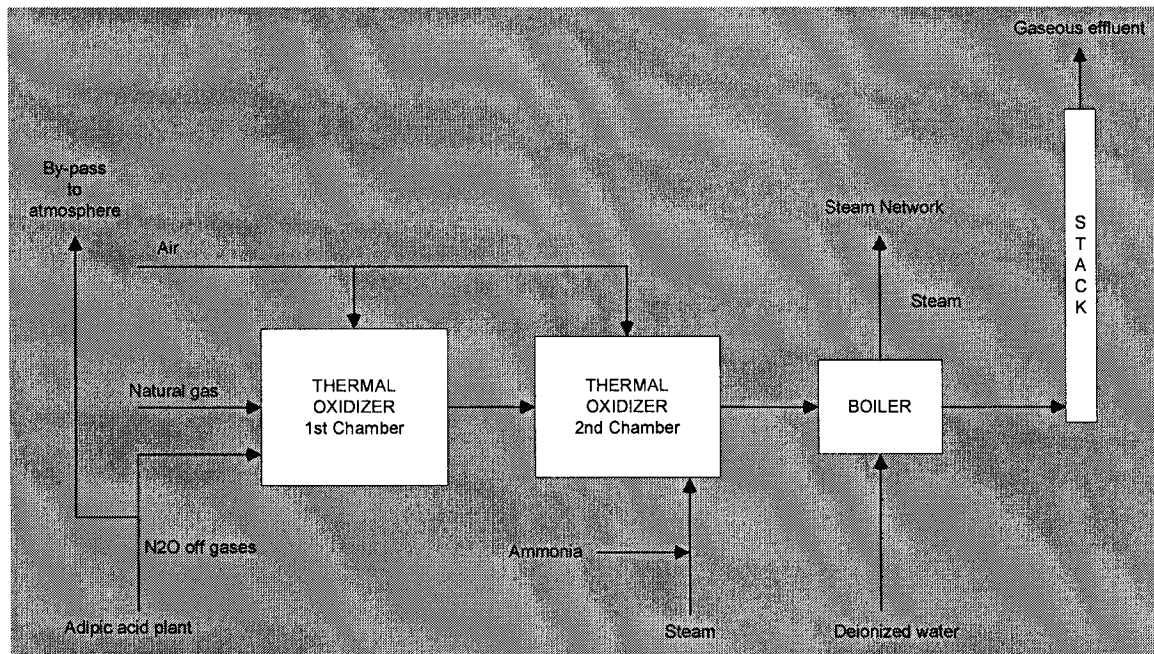


The temperature in the furnace is kept at about 1300°C and under fuel rich conditions, so as to promote the complete decomposition of N<sub>2</sub>O while minimizing the formation of unwanted combustion by-products such as NO and NO<sub>2</sub>.

The gas is then quenched with air to complete the combustion of carbon monoxide and hydrogen at a temperature of about 950°C in a second chamber. Steam and ammonia are injected to control the emission of NO and NO<sub>2</sub>.



Before release to the stack, the flue gas coming from the thermal oxidizer is used to produce saturated steam, which is fed into the existing on-site steam network.



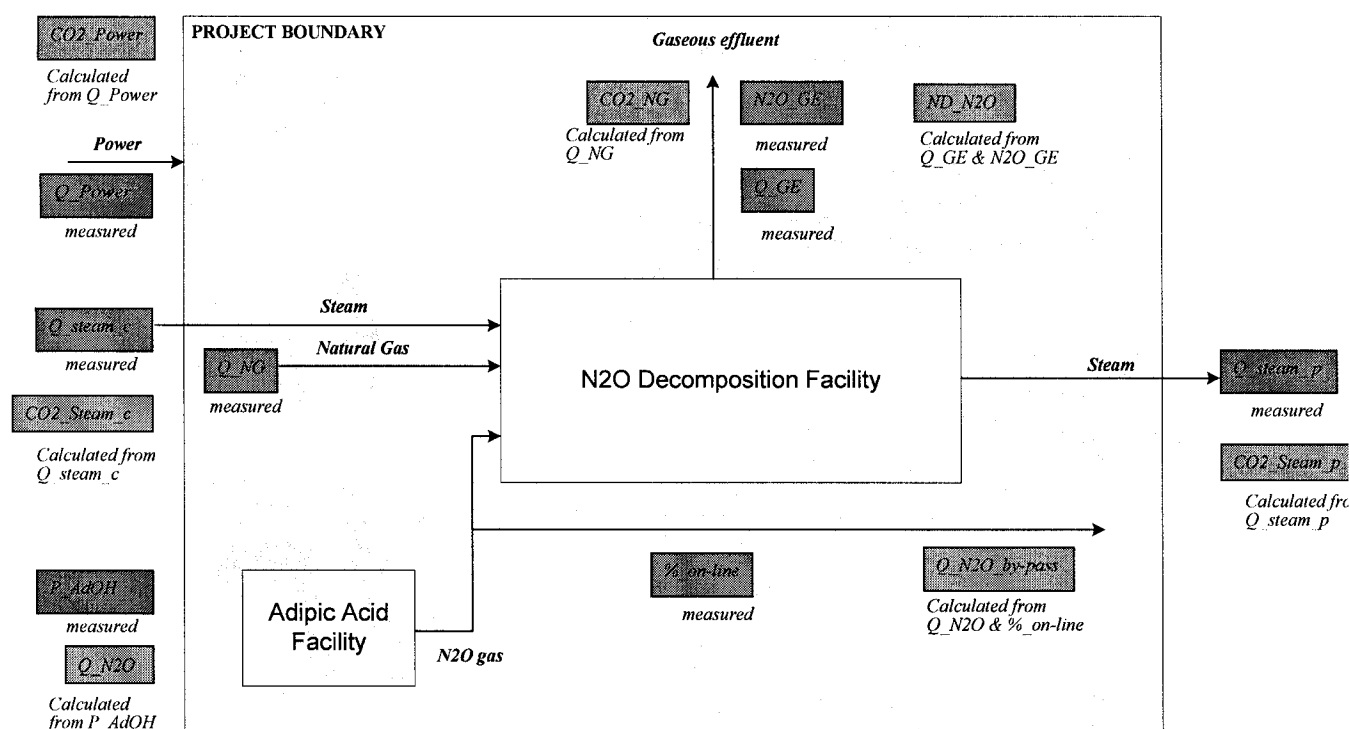


## 5. Baseline methodology

Approved baseline methodology AM 0021: “Baseline methodology for decomposition of N<sub>2</sub>O from existing adipic acid production plants” (AM0021), is applied to this project

The project boundary related to the baseline methodology is shown below and this project boundary is used and explained in the PDD.

Potential sources of anthropogenic emissions by sources of GHG within the project boundary and emissions which are not included in the project boundary are also shown in below.



## 6. Monitoring methodology and plan

Approved monitoring methodology AM 0021 / version 1 is applied to this project

This methodology is applicable to projects which decomposes N<sub>2</sub>O from an adipic acid production plant under the following conditions:

- either catalytic or thermal decomposition of the N<sub>2</sub>O by-product of adipic acid production at existing production plants
- The methodology is spatially generic, being applicable across regions where the data (both related and project activity as well) exist to undertake the assessment
- The methodology is applicable only for installed capacity (measured in tonnes of adipic acid per year) that exists by the end of the year 2004.

The present project satisfies these conditions.



Data being collected to monitor the GHG reduction is given in the table below

ID	Data variable	Source of data	Data unit	Recording frequency	Reference
Q_GE	Volume of effluent gas leaving the stack	Flow meter	Nm <sup>3</sup> /h	Monthly	Appendix 1
N <sub>2</sub> O_GE	Concentration of N <sub>2</sub> O in the effluent gas	Infra –Red online analyzer	ppm	Monthly	Appendix 2
ND_N2O	Quantity of N <sub>2</sub> O in the effluent gas leaving the stack	Calculated from Q_GE and N <sub>2</sub> O_GE	Kg- N <sub>2</sub> O	Monthly	Appendix 3
Q_NG	Amount of natural gas burned	Natural gas meter	Nm <sup>3</sup>	Monthly	Appendix 4
E_NG	Natural gas composition required for calculation of E_NG	Gas supplier	Kg- CO <sub>2</sub> /Nm <sup>3</sup>	Yearly	Appendix 5
%_on-line	% of production time the position switches on the by-pass valves are open	Position switches on bypass valves	% of production time	Monthly	Appendix 6
Q_N2O_by-pass	N <sub>2</sub> O by passing the decomposition facility	Calculated from Q_N2O and %_on-line	kg	Monthly	Appendix 7
P_AdOH	Amount of adipic acid production	Log sheet for packaged product and DCS for silo inventory	t	Monthly	Appendix 8
Nitric acid consumption (HNO <sub>3</sub> _consumption) & physical losses in the adipic acid production process (HNO <sub>3</sub> _physical)	All data required for calculation of HNO <sub>3</sub> chemical	Excel workbook based on the raw material consumption, DCS data and Lab data	-	Monthly	Appendix 9
Q N <sub>2</sub> O reg	Per Korean regulation allowed N <sub>2</sub> O emissions	Korean regulation	kg	Date when relevant legislation is in place	Appendix 10

ID	Data variable	Source of data	Data unit	Recording frequency	Reference
N <sub>2</sub> O reg/AdOH	Per Korean regulation allowed N <sub>2</sub> O emissions per kg of adipic acid produced	Korean regulation	kg	Date when relevant legislation is in place	Appendix 10
r <sub>y</sub>	Per Korean regulation required share of N <sub>2</sub> O emissions to be destroyed	Korean regulation	%	Date when relevant legislation is in place	Appendix 10
P N <sub>2</sub> O	Market price of N <sub>2</sub> O	Estimated	€/t	Yearly	Appendix 11
Q_Steam_p	Amount of steam produced by the decomposition process	Steam meter	kg	Monthly	Appendix 12
Steam supplier data	All data required for calculation of E_Steam	External steam supplier and steam properties	-	Yearly	Appendix 13
Q_Power	Electric consumption of the decomposition facility	Electricity meter	kWh	Monthly	Appendix 14
Electricity grid data	All data required for calculation of E_Power according to AM0002	Korean Energy Economics Institute	-	Yearly	Appendix 15
Q_Steam_c	Amount of steam consumed by the decomposition facility	Steam meter	kg	Monthly	Appendix 16
Steam suppliers data	All data required for calculation of E_Steam_c	Internal & External steam suppliers	-	Yearly	Appendix 17

## 7. Quality Control (QC) and Quality Assurance (QA)

### 7.1. Quality Management System

The thermal oxidation plant is operated by Rhodia operating personnel. Rhodia has assigned the responsibility for operating, monitoring and reporting to the Adipic Acid Plant Manager.

The operation, data transfer and reporting procedures are incorporated into the ISO 9001 procedures of the Onsan Adipic Acid plant

The personnel have been trained by the technology supplier i.e. M/s John Zink International Luxembourg.





## 7.2. Quality control (QC) and quality assurance (QA) procedures that are being undertaken for data monitored

The Onsan plant is certified according to ISO9001 and applies appropriate QA & QC procedures.

The equipment and analytical methods given by the technology supplier M/s John Zink International Luxembourg as well as those supplied by Rhodia are done according to internationally accepted standards.

The QA & QC procedures are set and implemented in order to:

1. Secure a good consistency through planning to implementation of this CDM project and,
2. Stipulate who has responsibility for what and,
3. Avoid any misunderstanding between people and organization involved.

Data (Indicate table and ID number e.g. 3.-1.; 3.2.)	Uncertainty level of data (High/Medium/ Low)	Explain QA/QC procedures planned for these data, or why such procedures are not necessary.
2a.1. (D.2.1.1) Q_GE	Low	<i>This flow meter is measured with an Averaging Pitot tube. This instrument is considered as a critical instrument in the QA/QC procedure.</i>
2a.2. (D.2.1.1) N <sub>2</sub> O_GE	Low	<i>Existing procedures are applied to this analyzer for QA &amp; QC.</i>
2a.4. (D.2.1.1) Q_NG	Low	<i>Is measured using natural gas meter from the supplier and as such is part of a regular procedure control between the Natural Gas supplier and Rhodia.</i>
2b.1. (D.2.1.3) P_AdOH	Low	<i>Is obtained from production records of the ONSAN adipic acid plant where the N<sub>2</sub>O waste originates. A QA/QC procedure is implemented. Production quantity is based on the packaged product plus silo volume.</i>
2a.5. (D.2.1.1) %_on-line	Low	<i>Use opening of high integrity performance connecting valves to limit leaks. Procedures currently in place in Chalampé for monitoring N<sub>2</sub>O emissions have been implemented in ONSAN to periodically check their tightness and assure their good operation. They have been added to the QA/QC existing procedures.</i>
2b.7. (D.2.1.3) Q_Steam_p	Low	<i>Steam meter placed on the list of critical instrument data in the QA/QC procedures</i>
3.1. (D.2.3.1) Q_Power	Low	<i>Electricity meter. Standard procedures are used. No QA/QC procedures implemented as this flow represents less than 0.01% of the baseline emissions.</i>
3.4. (D.2.3.1) Q_Steam_c	Low	<i>Steam meter placed on the list of critical instrument data in the QA/QC procedures.</i>

## 7.3. Calibration/Maintenance of Measuring and Analytical Instruments

All measuring and analytical instruments are being calibrated as per the methodology AM0021 and created as a protocol in Onsan's Quality management system procedures.

The maintenance methods and procedures have been incorporated as part of the ISO 9001 procedures and form an integral part of the systems and procedures for the organization.



#### 7.4. Environmental Impact

The Thermal oxidation plant has been installed with on line analyzers to monitor constantly some parameters that are required by Korean legislation. Starting on July 1<sup>st</sup> 2007, those parameters will be transmitted automatically to the local government environmental agency as part of the Telemonitoring System (TMS) required by a revised environmental law. Until that date regular checking by government agencies can be made.

A National Institute of Environment Research (NIER) representative came on September 28<sup>th</sup> to carry out an analysis of the gaseous releases discharged from the N<sub>2</sub>O stack. As evident from this independent data that confirm actual on-line analyzers data, the plant operation has been within compliance of the environmental standards.

Table showing analysis Gaseous Emission for Thermal Oxidation plant

Parameter		Value as per applicable standard	Typical on-line analysis	Actual analysis on September 28 <sup>th</sup> 2006
CO	ppm	50 max	< 10ppm	4.1 ppm
NOx	ppm	200 max	< 100 ppm	37.3 ppm
NH <sub>3</sub>	ppm	50 max	< 10 ppm	

#### 8. GHG Calculations

Statement of GHG emission reduction in 1<sup>st</sup> monitoring period.

As suggested by the methodology (AM0021/Version 1), the GHG emission reduction, (ER<sub>y</sub>), achieved by the project activity for a given year is  
$$ER_y = BE_y - PE_y - L_y$$

##### 8.1. Calculation of Q<sub>N2Oy</sub>

It has been checked that there are no Korean regulation into place that would limit the quantity of N<sub>2</sub>O emitted that can be taken into account for the calculation of the baseline emissions (see D.2.1.4. in the PDD).

The quantity Q<sub>N2Oy</sub> of N<sub>2</sub>O emitted over the period can then be calculated by:

$$Q_{N2Oy} = P_{AdOH} \times N2O_{AdOH}$$

Over the period of reference the emission factor from the adipic acid plant was above the capped value of 0.27 kg N<sub>2</sub>O/kg AdOH. So the capped value is being used according to AM 0021.

Parameter	value	Reference
Q <sub>N2Oy</sub>	5349510 kg	Calculated
P <sub>AdOH</sub>	19813 t	Appendix 8

%_on-line <sub>y</sub>	75.66 %	Appendix 6
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#### 8.4. Calculation of project emissions

The emissions due to the decomposition process PE<sub>y</sub> are the emissions due to the N<sub>2</sub>O that has not been sent to the decomposition process, the N<sub>2</sub>O non destroyed by the decomposition process and the emissions due to the use of natural gas.

$$PE_y = ((Q_{N_2O} \times (1 - \%_{on-line}))_y + (Q_{GE} \times N_{2O\_GE})_y) \times GWP_{N_2O} + Q_{NGy} \times E_{NGy}$$

The non destroyed N<sub>2</sub>O (ND<sub>N<sub>2</sub>O</sub>) is constantly monitored and obtained from the constant monitoring of the flow (Q<sub>GE</sub>) and the concentration of N<sub>2</sub>O (N<sub>2</sub>O<sub>GE</sub>) of the effluent gas:

$$ND_{N_2O} = Q_{GE} \times N_{2O\_GE}$$

$$PE_y = ((Q_{N_2O} \times (1 - \%_{on-line}))_y + ND_{N_2Oy}) \times GWP_{N_2O} + Q_{NGy} \times E_{NGy}$$

Parameter	value	Reference
<b>PE<sub>y</sub></b>	<b>406 916 t CO<sub>2</sub> eq.</b>	Calculated
(Q <sub>N<sub>2</sub>O</sub> × (1 - % <sub>on-line</sub> )) <sub>y</sub>	1 301 898 kg	Appendix 6
Q <sub>GE</sub>	16 620 313 Nm <sup>3</sup>	Appendix 1
N <sub>2</sub> O <sub>GE</sub>	9.47 ppm	Appendix 2
ND <sub>N<sub>2</sub>O</sub> y	309.09 kg N <sub>2</sub> O	Appendix 3
GWP <sub>N<sub>2</sub>O</sub>	310 kg CO <sub>2</sub> eq./ kg N <sub>2</sub> O	Kyoto Protocol Rule. Decision 2/CP.3
Q <sub>NGy</sub>	1 442 549 Nm <sup>3</sup>	Appendix 4
E <sub>NGy</sub>	2.240 kg CO <sub>2</sub> eq./ Nm <sup>3</sup>	Appendix 5

#### 8.5. Calculation of leakage

Leak emissions comprise the emissions associated with the energy sources used to generate any steam and electricity used by the decomposition plant.

Leakage amounts to:

$$L_y = Q_{Power} \times E_{Power} + Q_{steam\_cy} \times E_{steam\_cy}$$

Parameter	value	Reference
<b>L<sub>y</sub></b>	<b>170.8 t CO<sub>2</sub> eq.</b>	Calculated
Q <sub>Power</sub>	233 395 kWh	Appendix 14
E <sub>Power</sub>	0.649 kg-CO <sub>2</sub> /kWh	Appendix 15
Q <sub>Steam<sub>cy</sub></sub>	140 723 kg	Appendix 16
E <sub>Steam<sub>cy</sub></sub>	0.137 kg-CO <sub>2</sub> / kg of steam	Appendix 17

N <sub>2</sub> O /AdOH	0.27 kg N <sub>2</sub> O/kg AdOH	Appendix 9
Q N <sub>2</sub> O reg	No limit	Appendix 10
N <sub>2</sub> O reg / AdOH	No limit	Appendix 10
r <sub>y</sub>	NA	Appendix 10

The production of adipic acid during the year starting on October 23<sup>rd</sup> 2005 that includes this period is below the nameplate capacity of the adipic acid plant, and as such the total production of this period can be used as such.

### 8.2. Calculation of baseline emissions

The amount of baseline emissions in the given period y (measured in t CO<sub>2</sub> eq.) is calculated by

$$BE_y = Q_{N_2O_y} \times GWP_{N_2O} + Q_{Steam_{py}} \times E_{Steam_y}$$

Parameter	value	Reference
<b>BE<sub>y</sub></b>	<b>1 661 370 t CO<sub>2</sub> eq.</b>	Calculated
Q N <sub>2</sub> O <sub>y</sub>	5349510 kg	Calculated in 8.1
GWP <sub>N<sub>2</sub>O</sub>	310	Kyoto Protocol Rule. Decision 2/CP.3
Q <sub>Steam<sub>py</sub></sub>	24 768 597 kg of steam	Appendix 12
E <sub>Steam<sub>y</sub></sub>	0.122 kg-CO <sub>2</sub> /kg of steam	Appendix 13

### 8.3. Calculation of (Q<sub>N<sub>2</sub>O</sub> x (1-%<sub>on-line</sub>))<sub>y</sub>

The quantity of N<sub>2</sub>O that has by-passed the decomposition facility is calculated from the adipic acid production made while by-passing the decomposition facility.

The quantity of adipic acid produced while by-passing the destruction facility is monitored and the quantity of N<sub>2</sub>O that by-pass the decomposition facility is registered daily:

$$Q_{N_2O\_by-pass} = P_{AdOH} \times (1 - \%_{on-line}) \times N_2O_{/AdOH}$$

This value is a value by excess as during each connection/ disconnection phases the production is counted as completely by-passed.

The quantity of N<sub>2</sub>O that by-passed the decomposition facility over the period is:

$$(Q_{N_2O} \times (1 - \%_{on-line}))_y = Q_{N_2O\_by-pass_y}$$

The %<sub>on-line</sub> equivalent over the period is calculated as :

$$\%_{on-line_y} = 1 - (Q_{N_2O\_by-pass_y} / Q_{N_2O})$$

Parameter	Value	Reference
(Q <sub>N<sub>2</sub>O</sub> x (1-% <sub>on-line</sub> )) <sub>y</sub>	1 301 898 kg	Appendix 7
P <sub>AdOH</sub>	19813 t	Appendix 8
N <sub>2</sub> O /AdOH	0.27 kg N <sub>2</sub> O/kg AdOH	Appendix 9



#### 8.6. Calculation of emission reduction

The total emission reduction achieved by this project activity during the first monitoring period is therefore,

$$ER_y = BE_y - PE_y - L_y$$

Or,

$$ER_y = 1\,661\,370 \text{ t CO}_2 \text{ eq.} - 406\,916 \text{ t CO}_2 \text{ eq.} - 170.8 \text{ t CO}_2 \text{ eq.}$$

Or,

$$ER_y = 1,254,283 \text{ t CO}_2 \text{ eq.}$$

The above emission reduction covers the generation of N<sub>2</sub>O during the period from September 1<sup>st</sup> 2006 to October 22<sup>nd</sup> 2006.



## Appendix 1

Name of item                      Q\_GE  
Description                      Volume of effluent gas leaving the stack

Value in period

16 620 313 Nm<sup>3</sup>

Method of monitoring              Annubar flow meter  
Recording frequency              Monthly  
Background data                      Log sheet record / flowmeter

Period	Quantity of gaseous effluent Nm <sup>3</sup>
Sept 1 <sup>st</sup> – Oct 22 <sup>nd</sup>	16 620 313



## Appendix 2

Name of item

N2O\_GE

Description

Concentration of N<sub>2</sub>O in the effluent gas

Value in period

9.47 ppm

Method of monitoring

Infra-Red online analyzer

Recording frequency

Monthly

Background data

Log sheet record

Calculation method

The on-line analyzer values are used to calculate every 10 sec the quantity of ND\_N2O. Cumulated value is recorded (see appendix 3). Weighted average over the period based upon continuous online measures of the flow Q\_GE and the concentration of N2O is calculated.

The analyzer has a range of 0-200 ppm with a detection limit of 5 ppm, which is used as a default value when the measured value is below the detection limit.

Period	ND_N2O	Quantity of gaseous effluent	Weighted average concentration of N <sub>2</sub> O_GE
	kg	Nm <sup>3</sup>	ppm
Sept 1 <sup>st</sup> – Oct 22 <sup>nd</sup>	309.09	16 620 313	9.47



### Appendix 3

Name of item ND\_N2O

Description

Value in period

309.09 kg N <sub>2</sub> O
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Method of monitoring

On line DCS calculation

Recording frequency

Monthly

Background data

Log sheet record

Calculation method

Actual quantity of non destroyed N2O is calculated on-line in the DCS from the concentration of N2O and the flow rate of the gaseous effluent:

$$ND\_N2O = Q\_GE * N2O\_GE * Specific\_gravity\_of\_N2O$$

Period	ND_N2O kg
Sept 1 <sup>st</sup> – Oct 22 <sup>nd</sup>	309.09





#### Appendix 4

Name of item                      Q\_NG  
Description                      Amount of natural gas used by the decomposition  
   process

Value in period

1 442 549 Nm3
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Method of monitoring

Natural gas consumption data

Recording frequency

Monthly

Background data

Log sheet record / flowmeter

Period	Q_NG Nm <sup>3</sup>
Sept 1 <sup>st</sup> – Oct 22 <sup>nd</sup>	1 442 549



## Appendix 5

Name of item	E_NG
Description	CO2 emission factor for natural gas burning
Value in period	2.240 kg CO <sub>2</sub> /Nm <sup>3</sup>
Method of monitoring	Composition of natural gas
Recording frequency	Monthly
Background data	Composition data received from Kyung Dong City Gas Ltd, the natural gas supplier
Calculation method	The average number of C in a mole of NG is calculated from the composition = $\sum$ (number of C in each mole) x (volume ratio) The CO2 specific gravity in standard state is 1.965 $E\_NG = 1.965 \times$ (average number of C in a mole of NG)

Period	E_NG
Sept 1 <sup>st</sup> – Oct 22 <sup>nd</sup>	2.240



## Appendix 6

Name of item

%\_on-line

Description

% of production time that the N2O is sent to the decomposition facility

Value in period

75.66 %

Method of monitoring

Position of limit switches on the valves allowing to by-pass the decomposition facility

Recording frequency

Monthly

Background data

Log sheet record

Calculation method

Based upon the position of the limit switches on the valves by-passing the decomposition facility, the % of time that the production is connected to the facility is continuously counted and used to calculate Q\_ N2O\_by-pass (See Appendix 7).

At the end of the period, %\_on-line for the period is calculated as:

$$\%_{\text{on-line}_y} = 1 - (Q_{\text{N2O\_by-pass}_y} / (P_{\text{AdOH}_y} \times \text{N2O\_}/\text{AdOH}))$$

Period	N2O_by-pass <sub>y</sub> kg	P_AdOH <sub>y</sub> t	%_on-line <sub>y</sub> %
Sept 1 <sup>st</sup> – Oct 22 <sup>nd</sup>	1 301 898	19813.000	75.66323



## Appendix 7

Name of item

Q\_N2O\_by-pass

Description

N2O by-passing the decomposition facility

Value in period

1 301 898 kg
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Method of monitoring

Production record and %\_on-line DCS monitoring

Recording frequency

Monthly

Background data

Production & %\_on-line log sheet record

Calculation method

The quantity of adipic acid produced while by-passing the destruction facility is first calculated:

$AdOH_{by-pass} = P_{AdOH} \times (1 - \%_{on-line})$

The quantity of N2O that by-pass the facility is then recorded daily.

$N2O_{by-pass_d} = P_{AdOH_d} \times N2O_{/AdOH} \times (1 - \%_{on-line})$

At the end of the period the quantity of N2O that by-passed the facility is :

$N2O_{by-pass_y} = \Sigma (N2O_{by-pass_d})$

Period	Q_N2O_by-pass kg
Sept 1 <sup>st</sup> – Oct 22 <sup>nd</sup>	1 301 898



## Appendix 8

Name of item	P_AdOH
Description	Adipic acid production
Value in period	19813 t
Method of monitoring	Packaged production and silo inventory
Recording frequency	Monthly
Background data	Log sheet record

Month - year	Adipic acid production t
Sept 1 <sup>st</sup> – Oct 22 <sup>nd</sup>	19813



## Appendix 9

Name of item	N2O_AdOH
Description	N2O emission factor for adipic acid production
Value in period	0.270 kg N2O/ kg AdOH
Method of monitoring	Adipic acid production, nitric acid consumption and physical losses
Recording frequency	Period
Background data	Log sheet records
Calculation method	<p>Nitric acid physical losses (HNO3_physical) in the aqueous waste, the off gases, the adipic acid and the by-product are monitored.</p> <p>Those losses are deducted from the nitric acid consumption HNO3_consumption to get the chemical consumption HNO3_chemical.</p> <p>The N2O emission factor is then calculated over the period :</p> $\text{N2O\_AdOH} = \text{HNO3\_chemical} / \text{P\_AdOH} / 63 / 2 \times 0.96 / 44$

Year ending	Value calculated kg N2O/kg AdOH	N2O_AdOH kg N2O/kg AdOH
Oct 22 <sup>nd</sup> 06	> 0.270	0.270



## Appendix 10

Name of item	$Q_{N_2O \text{ reg}}$ , $N_2O_{\text{reg}}$ / AdOH and $r_y$
Description	<p>Evolution of Korean legislation that may require limitation of <math>N_2O</math> emissions using one of the following criteria:</p> <ul style="list-style-type: none"> <li>- <math>Q_{N_2O \text{ reg}}</math> : allowed <math>N_2O</math> emissions</li> <li>- <math>N_2O_{\text{reg}}</math> / AdOH : allowed <math>N_2O</math> emissions per kg of adipic acid produced</li> <li>- <math>r_y</math> : share of <math>N_2O</math> emissions required to be destroyed</li> </ul>
Value in period	not applicable
Method of monitoring	Survey
Recording frequency	When relevant
Background data	Korean legislation

Period	$Q_{N_2O \text{ reg}}$ t $N_2O$	$N_2O_{\text{reg}}$ / AdOH t $N_2O$ / t adipic acid	$r_y$ %
Sept 1 <sup>st</sup> – Oct 22 <sup>nd</sup>	No limit	No limit	0.



## Appendix 11

Name of item

Description

Value in period

Method of monitoring

Recording frequency

Background data

P\_N<sub>2</sub>O

Market price of N<sub>2</sub>O

0 €/t

Market survey

Yearly

No market for this low level of N<sub>2</sub>O concentration

Year	P_N <sub>2</sub> O
2005	0





## Appendix 12

Name of item	Q_Steam_p	
Description	Amount of steam produced by the decomposition facility	
Value in period	<table border="1"><tr><td>24 768 597 kg</td></tr></table>	24 768 597 kg
24 768 597 kg		
Method of monitoring	Flowmeter	
Recording frequency	Monthly	
Background data	Log sheet record	

Period	Q_Steam_p kg
Sept 1 <sup>st</sup> – Oct 22 <sup>nd</sup>	24 768 597



### Appendix 13

Name of item	E_Steam
Description	CO <sub>2</sub> emission factor for steam produced by the facility
Value in period	0.122 kg-CO <sub>2</sub> /kg of steam
Method of monitoring	Supplier data
Recording frequency	Yearly
Background data	Monthly external natural gas data from supplier
Calculation method	As we cannot get the data from the supplier, the calculation is made according to the monitoring plan. We first calculate the amount of natural gas required to generate steam in Nm <sup>3</sup> /t of steam in a very efficient boiler $QNG\_tsteam = \Delta H \text{ (kcal/t)} / (\text{LHV (kcal/Nm}^3\text{)} \times \eta \text{ (\%)})$ The LHV data is the yearly average value for the gas supplied by Kyung Dong City Gas Co,Ltd

Year ending	LHV kcal/Nm <sup>3</sup>	$\Delta H$ kcal/t	$\eta$ %	QNG_tsteam Nm <sup>3</sup> /t of steam	E_NG kg- CO <sub>2</sub> /Nm <sup>3</sup>	E_Steam kg-CO <sub>2</sub> / kg of steam
Sept 30 <sup>th</sup> 2006	10522	557960	97	54.669	2.240	0.122



#### Appendix 14

Name of item

Q\_Power

Description

Electricity consumption by the decomposition facility

Value in period

233 395 kWh

Method of monitoring

Power consumption data

Recording frequency

Monthly

Background data

Log sheet record / counter

Period	Q_Power kWh
Sept 1 <sup>st</sup> – Oct 22 <sup>nd</sup>	233 395



## Appendix 15

Name of item	E_Power
Description	CO2 intensity for electric generation
Value in period	0.649 kg-CO <sub>2</sub> /kWh
Method of monitoring	Survey of data publication
Recording frequency	Yearly
Background data	KEPCO data make publicly available by the Korean Energy Economics Institute (KEEI) for 2003, 2004 & 2005.
Calculation method	Calculated using the combined margin (CM) approach according to ACM0002. Conservative value used.

Date (year)	E_Power kg-CO <sub>2</sub> /kWh
Sept 1 <sup>st</sup> – Oct 22 <sup>nd</sup>	0.649



## **Appendix 16**

Name of item                      Q\_Steam\_c  
Description                      Amount of steam consumed by the decomposition facility

Value in period                      

140 723 kg
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Method of monitoring                      Mass flowmeter  
Recording frequency                      Monthly  
Background data                      Log sheet record

Period	Q_Steam_c kg
Sept 1 <sup>st</sup> – Oct 22 <sup>nd</sup>	140 723



## Appendix 17

Name of item	E_Steam_c
Description	CO2 intensity for steam consumed in the facility
Value in period	0.137 kg-CO <sub>2</sub> /kg of steam
Method of monitoring	Calculated from steam supplier data
Recording frequency	Yearly
Background data	Log sheet records / Composition from Kyung Dong City Gas Ltd, the natural gas supplier
Calculation method	<p>This steam is supplied by existing boilers on site. Steam production and natural gas consumption are monitored. They are used to calculate the natural gas consumption</p> <p>Q_NG_steam in Nm<sup>3</sup>/t of steam.</p> <p>E_Steam is obtained by using the CO<sub>2</sub> emission factor E_NG (see appendix 4)</p> <p><math>E\_Steam = QNG\_steam \times E\_NG</math></p>

Year ending	Q_NG_steam Nm <sup>3</sup> /t of steam	E_NG kg-CO <sub>2</sub> /Nm <sup>3</sup>	E_Steam kg-CO <sub>2</sub> / kg of steam
Oct 22 <sup>nd</sup> 2006	60.87	2.240	0.137