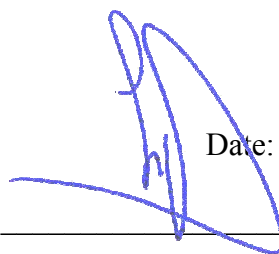




**CDM  
MONITORING REPORT # 26  
of  
“N2O Emission Reduction in Paulinia,  
SP, Brazil”  
UNFCCC 0116**

**From: June 25, 2009  
To: July 15, 2009**

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## 1 Introduction

The purpose of this monitoring report is to calculate and clarify GHG emission reduction quantity achieved by this project for periodic verification.

This monitoring report covers the activity from June 25<sup>th</sup>, 2009 to July 15<sup>th</sup>, 2009 as the 26<sup>th</sup> period.

Duration of the project activity period

The starting date of the project is defined as 11/19/2006.

Note: In the PDD the original starting date of the project activity is 01/01/2007. A demand to the UNFCCC for anticipating the actual start up of the project activity to 11/19/2006 was made and approved. The new starting date of the project activity has been updated on the UNFCCC website.

## 2. Reference

### **Approved Baseline methodology :**

Baseline Methodology for decomposition of N<sub>2</sub>O from existing adipic acid production plants (AM0021/version 1)

### **Approved Monitoring methodology :**

Monitoring Methodology for decomposition of N<sub>2</sub>O from existing adipic acid production plants (AM0021/version 1)

### **Project Design Document :**

N<sub>2</sub>O Emission Reduction in Paulinia, SP, Brazil.

Version number of the document : 4

Date : October 12<sup>th</sup>, 2005

### **CDM registration number :**

“N<sub>2</sub>O Emission Reduction in Paulinia, SP, Brazil” – UNFCCC ref number 0116

### **Directly related EB guidance:**

EB45 Annex13 “Guidance to calculate adipic acid production in cases where it cannot be measured directly” version 1, February 13<sup>th</sup> 2009

## 3. Definition

y : Monitoring period (in this report, see dates § 1)

PDD : Project Design Document of this project “N<sub>2</sub>O Emission Reduction in Paulinia, SP, Brazil.” Version number of the document: 4, issued on October, 12<sup>th</sup>, 2005

## 4. General description of project

### 4.1 Project activity

Nitrous oxide (N<sub>2</sub>O) is a by-product of adipic acid production. It is of low toxicity but is a greenhouse gas (GHG), whose GWP is large (GWP=310 in the IPCC 2nd Assessment Report). Emissions of N<sub>2</sub>O will be controlled under the Kyoto Protocol. As far as we are aware, there are however no national or regional regulations or restrictions on the emission of N<sub>2</sub>O in Brazil. There are in fact no governmental regulations with quantified emission limits in any non-Annex I countries at this point.

In this project, Rhodia Poliamida e Especialidades Ltda. additionally installed N<sub>2</sub>O collection and a thermal decomposition process equipment to the currently operating adipic acid manufacturing plant. This installation reduces the GHG emissions, which would otherwise be released to the atmosphere if the project were not implemented.

The decomposition facility was installed in the factory site of Paulinia Rhodia Poliamida e Especialidades Ltda. in October 2006 and destruction of N<sub>2</sub>O was started in November 2006. The starting date of the project as well as the starting date of the first crediting period is defined as November 19<sup>th</sup>, 2006. It should be noted that the original starting date of the project activity is 01/01/2007 according to the PDD. However the start up of the project activity was anticipated to 11/19/2006, as formalized to and approved by the UNFCCC.

This project activity was registered at UNFCCC on December 25<sup>th</sup>, 2005 with the number 0116.

### 4.2 Technical description of the project

#### **Location of the project activity**

The decomposition facilities were installed in the factory site Rhodia Poliamida e Especialidades Ltda in Paulínia, SP, Brazil in October, 2006.

#### **Technology employed by the project activity**

A thermal oxidizer with 2 chambers is the technology used to decompose N<sub>2</sub>O.

Natural gas is fed with the off gas adipic acid production containing N<sub>2</sub>O and some air in a reduction chamber, where it burns (oxidizes) to carbon dioxide CO<sub>2</sub> and water vapour. N<sub>2</sub>O is used as an oxidizer. Being oxygen deficient, the oxidation is not complete and carbon monoxide and hydrogen are present.

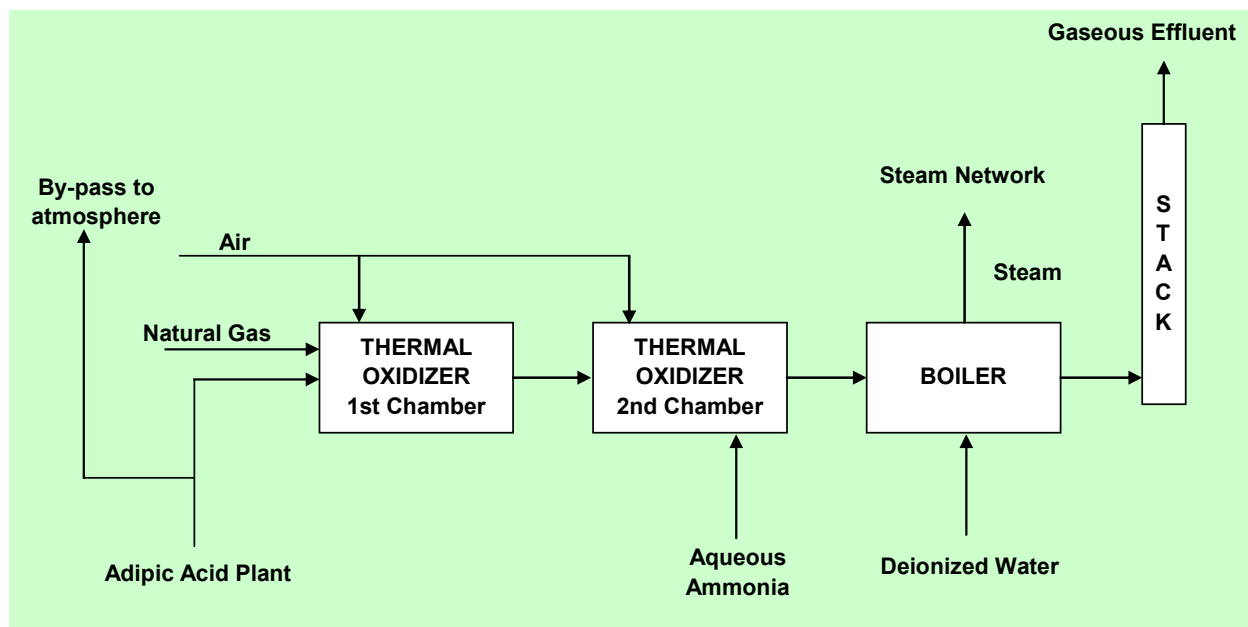


The temperature in the furnace is kept at about 1300°C and under fuel rich conditions, so as to promote the complete decomposition of N<sub>2</sub>O while minimizing the formation of unwanted combustion by-products such as NO and NO<sub>2</sub>.



The gas is then quenched with air to complete the combustion of carbon monoxide and hydrogen at a temperature of about 950°C in a second chamber. Aqueous ammonia is injected to control the emission of NO and NO<sub>2</sub>.

Before release to the stack, the flue gas coming from the thermal oxidizer is used to produce superheated steam, which is fed into the existing on-site steam network.



#### 4.3 Implementation of the project

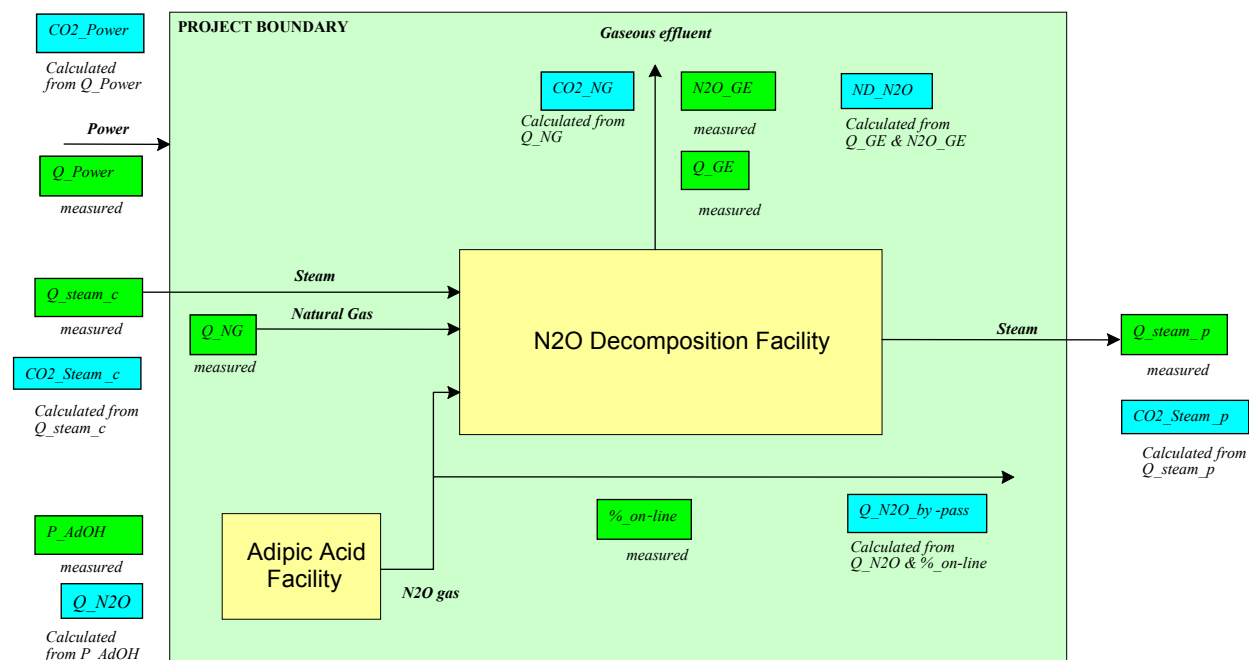
The project is fully implemented according to the description presented in the PDD. The project activity is completely operational.

## 5. Baseline methodology

Approved baseline methodology AM 0021 / version 1: “Baseline methodology for decomposition of N<sub>2</sub>O from existing adipic acid production plants” is applied to this project.

The project boundary related to the baseline methodology is shown below and this project boundary is used and explained in the PDD.

Potential sources of anthropogenic emissions by sources of GHG within the project boundary and emissions which are not included in the project boundary are also shown in below.



## 6. Applicability of the methodology

Approved monitoring methodology AM 0021 / version 1 is applied to this project.

This methodology is applicable to projects which decompose N<sub>2</sub>O from an adipic acid production plant under the following conditions:

- either catalytic or thermal decomposition of the N<sub>2</sub>O by-product of adipic acid production at existing production plants
- The methodology is spatially generic, being applicable across regions where the data (both related and project activity as well) exist to undertake the assessment
- The methodology is applicable only for installed capacity (measured in tonnes of adipic acid per year) that exists by the end of the year 2004.

The present project satisfies these conditions as:

- Thermal decomposition of the N<sub>2</sub>O by-product of adipic acid production was implemented in an existing production plant
- All required data (see following paragraph) are available and used
- The production of adipic acid within the current year is below the installed capacity that exists by the end of the year 2004 as defined in the PDD.

For the sake of clarity, the amount of Emission Reductions can exceed the amount calculated in a year period in the PDD in "SECTION E. Estimation of GHG emissions by sources" as all data in the PDD were conservative, in particular the performance of the N<sub>2</sub>O abatement unit (in fact, the actual efficiency has been > 85%, and the destruction rate > 99%).

## 7. Monitored Parameters

According to the methodology AM 0021/version 1 and the Monitoring Plan, the data being collected to monitor the GHG reduction are given in the table below:

ID	Data variable	Source of data	Data unit	Recording frequency	Reference
Q_GE	Volume of effluent gas leaving the stack	Flow meter	Nm <sup>3</sup>	Monthly	Appendix 1
N <sub>2</sub> O_GE	Concentration of N <sub>2</sub> O in the effluent gas	Laser diode online analyzer	ppm	Monthly	Appendix 2
ND_N2O	Quantity of N <sub>2</sub> O in the effluent gas leaving the stack	Calculated from Q_GE and N <sub>2</sub> O_GE	kg	Monthly	Appendix 3
Q_NG	Amount of natural gas burned	Natural gas meter	Nm <sup>3</sup>	Monthly	Appendix 4
NGC	Natural gas composition required for calculation of E_NG	Gas supplier	-	Monthly	Appendix 5
%_on-line	% of production time the position switch on the by-pass valve is closed	Position switches on bypass valve	% of production time	Monthly	Appendix 6
Q_N2O_by-pass	N <sub>2</sub> O by passing the decomposition facility	Calculated from Q_N2O and %_on-line	kg	Monthly	Appendix 7

ID	Data variable	Source of data	Data unit	Recording frequency	Reference
P_AdOH	Amount of adipic acid production	Excel workbook for calculation of nylon salt production, AA slurry production and dry AA production	ton	Monthly	Appendix 8
Nitric acid consumption (HNO <sub>3</sub> _consumption) & physical losses in the adipic acid production process (HNO <sub>3</sub> _physical)	All data required for calculation of HNO <sub>3</sub> chemical and the N <sub>2</sub> O emission factor N <sub>2</sub> O_AdOH	Excel workbook based on the raw material consumption, DCS data and Lab data	ton	Monthly	Appendix 9
Q N <sub>2</sub> O reg	Per Brazilian regulation allowed N <sub>2</sub> O emissions	Brazilian regulation	kg/a	Date when relevant legislation is in place	Appendix 10
N <sub>2</sub> O reg/AdOH	Per Brazilian regulation allowed N <sub>2</sub> O emissions per kg of adipic acid produced	Brazilian regulation	kg/kg	Date when relevant legislation is in place	Appendix 10
r <sub>y</sub>	Per Brazilian regulation required share of N <sub>2</sub> O emissions to be destroyed	Brazilian regulation	%	Date when relevant legislation is in place	Appendix 10
P N <sub>2</sub> O	Market price of N <sub>2</sub> O	Estimated	€/t	Yearly	Appendix 11
Q_Steam_p	Amount of steam produced by the decomposition process	Steam meter	kg	Monthly	Appendix 12





ID	Data variable	Source of data	Data unit	Recording frequency	Reference
Steam supplier data	All data required for calculation of E_Steam	Rhodia Industrial Platform of Paulínia	-	Yearly	Appendix 13
Q_Power	Electric consumption of the decomposition facility	Electricity meter	kWh	Monthly	Appendix 14
Electricity grid data	All data required for calculation of E_Power according to ACM0002 version 2 and the Monitoring Plan	Brazilian ONS (Operador Nacional do Sistema Elétrico)	-	Yearly	Appendix 15
Q_Steam_c	Amount of steam consumed by the decomposition facility	Steam meter	kg	Monthly	Appendix 16
Steam suppliers data	All data required for calculation of E_Steam_c	Rhodia Industrial Platform of Paulínia	-	Yearly	Appendix 17

## 8. Quality Control (QC) and Quality Assurance (QA)

### 8.1. Quality Management System

The Rhodia site is ISO 9001:2000 certified covering also the adipic acid plant and the N<sub>2</sub>O decomposition unit. The Quality Management System helps Rhodia to continually improve its product, processes and services, which includes quality planning, management responsibility, documentation and data control, resources management, product realization, process analysis and improvement. Rhodia site is also ISO 14000 certified.

The thermal oxidation plant is operated by Rhodia operating personnel. Rhodia has assigned the responsibility for operating, monitoring and reporting to the Adipic Acid Plant Manager.

The operation, data transfer and reporting procedures are incorporated into the ISO 9001 procedures of the Paulínia Adipic Acid plant.

The personnel have been trained by Rhodia engineers who have been trained by the technology supplier i.e. John Zink Company LLC, USA.



## 8.2. Quality control (QC) and quality assurance (QA) procedures that are being undertaken for data monitored

The Paulínia adipic acid plant is certified according to ISO9001 and applies appropriate QA & QC procedures.

The equipment and analytical methods given by the technology supplier John Zink Company LLC, USA as well as those supplied by Rhodia are done according to internationally accepted standards.

The QA & QC procedures are set and implemented in order to:

1. Secure a good consistency through planning to implementation of this CDM project and,
2. Stipulate who has responsibility for what and,
3. Avoid any misunderstanding between people and organization involved.

Data (Indicate table and ID number e.g. 3.-1.; 3.2.)	Uncertainty level of data (High/Medium/Low)	Explain QA/QC procedures planned for these data, or why such procedures are not necessary.
2a.1. (D.2.1.1) Q_GE	Low	<i>This flow rate is measured with an Averaging Pitot tube. This instrument is a critical instrument in the QA/QC procedure.</i>
2a.2. (D.2.1.1) N <sub>2</sub> O_GE	Low	<i>Measured using Laser Diode technology Specific procedures are applied to this analyzer for QA &amp; QC following the manufacturer's recommendation.</i>
2a.4. (D.2.1.1) Q_NG	Low	<i>Is measured using natural gas meter from the supplier and as such is part of a regular procedure control between the Natural Gas supplier and Rhodia.</i>
2b.1. (D.2.1.3) P_ADOH	Low	<i>Is obtained from production records of the Paulínia Adipic Acid plant where the N<sub>2</sub>O waste originates. A QA/QC procedure is implemented. Production quantity is based on the packaged product plus slurry production used for the Nylon Salt production. Both dry adipic acid and nylon salt are weighed.</i>
2a.5. (D.2.1.1) %_on-line	Low	<i>Use high integrity performance by-pass valve to limit leaks. Procedures currently in place in Chalampé for monitoring N<sub>2</sub>O emissions have been implemented in Paulinia to periodically check their tightness and assure their good operation. They have been added to the QA/QC existing procedures.</i>
2b.7. (D.2.1.3) Q_Steam_p	Low	<i>Steam meter placed on the list of critical instrument data in the QA/QC procedures</i>
3.1. (D.2.3.1) Q_Power	Low	<i>Electricity meter. Standard procedures are used. No QA/QC procedures implemented as this flow represents less than 0.01% of the baseline emissions.</i>
3.4. (D.2.3.1) Q_Steam_c	Low	<i>Steam meter placed on the list of critical instrument data in the QA/QC procedures.</i>

### Main QC and QA procedures specific to the project activity:

Data Handling Protocol ISAL-ADOH-QA-007

Data Review Protocol ISAL-ADOH-QA-008



### 8.3. Calibration/Maintenance of Measuring and Analytical Instruments

All measuring and analytical instruments are being calibrated as per the methodology AM0021/version 1 and the PDD using either existing or specifically created protocols in Paulinia's Quality Management System procedures.

The maintenance methods and procedures have been incorporated as part of the ISO 9001 procedures and form an integral part of the systems and procedures for the organization.

The Monitoring Equipment Calibration and Maintenance status is presented on Appendix 18.

### 8.4. Environmental Impact

After commissioning the thermal oxidation plant, online analysis of the NO<sub>x</sub> content in the gaseous effluents is carried out to verify such discharge from the plant. Monitoring of the NO<sub>x</sub> content in the waste gas is required by local environmental legislation stated in the Commitment Agreement (TAC) signed with the Public Attorney of the State of São Paulo. NO<sub>x</sub> in the gaseous effluent can be randomly checked by the environmental agency Cetesb through sampling and analysis by an external laboratory. Analytical data show that the plant complies with the established environmental standard.

Table showing analysis of Gaseous Emission for Thermal Oxidation plant

Parameter	Unit	Limit as per applicable standard	Analytical results in this period
NO <sub>x</sub>	vppm	300 max at least 95% of time	Average of 45 and less than 300 for 99.6% of time

## 9. GHG Calculations

A spreadsheet Excel file "WORKBOOK ER PAULINIA" containing all the values of the monitoring parameters and the emission reduction calculation according to the methodology (AM0021/version 1) and the PDD is submitted to the DOE and to the UNFCCC for the request of issuance.

Statement of GHG emission reduction in this monitoring period.

As suggested by the methodology (AM0021/version 1), the GHG emission reduction, (ER<sub>y</sub>), achieved by the project activity for the period is  
$$ER_y = BE_y - PE_y - L_y$$

### 9.1. Calculation of Q\_N2Oy

It has been checked that there are no Brazilian regulation into place that would limit the quantity of N<sub>2</sub>O emitted that can be taken into account for the calculation of the baseline emissions (see D.2.1.4. in the PDD).

The quantity Q\_N2Oy of N<sub>2</sub>O emitted over the period can then be calculated by (AM0021/version 1 equation (2)):

$$Q_{N2Oy} = P_{AdOH} \times N2O_{/AdOH}$$

Over the period of reference the emission factor from the adipic acid plant was above the capped value of 0.27 kg N<sub>2</sub>O/kg AdOH (see Appendix 9). So the capped value is being used according to AM 0021/version 1.

Parameter	Value	Reference
Q_N2Oy	1 282 857 kg	Calculated
P_AdOH	4 751.3	Appendix 8
N2O_/AdOH	0.27 kg N2O/kg AdOH	Appendix 9
Q_N2O reg	No limit	Appendix 10
N2O_reg / AdOH	No limit	Appendix 10
r <sub>y</sub>	NA	Appendix 10

The Executive Board has confirmed on EB36 the application of a yearly Adipic acid production cap as required by the methodology. The current year period started on November 19, 2008 and will end on November 18, 2009. The accumulated production of adipic acid in the period starting on November 19, 2008 and ending in the last day of this period is lower than 87 308 tons which is the yearly capped value as stated in the decision made by the EB47th meeting on 28<sup>th</sup> May 2009. Therefore the total production of this period can be used as such (see details in Appendix 8). This approach is consistent with the definitions and requirements of the "Guidance on accounting eligible HFC-23" AM0001 (EB39 Annex 8): the year of the crediting period is defined on the basis of the starting date of the crediting period of a project activity (in the present case November 19th).

### 9.2. Calculation of baseline emissions

The amount of baseline emissions in the given period y (measured in t CO<sub>2</sub> eq.) is calculated by (AM0021/version 1 equation (1)):

$$BE_y = Q_{N2Oy} \times GWP_{N2O} + Q_{Steam_{py}} \times E_{Steam_y}$$

and rounded down in t CO<sub>2</sub> eq. to get conservative consistency of final calculation of emission reductions formula.

Parameter	Value	Reference
<b>BE<sub>y</sub></b>	<b>398 476 t CO<sub>2</sub> eq.</b>	Calculated
Q_N <sub>2</sub> O <sub>y</sub>	1 282 857 kg	Calculated in 9.1
GWP_N <sub>2</sub> O	310 kg CO <sub>2</sub> eq./ kg N <sub>2</sub> O	Kyoto Protocol Rule. Decision 2/CP.3 and IPCC
Q_Steam <sub>y</sub>	5 455 200 kg of steam	Appendix 12
E_Steam <sub>y</sub>	0.145 kg-CO <sub>2</sub> /kg of steam	Appendix 13

### 9.3. Calculation of (Q\_N<sub>2</sub>O x (1-%\_on-line))<sub>y</sub>

The quantity of N<sub>2</sub>O that has by-passed the decomposition facility is calculated from the adipic acid production made while by-passing the decomposition facility.

The quantity of adipic acid produced while by-passing the destruction facility is monitored and the quantity of N<sub>2</sub>O that by-pass the decomposition facility is registered daily:

$$Q_{N_2O\_by-pass} = P_{AdOH} \times (1 - \%_{on-line}) \times N_{2O\_AdOH}$$

This value is a value by excess as during each connection/ disconnection phases the production is counted as completely by-passed.

The quantity of N<sub>2</sub>O that by-passed the decomposition facility over the period is:

$$(Q_{N_2O} \times (1 - \%_{on-line}))_y = Q_{N_2O\_by-pass}_y$$

The %\_on-line<sub>y</sub> equivalent over the period is calculated as:

$$\%_{on-line}_y = 1 - (Q_{N_2O\_by-pass}_y / Q_{N_2O}_y)$$

Parameter	Value	Reference
Q_N <sub>2</sub> O_by-pass <sub>y</sub>	36 342 kg	Appendix 7
P_AdOH	4 751.3 t	Appendix 8
N <sub>2</sub> O_AdOH	0.27 kg N <sub>2</sub> O/kg AdOH	Appendix 9
%_on-line <sub>y</sub>	97.167 %	Appendix 6

### 9.4. Calculation of project emissions

The emissions due to the decomposition process PE<sub>y</sub> are the emissions due to the N<sub>2</sub>O that has not been sent to the decomposition process, the N<sub>2</sub>O non destroyed by the decomposition process and the emissions due to the use of natural gas.

$$PE_y = ((Q_{N_2O} \times (1 - \%_{on-line}))_y + (Q_{GE} \times N_{2O\_GE} \times Specific\_gravity\_of\_N_{2O})_y) \times GWP_{N_2O} + Q_{NGy} \times E_{NGy} \quad (AM0021/version 1 equation (6))$$

$$PE_y = (Q_{N_2O\_by-pass}_y + (Q_{GE} \times N_{2O\_GE} \times Specific\_gravity\_of\_N_{2O})_y) \times GWP_{N_2O} + Q_{NGy} \times E_{NGy}$$



The non-destroyed N<sub>2</sub>O (ND\_ N<sub>2</sub>O<sub>y</sub>) is constantly monitored and obtained from the constant monitoring of the flow (Q\_GE) and the concentration of N<sub>2</sub>O (N<sub>2</sub>O\_GE) of the effluent gas:  
 $ND\_N_2O = Q\_GE \times N_2O\_GE \times Specific\_gravity\_of\_N_2O$

$PE_y = (Q\_N_2O\_by-pass_y + ND\_N_2O_y) \times GWP\_N_2O + Q\_NG_y \times E\_NG_y$  (AM0021/version 1 equation (5))

PE<sub>y</sub> is rounded up in t CO<sub>2</sub> eq. to get conservative consistency in final calculation of emission reductions formula.

Parameter	Value	Reference
<b>PE<sub>y</sub></b>	<b>12 231 t CO<sub>2</sub> eq.</b>	Calculated
Q_N2O_by-pass <sub>y</sub>	36 342 kg	Appendix 7
Q_GE	5 853 796 Nm <sup>3</sup>	Appendix 1
N <sub>2</sub> O_GE	17.0 vppm	Appendix 2
Specific gravity of N <sub>2</sub> O	$1.963 \times 10^{-6}$	Appendix 2 and 3
ND_ N <sub>2</sub> O <sub>y</sub>	197 kg N <sub>2</sub> O	Appendix 3
GWP_ N <sub>2</sub> O	310 kg CO <sub>2</sub> eq./ kg N <sub>2</sub> O	Kyoto Protocol Rule. Decision 2/CP.3 and IPCC
Q_NG <sub>y</sub>	410 058 Nm <sup>3</sup>	Appendix 4
E_NG <sub>y</sub>	2.211 kg CO <sub>2</sub> eq./ Nm <sup>3</sup>	Appendix 5

Note:

- 1) The value of E\_NG<sub>y</sub> shown above is the yearly moving average of E\_NG as required by the PDD for calculation of E\_Steam. The project emissions are more accurately calculated using the monthly values of E\_NG shown in Appendix 5, following methodology AM0021/version 1 and the Monitoring Plan.
- 2) The value of ND\_N<sub>2</sub>O<sub>y</sub> is calculated by the DCS using every 10 second data of Q\_GE and N<sub>2</sub>O\_GE (see Appendix 2 and 3) and is more accurate than the value calculated using total average values.

### 9.5. Calculation of leakage

Leak emissions comprise the emissions associated with the energy sources used to generate any steam and electricity used by the decomposition plant.

Leakage amounts to (AM0021/version 1 equation (7) ):

$$L_y = Q\_Power \times E\_Power + Q\_steam\_c_y \times E\_steam\_c_y$$

L<sub>y</sub> is rounded up in tCO<sub>2</sub> eq. to get conservative consistency in final calculation of emission reductions formula.

Parameter	Value	Reference
<b>Ly</b>	<b>32 t CO<sub>2</sub> eq.</b>	Calculated
Q_Power	25 451 kWh	Appendix 14
E_Power	1.095 kg CO <sub>2</sub> /kWh	Appendix 15
Q_Steam_c <sub>y</sub>	18 000 kg	Appendix 16
E_Steam_c <sub>y</sub>	0.214 kg CO <sub>2</sub> / kg of steam	Appendix 17

#### 9.6. Calculation of emission reduction

Following the PDD section D.2.4, the total emission reduction achieved by this project activity during this monitoring period is therefore,

$$ER_y = BE_y - PE_y - Ly$$

Or,

$$ER_y = 398\,476 \text{ t CO}_2 \text{ eq.} - 12\,231 \text{ t CO}_2 \text{ eq.} - 32 \text{ t CO}_2 \text{ eq.}$$

Or,

$$ER_y = 386\,213 \text{ t CO}_2 \text{ eq.}$$

The above emission reduction covers the generation of N<sub>2</sub>O during this monitoring period.

#### 9.7. Comparison of the emission reduction with the PDD estimates

In the PDD section E, the annual emission reduction is estimated to be 5 961 165 tCO<sub>2</sub>eq. So the PDD-estimated emission reduction relative to the monitoring period of 21 days is around 342 971 tCO<sub>2</sub>eq. The higher volume of the actual emission reduction is explained by the significant higher performance of the N<sub>2</sub>O abatement unit (the actual %\_on-line of 97.167% in this period is significantly higher than the value of 85% estimated in the PDD due to excellent operational performance). The estimate of 85% in the PDD assumed a low performance rate of the destruction equipment due to the lack of experience with such equipment. Moreover, given the general experiences with consistent overestimation of CER volumes in the first years of CDM project development, Rhodia wanted to set the CER estimates in the PDD in a conservative fashion, especially regarding performance of the abatement equipment.



## **Appendix 1**

Name of item	Q_GE
Description	Volume of effluent gas leaving the stack
Value in period	5 853 796 Nm <sup>3</sup>
Method of monitoring	Annubar flow meter
Recording frequency	Monthly
Background data	Log sheet record / flowmeter

Period	Quantity of gaseous effluent Nm <sup>3</sup>
June 25 <sup>th</sup> – June 30 <sup>th</sup> , 2009	1 559 789
July 1 <sup>st</sup> – July 15 <sup>th</sup> , 2009	4 294 007





## **Appendix 2**

Name of item	N2O_GE
Description	Concentration of N <sub>2</sub> O in the effluent gas
Value in period	17.0 vppm
Method of monitoring	Laser diode online analyzer
Recording frequency	Monthly
Background data	Log sheet record
Calculation method	<p>According to AM0021/version1, the instant values of the on-line analyzer is used to calculate the quantity of ND_N2O every 10 sec:</p> $ND\_N2O = Q\_GE \times N2O\_GE \times Specific\_gravity\_of\_N2O$ <p>N2O_GE need to be converted in kg/Nm<sup>3</sup> according to AM0021/version1 note 2 table 2a, using the specific_gravity_of_N2O = 44/22.414 x 10<sup>-6</sup></p> <p>The analyzer has a range of 0-500 ppm with a detection limit of 5 ppm (1% of range). We use 5 ppm as a default value when the measured value is below the detection limit.</p> <p>Cumulated value for ND_N2O is recorded (see appendix 3).</p> <p>At the end of the month/period based upon the flow Q_GE, and ND_N2O the concentration of N2O equivalent for the month/period is calculated.</p> $N2O\_GE = ND\_N2O / (Q\_GE \times N2O\_GE \times Specific\_gravity\_of\_N2O)$ <p>This value is for information as the constant calculation of ND_N2O is more accurate.</p>

Period	ND_N2O Kg	Quantity of gaseous effluent Nm <sup>3</sup>	Average concentration of N <sub>2</sub> O_GE vppm
June 25 <sup>th</sup> – June 30 <sup>th</sup> , 2009	42	1 559 789	13.4
July 1 <sup>st</sup> – July 15 <sup>th</sup> , 2009	155	4 294 007	18.3



### **Appendix 3**

Name of item	ND_N2O
Description	Quantity of non-destroyed N2O emitted by the decomposition facility
Value in period	197 kg N <sub>2</sub> O
Method of monitoring	On-line DCS calculation
Recording frequency	Monthly
Background data	Log sheet record
Calculation method	According to AM0021/version1, the actual quantity of non destroyed N2O is calculated on-line in the DCS from the concentration of N2O and the flow rate of the gaseous effluent, both measured on a wet basis (Method D) of EB47 “Tool to determine the mass flow of a greenhouse gas in a gaseous stream”: $ND\_N2O = Q\_GE * N2O\_GE * Specific\_gravity\_of\_N2O$ N2O_GE need to be converted in kg/Nm <sup>3</sup> according to AM0021/version1 note 2 table 2a, using the $specific\_gravity\_of\_N2O = 44/22.414 \times 10^{-6}$

Period	ND_N2O kg
June 25 <sup>th</sup> – June 30 <sup>th</sup> , 2009	42
July 1 <sup>st</sup> – July 15 <sup>th</sup> , 2009	155



#### **Appendix 4**

Name of item	Q_NG
Description	Amount of natural gas used by the decomposition process
Value in period	410 058 Nm <sup>3</sup>
Method of monitoring	Natural gas consumption data
Recording frequency	Monthly
Background data	Log sheet record / flowmeter

Period	Q_NG Nm <sup>3</sup>
June 25 <sup>th</sup> – June 30 <sup>th</sup> , 2009	107 798
July 1 <sup>st</sup> – July 15 <sup>th</sup> , 2009	302 260

## Appendix 5

Name of item	E_NGy with NGC
Description	Emissions coefficient for natural gas combustion Natural Gas Composition (NGC) is informed by the natural gas supplier
Value in period for E_NG <sub>y</sub>	2.211 kg CO <sub>2</sub> /Nm <sup>3</sup>
Method of monitoring	Natural Gas Composition (NGC)
Recording frequency	Monthly
Background data	Composition data received from COMGAS, the natural gas supplier
Calculation method	Following the PDD Monitoring Plan The average number of C in a mole of NG is calculated from the composition = $\sum$ (number of C in each mole) x (volume ratio) Following monthly data are used to calculate monthly project emissions due to the consumption of Natural Gas. For this monitoring period was applied only June data, because July data are not available yet.

The yearly value (E\_NGy) is calculated with the data available for the year prior to the beginning of the period and is used for the calculation of E\_Steam.

Component	June Natural Gas Composition	Number of C
CH <sub>4</sub> (Methane)	88.83	1
C <sub>2</sub> H <sub>6</sub> (Ethane)	6.19	2
C <sub>3</sub> H <sub>8</sub> (Propane)	1.78	3
I-C <sub>4</sub> H <sub>10</sub> (I-Butane)	0.27	4
N-C <sub>4</sub> H <sub>10</sub> (N-Butane)	0.39	4
I-C <sub>5</sub> H <sub>12</sub> (I-Pentane)	0.11	5
N-C <sub>5</sub> H <sub>12</sub> (N-Pentane)	0.08	5
C <sub>6</sub> H <sub>14</sub> + (Hexane)	0.06	6
N <sub>2</sub> (Nitrogen)	0.71	0
CO <sub>2</sub> (Carbon dioxide)	1.58	1
Average number of C	1.121	
E_NG (month)	<b>2.202</b>	

The CO<sub>2</sub> specific gravity in standard state is 1.965  
 $E_{NG} = 1.965 \times (\text{average number of C in a mole of NG})$



## Appendix 6

Name of item	%_on-line
Description	% of production time that the N <sub>2</sub> O is sent to the decomposition facility
Value in period	97.167 %
Method of monitoring	Position of limit switch on the valve allowing to by-pass the decomposition facility
Recording frequency	Monthly
Background data	Log sheet record
Calculation method	<p>%_on-line is determined following the PDD. Based upon the position of the limit switch on the valve by-passing the decomposition facility, the % of time that the production is connected to the facility is continuously counted and used to calculate the daily value of Q_ N<sub>2</sub>O_by-pass (See Appendix 7). The daily values of Q_ N<sub>2</sub>O_by-pass are added to determine the monthly values of Q_ N<sub>2</sub>O_by-pass, as required by the PDD.</p> <p>At the end of the period, %_on-line for the period y is calculated as:</p> $\%_{\text{on-line}}_y = 1 - (Q_{\text{N}_2\text{O\_by-pass}}_y / (P_{\text{AdOH}}_y \times \text{N}_2\text{O\_}/\text{AdOH}))$

Period	Q_ N <sub>2</sub> O_by-pass <sub>y</sub> kg	P_ AdOH <sub>y</sub> t	%_on-line <sub>y</sub> %
June 25 <sup>th</sup> – June 30 <sup>th</sup> , 2009	36 342	1 287.6	89.547
July 1 <sup>st</sup> – July 15 <sup>th</sup> , 2009	0	3 463.7	100.000



## **Appendix 7**

Name of item	Q_N2O_by-pass
Description	N2O by-passing the decomposition facility
Value in period	36 342 kg
Method of monitoring	Production record and %_on-line DCS monitoring
Recording frequency	Monthly
Background data	Production & %_on-line log sheet record
Calculation method	<p>The quantity of N2O that by-pass the facility is then recorded daily and calculated following AM0021/version1.</p> $Q\_N2O\_by-pass_d = Q\_N2O_d \times (1 - \%\_on-line) \text{ or}$ $Q\_N2O\_by-pass_d = P\_AdOH_d \times N2O\_/AdOH \times (1 - \%\_on-line)$ <p>At the end of the period the quantity of N2O that by-passed the facility is:</p> $Q\_N2O\_by-pass_y = \Sigma (Q\_N2O\_by-pass_d)$

Period	Q_N2O_by-pass <sub>y</sub> kg
June 25 <sup>th</sup> – June 30 <sup>th</sup> , 2009	36 342
July 1 <sup>st</sup> – July 15 <sup>th</sup> , 2009	0



## **Appendix 8**

Name of item	P_AdOH
Description	Adipic acid production
Value in period	4 751.3 t
Method of monitoring	Packaged production and slurry used to nylon salt production
Recording frequency	Monthly
Background data	Log sheet record

The production of adipic acid over the year ending with the last day of this period (from November 19th, 2008 to November, 18th 2009) is  $P_{AdOH\_cur\_year} = 52\,502.3$  t lower than the yearly capped value of 87 308 t as stated by the EB 47<sup>th</sup> meeting decision on May 28<sup>th</sup> (detailed information is available in the Excel file "Workbook ER Paulinia", sheet BE, line 22, submitted to UNFCCC). Therefore, the total production of this period can be used as such. The Executive Board has confirmed on EB36 the application of a yearly Adipic acid production cap as required by the methodology. This approach is consistent with the definitions and requirements of the "Guidance on accounting eligible HFC-23" AM0001 (EB39 Annex 8): the year of the crediting period is defined on the basis of the starting date of the crediting period of a project activity (November 19th); the current period ends on November 18th, which is the end date of the year of the crediting period.

Month - year	Adipic acid production T
June 25 <sup>th</sup> – June 30 <sup>th</sup> , 2009	1 287.6
July 1 <sup>st</sup> – July 15 <sup>th</sup> , 2009	3 463.7

As described in the PDD (Section A.2, Section B.2 Table 3 and annex4 Monitoring plan), the adipic acid production is measured by adding the dry adipic acid production, the slurry adipic acid production contained in the Nylon salt, and the in-process product inventory variations. In this case:

- Dry adipic acid: is the product which was packaged (determined by weigh scales).
- Slurry adipic Acid: is the product used to be mixed in fixed proportions with Hexamethyldiamine and make Nylon salt on Paulinia site. Nylon salt quality is very



accurately analyzed and controlled. Daily Nylon salt production is obtained by the sum of the weight of the truckloads plus the variation of Nylon salt storage tank levels. Both the concentration of Nylon salt as well as adipic acid content are controlled in the Nylon salt production process: the Nylon salt concentration is monitored online by refractive index measurement and the adipic acid slurry content is monitored through precise pH measurement. Furthermore, following the Quality Control procedure to guarantee the Nylon salt specification, the content of the storage tank F5300 is analyzed every 2 hours for pH and concentration using very accurate instruments in the laboratory, according to the Quality Document “ISAL-HMD-SAL-QA-006” as stated in the PDD, section D3 line 2b.1. Should a parameter show a deviation, the Nylon salt unit operator would immediately correct the concentrations in the process to correct Nylon salt concentration and/or adipic acid content. The Nylon salt specification is very narrow ( $\pm 0.02$  for pH and  $\pm 0.2\%$  for concentration) and the analysis of the storage tank present a very low variability within those limits. This accuracy was checked by the auditor during the Initial Verification. Rhodia follows the PDD annex 3 and the monitoring plan and utilizes the Excel file “SAP-HMD.xls” to determine the nylon salt produced and automatically the corresponding adipic acid slurry. The calculation of the quantity of adipic acid in nylon salt on dry basis is based on a constant ratio of adipic acid in Nylon salt which is constant as fixed by the very precise value of the pH of the Nylon salt. The analytical results of pH and concentration of the Nylon salt solution for each period of one month are kept in an Excel file named “Qualidade SALN\_month.xls” which is shown to the DOE for verification along with the file “SAP-HMD.xls”. The ratio of Adipic Acid in Nylon Salt is 0.55748 in the Excel file “SAP-HMD.xls” in compliance with the guidance issued by the Executive Board in its 45<sup>th</sup> meeting of February 2009.

The details of the calculation of the production amount are as follows.

The total daily adipic acid made by the nitric oxidation reaction is the sum of two terms (Equation (1)):

Total Production [P_AdOH] = [Finished Product] + [Variation of the In-Process Product]	(1)
--	-----

The finished adipic acid production is obtained by adding the production of dry and slurry adipic acid, according to Equation (2).

[Finished Product] = [Dry Adipic Acid] + [Slurry Adipic Acid]	(2)
---	-----

The in-process adipic acid is obtained by adding the amount of adipic acid contained in all process equipment where adipic acid is present at different concentrations.

The variation of the In-Process Product inventory of day N is obtained by subtracting the total In-Process Product of day N minus In-Process Product of day (N-1) as in Equation (3):

[Variation of the In-Process Product] = [In-process Product of day N] – [In-process Product of day (N-1)]	(3)
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Therefore, according to described in the sections above, the total production of adipic acid is the sum of the following terms described in Equation (4), after rewriting Equation (1) using Equation (2):

Total Production [P_AdOH] = [Dry Adipic Acid] + [Slurry Adipic Acid] + [Variation of the In-Process Product]	(4)
--	-----

The total production is normally different from the finished product on a daily basis since the in-process product is always varying. The total production can be higher or lower than the finished product. On a long term basis however those differences compensate each other and the accumulated total production will of course approach the sum of dry + slurry.

For the purpose of determining the daily amount of N<sub>2</sub>O generated by the nitric oxidation of the raw materials, it must be used the total production, not the finished adipic acid production, since N<sub>2</sub>O is generated by the reaction and is independent of the finished production for a limited time (up to 1 or 2 days). In fact during such limited time the adipic acid made at the reaction can be accumulated in the process equipments awaiting to be processed through purification and drying.

## Appendix 9

Name of item	HNO <sub>3</sub> _consumption & HNO <sub>3</sub> _physical
Description	Nitric acid consumption and losses in the adipic acid process
Value in period	(see table below)
Method of monitoring	Excel workbook based on monitoring data and analysis
Recording frequency	Monthly

Background data	Log sheet records
Calculation method	Nitric acid physical losses (HNO <sub>3</sub> _physical) in the aqueous wastes, the off gases, the adipic acid and the by-product are monitored. Those losses are deducted from the nitric acid consumption, (HNO <sub>3</sub> _consumption) to get the chemical consumption, (HNO <sub>3</sub> _chemical) (AM0021/version 1 equation (3)).

Period	HNO <sub>3</sub> _consumption t	HNO <sub>3</sub> _physical t	HNO <sub>3</sub> _chemical t
June 25 <sup>th</sup> – June 30 <sup>th</sup> , 2009	1 124.9	44.1	1 080.8
July 1 <sup>st</sup> – July 15 <sup>th</sup> , 2009	3 065.0	70.4	2 994.6
Rolling year July 15 <sup>th</sup> , 2009	75 112	3 762	71 350

Name of item	N <sub>2</sub> O_AdOH
Description	N <sub>2</sub> O emission factor for adipic acid production
Value in period	0.270 kg N <sub>2</sub> O/kg AdOH
Method of monitoring	Adipic acid production, nitric acid consumption and physical losses
Recording frequency	Yearly

Calculation method	The N <sub>2</sub> O emission factor is then calculated over the period on one year using the last rolling year data (AM0021/version 1 equation (4)):
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$$N_2O\_AdOH = HNO_3\_chemical / P\_AdOH / 63 / 2 \times 0.96 \times 44$$

The calculated value for this period is above 0.270 and is then capped by the value of KE\_N<sub>2</sub>O = 0.27, as specified in the PDD table D.2.1.3 and required by the methodology AM0021/version 1 referring to the IPCC Good Practice Guidance.

Period	Value N <sub>2</sub> O_AdOH calculated kg N <sub>2</sub> O/kg AdOH	KE_N <sub>2</sub> O kg N <sub>2</sub> O/kg AdOH	N <sub>2</sub> O_AdOH kg N <sub>2</sub> O/kg AdOH
Rolling year July 15 <sup>th</sup> , 2009	0.282	0.270	0.270



## Appendix 10

Name of item	Q_N <sub>2</sub> O reg, N <sub>2</sub> O_reg / AdOH and r <sub>y</sub>
Description	Evolution of Brazilian legislation that may require limitation of N <sub>2</sub> O emissions using one of the following criteria: <ul style="list-style-type: none"> <li>- Q_N<sub>2</sub>O reg : allowed N<sub>2</sub>O emissions</li> <li>- N<sub>2</sub>O_reg / AdOH: allowed N<sub>2</sub>O emissions per kg of adipic acid produced</li> <li>- r<sub>y</sub>: share of N<sub>2</sub>O emissions required to be destroyed</li> </ul>
Value in period	not applicable
Method of monitoring	Survey
Recording frequency	When relevant
Background data	Brazilian legislation No evolution of legislation since PDD emission.

Period	Q_N <sub>2</sub> O reg kg	N <sub>2</sub> O_reg / AdOH kg	r <sub>y</sub> %
June 25 <sup>th</sup> – July 15 <sup>th</sup> , 2009	No limit	No limit	0

Note: Rhodia follows the evolution of Brazilian legislation about N<sub>2</sub>O emissions that could affect the project Emission Reduction through the parameters N<sub>2</sub>O\_reg / AdOH, Q\_N<sub>2</sub>O reg, or r<sub>y</sub> as part of the ISO 14000 requirements.

Rhodia has hired an external company specialized in regulations. It sends to GSIMAP (Rhodia Industrial Platform) all the changes in regulations that may impact Rhodia. GSIMAP team evaluates the changes and discusses the applicability to the Rhodia operations in a steering committee. The conclusions from this steering committee are then presented to the Quality representatives of all plant units in a formal meeting that happens every three months. Furthermore GSIMAP experts on environmental issues participate on meetings held on external organizations (such as ABIQUIM - Brazilian Association of Chemical Industries, CETESB - local environmental agency) that discuss draft regulations. Those experts know in advance what comes next in terms of environmental laws.



## **Appendix 11**

Name of item

P\_N<sub>2</sub>O

Description

Market price of N<sub>2</sub>O in waste gas

Value in period

0 €/t
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Method of monitoring

Market survey

Recording frequency

Yearly

Background data

No market for this low level of N<sub>2</sub>O concentration

Beside the very high investment cost in a purification-concentration-liquefaction unit to extract the N<sub>2</sub>O from the exhaust flow of the adipic acid plant, neither the process as the product will get the necessary certifications for the pharmaceutical and food markets.

As pharmaceutical and food markets are the largest of the N<sub>2</sub>O usages we can conclude that there is no N<sub>2</sub>O market for the N<sub>2</sub>O produced as by-product of adipic acid.

Year	P_N <sub>2</sub> O
2009	0



## **Appendix 12**

Name of item	Q_Steam_p
Description	Amount of steam produced by the decomposition facility
Value in period	5 455 200 kg
Method of monitoring	Flowmeter
Recording frequency	Monthly
Background data	Log sheet record

Period	Q_Steam_p Kg
June 25 <sup>th</sup> – June 30 <sup>th</sup> , 2009	1 402 600
July 1 <sup>st</sup> – July 15 <sup>th</sup> , 2009	4 052 600



### **Appendix 13**

Name of item	E_Steam
Description	CO <sub>2</sub> emission factor for steam produced by the facility
Value in period	0.145 kg CO <sub>2</sub> /kg of steam
Method of monitoring	Supplier data
Recording frequency	Yearly
Background data	Data supplied by the Rhodia Paulínia Industrial Platform
Calculation method	<p>Calculation is made according to the monitoring plan, section 6.3.</p> <p>We first calculate the amount of natural gas required to generate steam in Nm<sup>3</sup>/t of steam in a very efficient boiler</p> $QNG\_steam = \Delta H \text{ (kJ/t)} / (\text{LHV (kJ/Nm}^3\text{)} \times \eta \text{ (\%)})$ <p>The LHV data is the yearly average value for the gas supplied by COMGAS.</p> <p>E_NG<sub>y</sub> is the yearly average value for the gas supplied by COMGAS (see appendix 5).</p> <p>The yearly value of E_Steam is calculated with the data available for the year prior to the beginning of the period in order to assure to have the data.</p>
Comment	LHV data is supplied by COMGAS in kcal/m <sup>3</sup> at 20 °C. Data were converted to kJ/Nm <sup>3</sup> .

Year ending	LHV kJ/Nm <sup>3</sup>	$\Delta H$ kJ/t	$\eta$ %	QNG_tsteam Nm <sup>3</sup> /t of steam	E_NG <sub>y</sub> kg- CO <sub>2</sub> /Nm <sup>3</sup>	E_Steam kg-CO <sub>2</sub> / kg of steam
June 24 <sup>th</sup> , 2009	38 731	2624000	97	65.72	2.211	0.145



#### **Appendix 14**

Name of item	Q_Power
Description	Electricity consumption by the decomposition facility
Value in period	25 451 kWh
Method of monitoring	Power consumption data
Recording frequency	Monthly
Background data	Log sheet record / counter

Period	Q_Power kWh
June 25 <sup>th</sup> – June 30 <sup>th</sup> , 2009	7 398
July 1 <sup>st</sup> – July 15 <sup>th</sup> , 2009	18 053



## Appendix 15

Name of item	E_Power
Description	CO <sub>2</sub> intensity for electric generation
Value in period	1.095 kg CO <sub>2</sub> /kWh
Method of monitoring	Survey of data publication
Recording frequency	Yearly
Background data	Latest data made publicly available by the Brazilian Operador Nacional do Sistema Elétrico, ONS, are for 2007.

[http://www.ons.com.br/biblioteca\\_virtual/publicacoes\\_operacao\\_sin.aspx](http://www.ons.com.br/biblioteca_virtual/publicacoes_operacao_sin.aspx)

[http://www.mme.gov.br/site/menu/select\\_main\\_menu\\_item.do?channelId=1432&pageId=4124](http://www.mme.gov.br/site/menu/select_main_menu_item.do?channelId=1432&pageId=4124)

Calculation method	<p>Calculated according to the PDD monitoring plan based on ACM0002 version 2. E_Power is calculated by taking into account only the emission factors of the fossil-fuel electricity generation (simple OM). As explained in the PDD Monitoring Plan, ONS still does not supply the plant-specific data required for BM (build margin) calculation. This is a very conservative approach since only 4% of the total electricity supplied to the grid is generated using fossil fuels (96% of Hydro and Nuclear).</p> <p>The detailed calculation is available in the Excel file “Workbook ER Paulínia” of this period (in the worksheet “E_Power”) which is a confidential document communicated to the DOE and to the CDM Executive Board. The data and the calculations were verified by the DOE prior to their utilization.</p>
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Date (year)	E_Power kg CO <sub>2</sub> /kWh
2009	1.095





## **Appendix 16**

Name of item

Q\_Steam\_c

Description

Amount of steam consumed by the decomposition facility

Value in period

18 000 kg

Method of monitoring

Mass flowmeter

Recording frequency

Monthly

Background data

Log sheet record

Period	Q_Steam_c Kg
June 25 <sup>th</sup> – June 30 <sup>th</sup> , 2009	5 200
July 1 <sup>st</sup> – July 15 <sup>th</sup> , 2009	12 800



## Appendix 17

Name of item	E_Steam_c
Description	CO <sub>2</sub> intensity for steam consumed in the facility
Value in period	0.214 kg CO <sub>2</sub> /kg of steam
Method of monitoring	Calculated from steam supplier data
Recording frequency	Yearly
Background data	Data supplied by the Rhodia Paulínia Industrial Platform
Calculation method	<p>This steam is supplied by existing boilers on site. Steam production, natural gas, fuel oil and by-products consumptions are monitored. From the monthly consumption of all fuels, the monthly value of E_NG and of the carbon content of each liquid fuel, monthly emissions of CO<sub>2</sub> for steam production are calculated and cumulated over the year. E_Steam_c is obtained from the ratio of yearly CO<sub>2</sub> emission over the yearly steam production.</p> <p>According to the PDD we calculate E_steam_c as a weighted average of the coefficients E_steam_c_NG (emission factor of steam produced by the boilers running on natural gas) and E_steam_c_chem&amp;oil (emission factor of the steam produced by the boilers running on by-products and fuel oil) with the real share of the steam generated with each type of fuel.</p> $E\_steam\_c = E\_steam\_c\_NG \times \%\_gen\_NG + E\_steam\_c\_chem\&oil \times \%\_gen\_chem\&oil$ <p>where <math>\%\_gen\_chem\&amp;oil = 100\% - \%gen\_NG</math></p> <p>The yearly value of E_Steam_c is calculated with the data available for the year prior to the beginning of the period in order to assure to have the data.</p>

Year ending	E_Steam_c_NG kg CO <sub>2</sub> /kg of steam	E_Steam_c_chem&oil kg CO <sub>2</sub> /kg of steam	%_gen_NG Share of steam generated using natural gas	E_Steam_c kg CO <sub>2</sub> / kg of steam
Jun 24 <sup>th</sup> , 2009	0.211	0.258	93.6	0.214

# Appendix 18 INSTRUMENT CALIBRATION & MAINTENANCE STATUS (see remarks in the Workbook ER Paulinia, sheet Cal\_Maint)

Related PDD parameter	Description	Tag Number	Parameter in PDD	Period	Done by	2008												2009											
						1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	4	5	6	7	8	9	10	11	12
P_AdOH	Packaging machine 25 kg	Z-3110	Dry AA (P_AdOH)	1/month	Third party	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
P_AdOH	Packaging machine 25 kg	G-2532	Dry AA (P_AdOH)	1/month	Third party	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
P_AdOH	Weigh scale 1000 kg	Z-3120	Dry AA (P_AdOH)	4/year	Third party	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
P_AdOH	Trucks weigh scale	BB-0090	N-salt production (P_AdOH)	2/year	Third party	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
P_AdOH	Trucks weigh scale	BB-0335	N-salt production (P_AdOH)	2/year	Third party	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
P_AdOH	Level of tank R-5300	LT-4500	N-salt production (P_AdOH)	Yearly	Rhodia	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
P_AdOH	Level of tank R-5310	LT-4509	N-salt production (P_AdOH)	Yearly	Rhodia	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
P_AdOH	Refractometer	Lab equipment RFM-340	N-salt production (P_AdOH)	Weekly	Rhodia	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
P_AdOH	pH meter (PHLAC1 / PHLAC2 / PHLAC3)	Lab equipment 780	N-salt production (P_AdOH)	2/Year	Third party	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
P_AdOH	pH meter (PHLAC1 / PHLAC2 / PHLAC3)	Lab equipment 780	N-salt production (P_AdOH)	3x/Week	Rhodia	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
P_AdOH	pH meter (PHLAC1 / PHLAC2 / PHLAC3)	Lab equipment 780	N-salt production (P_AdOH)	2/year	Third party	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
HNO3_cons	Nitric acid mass flowmeter	FQ-2179	Nitric Cons	2 years	Third party	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
HNO3_cons	Fresh nitric acid conc analyzer	AI-2179	Nitric Cons	2 years	Third party	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
HNO3_physical	Flowmeter of effluent to biological WWT	FQ-2973	Nitric Loss	Yearly	Rhodia	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
HNO3_physical	Flowmeter of effluent to neutralization	FQ-2974	Nitric Loss	Yearly	Rhodia	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
HNO3_physical	Waste gas flowmeter	FQ-3450	Nitric Loss	Yearly	Rhodia	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
HNO3_physical	Nitric analyzer on effluent to neutralization	AI-2974	Nitric Loss	2/month	Rhodia	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
HNO3_physical	Nitric analyzer on effluent to neutralization	AI-2974B	For failure of AI-2974	2/month	Rhodia	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
HNO3_physical	NOx analyzer in the waste gas stream	AI-2195AB	Nitric Loss	1/month	Rhodia	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
HNO3_cons	Level of nitric acid storage tank F-1769	LI -3350	Nitric Cons (backup)	Yearly	Rhodia	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
HNO3_cons	Flowmeter of fresh nitric acid to storage	FQ-3318	Nitric Cons (backup)	Yearly	Third party	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
Q_NG	Natural gas flowmeter	FQ-3408	Project emission	2 years	Third party	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
Q_Steam_p	40 bar steam flowmeter	FQ-3470	Baseline emission	Yearly	Third party	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
Q_Steam_c	6,5 bar steam flowmeter	FQ-3409	Leakage	Yearly	Third party	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
Q_GE	Stack effluent gas flowmeter	FQ-3490	Project emission	Yearly	Third party	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
N2O_GE	Stack N2O analyzer (in-situ, laser diode)	AI-3490B	Project emission	Yearly	Rhodia	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
N2O_GE	Stack N2O analyzer (extractive, infrared)	AI-3490G	Project emission (backup)	Monthly	Rhodia	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
Q_GE, Q_steam_p	Stack O2 analyzer (in-situ, laser diode)	AI-3460	Project emission (backup), steam production (backup)	Yearly	Third party	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
Q_N2O_bypass	By-pass valve leak test	HV-3402	Project emission	Yearly	Third party	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
Q_Power	Electricity meter	JI-3461	Leakage	2 years	Third party	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
HNO3_physical	Waste gas flowmeter	FIC-3401	For failure of FQ-3450	Yearly	Rhodia	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
Q_NG	Natural gas flowmeter	FIC-3406	For failure of FQ-3408 and FQ-3460	2 years	Third party	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
Q_NG	Natural gas flowmeter	FQ-3460	For failure of FQ-3408	2 years	Third party	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
Q_Steam_p	Boiler feed water flowmeter	FQ-3410	For failure of FQ-3470	Yearly	Rhodia	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	
P_AdOH	Level of tank RE-2422	LI-2422	Inventory variation	Yearly	Rhodia	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	●	