



**CLEAN DEVELOPMENT MECHANISM
PROJECT DESIGN DOCUMENT FORM (CDM-PDD)
Version 02 - in effect as of: 1 July 2004)**

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**SECTION A. General description of project activity****A.1 Title of the project activity:**

Durban Landfill-gas-to-electricity project – Mariannhill and La Mercy Landfills

Version 14/05/2013

The changes made to this version 14/05/2013 of the PDD, compared to version 05/03/2012 and to the registered project design document version 04/05/2006, are related to a typo in the accuracy of WIKA temperature transmitters. As per manufacturer specifications, the correct accuracy is 0.75%.

The changes made to version 05/03/2012 of the PDD compared to the registered project design document, version 04/05/2006 are related to the updating of the PDD according to EB48 Annex 66 and 67, and revision of the Monitoring Plan as per EB49 Annex 28, along with clarification guidance on paragraph 66 of EB59 and paragraphs 35 and 72 of EB65. The changes neither affect the additionality of the project, nor its contribution to sustainable development, the accuracy and completeness in the monitoring and verification process, or the emission reduction calculations as described further on in the revised sections below.

Additionally it takes into account the guidance from the CDM EB, on the request for deviation¹ for the first monitored period accepted in July 2007 and the guidance from the meth panel on the request for clarification for the project discussed at EB42²

A.2. Description of the project activity:

The project consists in an enhanced collection of landfill gas at two landfill sites of the municipality of Durban and the use of the recovered gas to produce electricity. The produced electricity will be fed into the municipal grid and replace electricity that the municipal electric company is currently buying from other suppliers. The project will be implemented on the Mariannhill and the La Mercy landfill sites.

The Mariannhill landfill is an active landfill site where waste will be deposited until 2024. It extends over 49 ha and receives 550 to 700 tonnes of waste per day. To date, the site has received approximately 850,000 tonnes. The Mariannhill landfill was officially designated a Nature Conservancy site in late 2002. It is the only landfill in South Africa granted such a status.

The second landfill site, La Mercy, is an old landfill, already closed and far away from residential areas. It used to receive 350 tonnes of waste per day and has about 1 Million. tonnes of waste in place.

The proposed project will newly implement landfill gas recovery at La Mercy and substantially upgrade the collection system at Mariannhill where 6 wells have been installed as a pilot activity. The project will also install 0.5 MW of electricity generation at each site for export to the municipal grid. After successful

¹ I-DEV0082 “Deviation of registered PDD and approved methodology AM0010 version 01” submitted by JCI on 27 March 2007 and EB guidance found online at <http://cdm.unfccc.int/Projects/deviations/96737>

² Request for clarification AM_CLA_0100 found online at <http://cdm.unfccc.int/methodologies/PAmethodologies/clarifications/42698>



installation and depending on gas availability, electric generation may be subsequently augmented to up to 2MW of combined capacity.

With regard to the local environment the project has positive effects on air and groundwater quality. By displacing electricity from the grid the project reduces emissions related to coal-fired power production which include sulphur oxides, nitrogen oxides, and particulates. It also reduces the adverse impacts related to transportation of coal and coal mining (dust and acid mine drainage). Near the landfill sites the project improves the air quality by further reducing the amount of landfill gas released into the atmosphere and thus reducing the risk of exposure of neighbouring residents to odour.

With regard to local employment the project will result in a small increase in the area of skilled jobs for operation and maintenance of the equipment.

Since the registration of the project, the Mariannhill site has installed a 1MW electricity generation capacity instead of the initially planned 0.5 MW that was described on the registered version of the PDD; while the La Mercy landfill site, due to operational difficulties, was decommissioned in June 2009. These changes have left only the Mariannhill landfill site operational, as per the description of the registered PDD version 2006-05-04, and therefore led to the revision of the current version of the PDD.

The removal of the La Mercy site and the change of the capacity installed at Mariannhill have led to a revision of expected emission reductions, as of the 23 of June 2009 since no ERs will be claimed from the La Mercy site after that date. The additional analysis follows in the sections below.

A.3. Project participants:

Name of Party involved ((host) indicates a host Party)	Private and/or public entity(ies) project participants (as applicable)	Kindly indicate if the Party involved wishes to be considered as project participant (Yes/No)
Republic of South Africa (host)	- Durban Solid Waste (DSW), project developer and operator - eThekweni municipality, formerly known as Durban, project sponsor	No
The State of the Netherlands	International Bank for Reconstruction and Development as the Trustee of the Prototype Carbon Fund (PCF)	Yes

Please see Annex 1 for contact details.

Official contact for the CDM project activity is the PCF.

A.4. Technical description of the project activity:

**A.4.1. Location of the project activity:****A.4.1.1. Host Party(ies):**

Republic of South Africa

A.4.1.2. Region/State/Province etc.:

KwaZulu Natal, South Africa

A.4.1.3. City/Town/Community etc:

Municipality of eThekweni, formerly known as Durban

A.4.1.4. Detail of physical location, including information allowing the unique identification of this project activity (maximum one page):

The La Mercy site is situated 35 km north of Durban, away from residential areas.

The Mariannhill landfill site is located in the western area of the Durban unicity around 20 km to the west of Durban in the Metro area formerly called the Inner West City Council (IWCC).

Durban is geographically located in the southeast region of South Africa on the Indian Ocean coast.

A.4.2. Category(ies) of project activity:

Sectoral Scope 13: Waste Handling and Disposal
Sectoral Scope 1: Renewable Energy

A.4.3. Technology to be employed by the project activity:

Durban Solid Waste (DSW) is the municipal agency responsible for management and operation of multiple landfills in the Durban metropolitan area. Under the proposed project, DSW will commission the installation of landfill gas extraction wells, flare units and landfill gas generators for the Mariannhill and La Mercy landfill sites. DSW will function as the technical advisor and operator of the project.

Specifically, the following technology will be installed:

- *Extraction wells*: Some 51 vertically driven gas wells (33 on Mariannhill and 18 on La Mercy) will be constructed during phased restoration of the site to extract the landfill gas as it is produced.
- *Gas collection pipework*: These pipes collect and transport the gas from the wells to the extraction plant from where the gas will be used for electricity generation, with any surplus gas being flared.
- *Gas extraction plant (blower)*: A centrifugal blower is required to extract landfill gas from the wells and supply this to either the generation engines or the flare unit. The blower creates lower pressure inside the wells than in the landfill, thereby sucking the gas from the landfill into the wells and from there to the extraction plant.
- *Flare units*: A landfill gas flare with minimum capacity of 1,000Nm³/hr will be installed at each site



- *Landfill gas generators:* A single 1MW unit will be installed (phase 1) which can be turned down to as low as 50% capacity (Jenbacher type 320 engine). Gas supply for phase 2 will be assessed at a later date;
- *Switch gears, transformers and cabling:* as needed for the interconnection with the eThekweni Electricity grid

The initially registered PDD included a description of the project activity that was designed assuming no technical problems would be encountered in the extraction of the gas. In practice it proved to be impossible to extract sufficient and sustained volumes of landfill gas from the La Mercy site to operate the engine (where the practical effect was that the project entity was not able to make the engine operational at the La Mercy site), and the same situation was observed for the flare.

Due to these operational difficulties, a site investigation was carried out by an experienced consulting firm³, after the construction and commissioning of the gas management system at La Mercy, which confirmed that the site suffers from high levels of leachate within the waste, and also a significant quantity of fine Red Berea Sand which had been used as daily cover material when the landfill was operational. The combined effect of the sand and the leachate was to effectively block up the landfill gas extraction wells, preventing the engine and flare from operating.

The site therefore presents serious technical difficulties which prevent the collection system from operating as designed. As a result, the decision was taken to remove the engine and flare infrastructure in June 2009. Consequently, no emission reductions will be claimed for the La Mercy site from the 23 of June 2009 onwards.

Additionally, at the Marinahill site a 1 MW engine was installed, which has also been taken into account in this revised version of the PDD.

A.4.4. Brief explanation of how the anthropogenic emissions of anthropogenic greenhouse gas (GHGs) by sources are to be reduced by the proposed CDM project activity, including why the emission reductions would not occur in the absence of the proposed project activity, taking into account national and/or sectoral policies and circumstances:

This project is composed of two complementary components as follows:

- Collection, flaring, and combustion of landfill gas, thus converting its methane content into CO₂ and reducing its greenhouse gas effect; and,
- Generation and supply of electricity to the regional grid, thus displacing electricity generation from thermal (mainly coal) power plants.

The baseline scenario is defined as the most likely future scenario. Establishing the most likely future scenario requires an analysis and comparison of possible future scenarios using a baseline methodology that is justifiable and appropriate given the project circumstances. Based on this analysis (see sections B.2. and B.3. below), the most likely baseline scenario is expected to be a continuation of the current business-as-usual (BAU) situation where the Mariannhill landfill collects and flares a minimum portion of the generated methane, while La Mercy landfill continues passive venting solely in order to ensure that the landfill gas concentration remains below hazardous levels. It is not likely that economic, technical,

³ Report from this site investigation by SLR Consulting, carried out the 19th of September 2007 has been made available to the Verifier



regulatory, or other types of incentives that could significantly change the current practice will develop in the foreseeable future.

The primary purpose of the project is electricity generation and it is characterized as a municipal auto-generation project. The project is additional because it will generate emission reductions that would not occur otherwise, since the project does not present an economically attractive investment opportunity. As energy generation by the proposed project is more costly than the continued purchase of electricity from the national utility company, Eskom, the project sponsor would not invest in the project in the absence of carbon finance.

It is estimated that the project will reduce an aggregated 403,407 tons of CO₂ in the first 7 year crediting period.

A.4.4.1. Estimated amount of emission reductions over the chosen crediting period:

Years*	Annual estimation of emission reductions in tonnes of CO ₂ e
2006	56,731
2007	71,671
2008	71,478
2009	66,136
2010	47,315
2011	45,711
2012	44,367
Total estimated reductions (tonnes of CO₂e)	403,407
Total number of crediting years (First crediting period)	7
Annual average over the crediting period of estimated reductions (tonnes of CO₂e)	57,630

*as the starting date of the project activity is 1 July 2006, the years cover the period from 1 July to 30 June of the following year.

*Since the project registration date was 15th December 2006, the years cover the period from 15th December to 14th December of the following year.

A.4.5. Public funding of the project activity:

This project will not be funded by international Official Development Assistance (ODA) or other sources earmarked for development assistance.

SECTION B. Application of a baseline methodology

**B.1. Title and reference of the approved baseline methodology applied to the project activity:**

Approved baseline methodology AM0010: “Landfill gas capture and electricity generation projects where landfill gas capture is not mandated by law”

B.1.1. Justification of the choice of the methodology and why it is applicable to the project activity:

The selected baseline methodology has been developed in the context of this project.

The project meets the application criteria that have been specified for the use of this methodology, namely:

- The landfill is subject to regulation of methane (CH₄) concentration but landfill gas capture is not mandated by law
- The captured gas is used to generate electricity and the CO₂ emissions intensity of this electricity is lower than the emissions intensity of the electricity displaced; and
- The electricity generation capacity of the project does not exceed 15MW.

B.2. Description of how the methodology is applied in the context of the project activity:**Baseline scenario**

AM0010 defines the baseline as the scenario reflecting all actions that have to be implemented in order to meet the regulations on methane concentration, as well as good management practice to address safety and odour concerns. If these actions correspond to the establishment of several “baseline” wells, the quantity of methane collected via these wells shall be monitored, and it should be demonstrated that the quantity collected is sufficient to meet the regulation on methane concentration during the entire crediting period.

In the below paragraphs, the baseline scenario for the Mariannhill and La Mercy landfills is determined following the four steps outlined in AM0010.

Step 1: Provide a convincing justification that there is no plausible baseline scenario except the project and the business as usual (BAU) scenario. If there is another plausible baseline scenario, this methodology cannot be used for the proposed project activity. The justification of the baseline scenario shall take into account whether national or local regulations require capture of landfill gas.

For Durban, several scenarios have been identified as possible future developments, namely:

- (a) Business-as-usual (BAU): Currently, neither landfill has an active landfill gas collection and utilization system in place. Landfill gas is currently vented to ensure that the concentration of methane in any particular area of the landfill stays below hazardous levels. In the past, 6 collection wells were installed on the Mariannhill landfill as a pilot to investigate the feasibility of landfill gas recovery for electricity generation. However, as it turned out that this option was uneconomical, DSW has abandoned all further activities. The BAU scenario is the continuation of passive venting at both sites and the operation of 6 test wells with declining efficiency
- (b) The proposed project: collection of most landfill gas, its use for municipal power generation on the landfill site, and an equivalent reduction in power purchases from Eskom.



(c) Collection and flaring of most of the landfill gas without use of the gas for power generation.

Existing landfilling capacity, cost considerations and regulatory requirements governing waste management were identified as the key factors that influence the realization of the above scenarios. Based on these factors, scenario (c) was rejected as an implausible baseline alternative.

Currently no collection and flaring are required by South Africa's waste management regulations. The installation of a gas collection and flaring system in excess of current practice and legal requirements would result in unnecessary costs without associated income (or cost savings) to offset these costs.

The South African Department of Water Affairs & Forestry (DWAF) requires all landfill operators to monitor CO₂ and CH₄ concentrations. The DWAF specifies the requirements for landfill operators as follows:

"The Permit Holder shall implement adequate measures to the satisfaction of the Regional Director, to ventilate or to prevent lateral migration of CH₄ gas generated in the site so that build up of dangerous concentrations is prevented. The concentration of flammable gas outside the waste disposal area and inside the Site shall not exceed 1% by volume in air and the concentration of CO₂ should not exceed 0.5% by volume in air, amended for Standard Temperature and Pressure." (from Landfill Permit Requirements)

The minimum requirements for waste disposal by landfill in South Africa include gas monitoring at all hazardous and large landfills, reporting to the department if the concentration of soil gas exceeds 1%, and permanent venting systems if the methane concentration exceeds 5% in air (per Minimum Requirements for Waste Disposal by Landfill, Second Edition 1998.)

In the past, the environmental standards for landfills have been tightened on average every four years with the last revision dating back to 1998. New Revised DWAF Minimum Requirements were issued on 21st October 2005. The revised DWAF requirements do not require gas capture and flaring from permit holders, given the high costs that such a requirement would incur on landfill operators. The Bisasar Road, the Mariannhill and the Durban Bulbul Drive landfills are currently the only landfill sites in South Africa which have installed limited gas flaring systems. Rather, ongoing discussions indicate that the upcoming revision of the permit requirements will loosen the acceptable standard for CO₂ concentration.

Both landfills are operating in compliance with the mandatory requirements. In the absence of further regulatory or economic incentives to collect and destroy landfill gas, the plausible baseline alternatives are reduced to the project and the BAU scenario.

Step 2: Calculate the cost of a kWh of electricity generated by the project using conservative assumptions. The calculation must include the incremental investment cost, the operations and maintenance costs, and all other costs of upgrading the BAU scenario to the proposed project activity. Assumptions are conservative if they tend to reduce the cost of the electricity generated. Conservatism of the assumptions should be ensured by obtaining expert opinions and by the Operational Entity validating the project.

The expected cost of electricity generation by the project is calculated at US\$ 0.0422 per kWh.

Details to the calculation are provided in Annex 3 (Baseline Information).

After the decommissioning of the La Mercy site, and as per the guidelines on EB48, Annex 66 and 67, a conservative reassessment was done for the expected cost of electricity generation only by the Mariannhill landfill site. Under this consideration two analyses were made: 1-Isolating Mariannhill site under exactly



the same assumptions as the original analysis, and 2-Isolating Mariannhill site and updating the actual energy generation capacity installed and the number of wells.

The result under both analyses is: 1-US\$ 0.0476 per kWh and US\$ 0.0377 per kWh respectively. Details to the calculation are also provided in Annex 3.

Step 3: Determine the long run marginal cost (LRMC) of continued electricity generation by the grid. The LRMC is expressed as a cost per kWh. To be conservative, assumptions used to calculate the LRMC should increase the cost per kWh.

Until the end of the project's first crediting period in 2012, the LRMC of electricity generation by the grid are conservatively estimated at US\$ 0.0225 per kWh. Over the project lifetime, the LRMC are expected not to exceed US\$ 0.0365 per kWh.

Details to the calculation are provided in Annex 3 (Baseline Information).

Step 4: Demonstrate that the cost of the electricity generated by the project (*Step 2*) is higher than the LRMC (*Step 3*). If that is the case, it can be assumed that generation by the grid (the baseline scenario) is financially more attractive than generation by the project and that the project is additional.

Based on current low power purchase prices and using the equally low LRMC for power production in South Africa as an approximation of future electricity prices charged to communities, it is concluded that, from an investment point of view, the auto-generation option using the landfill gas is not an economically attractive course of action for the municipality now or in any foreseeable future. The same holds true for the analysis carried out after the decommissioning of the La Mercy site, and with the current configuration of the Mariannhill site up to 2011; the same will also hold true with further installation of wells, as the project will become even less economically attractive.

The baseline scenario, as determined above, is the continuation of the current practice of limited collection and flaring of methane from the landfills in compliance with applicable regulations. Given the long-run calculation performed in the baseline study, the BAU baseline is likely to be valid for the duration of the 21-year crediting period selected for this project. However, the BAU baseline includes the possibility that future South African waste management regulations will require the treatment of landfill gas, in which case the baseline scenario would have to reflect such new obligations. The baseline scenario therefore incorporates regulatory changes that would require a change in the current, business-as-usual operation of the landfill sites. The project will monitor any regulatory changes that impact waste management in South Africa and will adjust the baseline scenario by re-designating some landfill gas project wells to baseline wells.

Emission reductions

According to AM0010, the greenhouse gas emission reduction achieved by the project activity during a given year (ER_y) is the difference between the amount of methane actually destroyed during the year ($MD_{project_y}$) and the amount of methane that would have been destroyed during the year in the absence of the project activity ($MD_{baseline_y}$), times the approved Global Warming Potential value for methane (GWP_{CH_4}) plus the quantity of net electricity sold to the grid during the year (ES_y) multiplied by the CO_2 emissions intensity of the electricity displaced (EI_{grid_y}).



$$ER_y = (MD_{project_y} - MD_{baseline_y}) \times GWP_{CH_4} + ES_y \times EI_{grid_y}$$

Where:

ER_y are the emission reductions in a year (tCO₂e/year).

$MD_{project_y}$ is the methane destroyed in a year (tCH₄/year).

$MD_{baseline_y}$ is the methane that would have been destroyed during a year in the absence of the project (tCH₄/year).

GWP is the approved Global Warming Potential for methane (21 tCO₂e/tCH₄)

ES_y is the quantity of net electricity sold to the grid (MWh).

EI_{grid_y} is the CO₂ emissions intensity of the grid (tCO₂e/MWh).

Grid emission factor

In compliance with approved baseline methodology AM0010, the CO₂ emission intensity of the grid is calculated as the average annual CO₂ emission intensity of the grid, which is obtained from the grid operator. The use of an average annual emission rate for grid electricity is justified if it is determined in a conservative manner, i.e. it is very unlikely to overstate the emission reductions.

For this project, the grid emission rate is determined using Eskom's reported data for annual CO₂ emissions and power output. This method averages the coal-fired power plants and other less carbon-intensive power sources in South Africa.

In its 2003 Annual Report (published in 2004) Eskom publicly reported that it emitted 0.895978 kg of CO₂ per kWh of electricity produced. To calculate the emission reduction from displacement of grid electricity by the project, the project's annual power sales (in kWh) will be multiplied with the annual average emission rate for that year (as derived from Eskom's annual reports).

This methodology is adequate because it is highly improbable that the project will significantly affect the dispatch of peak load plants, but will primarily displace electricity from base load suppliers. Due to overcapacity in South Africa, peak load plants are mainly used as "shock absorbers". Because of the project's character as must-run-capacity and its very small contribution to meet the overall Durban metro-area demand, it is expected that Eskom will reduce the generation of the base load power plant with the highest marginal costs in its regional supply mix to adjust for a reduced power purchase by eThekweni Electricity.

The methodology for the calculation of the emission factor is conservative for the following reasons:

- Averaging the emissions across all Eskom power plants includes the low emission intensity of more efficient coal-fired plants. The project however displaces the plant with highest marginal costs in its territory and hence is likely to displace the least efficient and most emission intensive coal power plant in that region.
- Being located close to the Durban municipality, the project feeds electricity directly into the low voltage municipal grid. Most of Durban's electricity is supplied from the high voltage system. By displacing electricity from the high voltage system the project also reduces the amount of transmission losses that occur over longer distances and at the substations where the voltages are reduced.
- The emissions from the Eskom power stations' parasitic load are not included in the Eskom data and are therefore not included in the emission rate.

**B.3. Description of how the anthropogenic emissions of GHG by sources are reduced below those that would have occurred in the absence of the registered CDM project activity:**

The baseline is defined as the scenario, in which the currently existing wells continue to operate with a declining efficiency, but no further wells would be installed, unless national legislation tightens. The proposed project is additional because it reduces emissions relative to the projected emission level in the baseline scenario.

In the absence of the project, only about 7.4% of the gas produced in the landfills would be collected and flared. The project upgrades the methane recovery system to 83% in 2012, and thereafter progressively dropping in parallel to diminishing gas production to 44.3% in 2025 at the probable end of the commercial project life. In addition, the displacement of mainly coal-based electricity with renewable energy from landfill gas would not take place in the absence of the CDM activity.

B.4. Description of how the definition of the project boundary related to the baseline methodology selected is applied to the project activity:

The boundary of the project is the site of the project activity where the gas is captured and destroyed, the Mariannahill and the La Mercy landfill sites.

After the changes of the PDD, the project boundary is the site of the project activity where the gas is captured and destroyed, that is the Mariannahill landfill site.

B.5. Details of baseline information, including the date of completion of the baseline study and the name of person (s)/entity (ies) determining the baseline:

Sandra Greiner/Robert Chronowski/Johannes Heister/Noreen Beg

Carbon Finance Business
World Bank
1818 H Street, NW
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nbeg@worldbank.org

Completion date: 2006-04-11

The revision of the baseline information has been completed by 01/04/2011 by

Claudia Barrera



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SECTION C. Duration of the project activity / Crediting period**C.1 Duration of the project activity:****C.1.1. Starting date of the project activity:**

1st February 2006

C.1.2. Expected operational lifetime of the project activity:

21 years

C.2 Choice of the crediting period and related information:**C.2.1. Renewable crediting period**

Chosen

C.2.1.1. Starting date of the first crediting period:

1st July 2006

**C.2.1.2. Length of the first crediting period:**

7 years

C.2.2. Fixed crediting period:

Not chosen

C.2.2.1. Starting date:

Not applicable

C.2.2.2. Length:

Not applicable

SECTION D. Application of a monitoring methodology and plan**D.1. Name and reference of approved monitoring methodology applied to the project activity:**

Approved baseline methodology AM0010: "Landfill gas capture and electricity generation projects where landfill gas capture is not mandated by law"

D.2. Justification of the choice of the methodology and why it is applicable to the project activity:

The selected methodology has been developed in the context of this activity.

1) For a landfill methane gas capture project such as the Durban Landfill-gas-to-electricity project it is adequate and most accurate to directly measure the methane combusted in flares and generators, i.e. the emission reductions attributable to the project. Each ton of methane collected and destroyed equals one ton of methane not released to the atmosphere and, thus, one ton of methane emissions reduced. Emission reductions do not have to be established through a comparison between baseline and project emissions and, as a consequence, the quantity of emissions in the baseline scenario can remain unknown.

2) The greenhouse gas emissions achieved through displacement of grid electricity can be estimated by multiplying the amount of net sold electricity (kWh) injected into the grid by an appropriately conservative carbon emission factor for the South African grid, measured as kgCO₂/kWh. This methodology has low transaction costs as it only involves computations based on data that are routinely collected by the project operator.

**D.2. 1. Option 1: Monitoring of the emissions in the project scenario and the baseline scenario**

Not applicable, because the project directly monitors and calculates emission reductions.

D.2.1.1. Data to be collected in order to monitor emissions from the project activity, and how this data will be archived:

ID number (Please use numbers to ease cross-referencing to D.3)	Data variable	Source of data	Data unit	Measured (m), calculated (c) or estimated (e)	Recording frequency	Proportion of data to be monitored	How will the data be archived? (electronic/paper)	Comment

D.2.1.2. Description of formulae used to estimate project emissions (for each gas, source, formulae/algorithm, emissions units of CO₂ equ.)

Not applicable

D.2.1.3. Relevant data necessary for determining the baseline of anthropogenic emissions by sources of GHGs within the project boundary and how such data will be collected and archived :

ID number (Please use numbers to ease cross-referencing to table D.3)	Data variable	Source of data	Data unit	Measured (m), calculated (c), estimated (e),	Recording frequency	Proportion of data to be monitored	How will the data be archived? (electronic/paper)	Comment

D.2.1.4. Description of formulae used to estimate baseline emissions (for each gas, source, formulae/algorithm, emissions units of CO₂ equ.)

Not applicable

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**D. 2.2. Option 2: Direct monitoring of emission reductions from the project activity (values should be consistent with those in section E).**

The following data will be collected in conformance with approved monitoring methodology AM0010 :

ID number	Data type	Data unit	Measured (m), calculated (c) or estimated (e)	Recording frequency	Proportion of data to be monitored	How will the data be archived? (electronic/ paper)	For how long is archived data to be kept?	Comment
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ID number	Data type	Data unit	Measured (m), calculated (c) or estimated (e)	Recording frequency	Proportion of data to be monitored	How will the data be archived? (electronic/ paper)	For how long is archived data to be kept?	Comment
1. MV baseline _y	Amount of landfill gas collected from baseline wells	m ³	m	continuous	100%	electronic	Duration of project crediting period	Measured by a flow meter. Data will be aggregated monthly and yearly. Temperature and pressure will also be measured with volume adjusted to standard temperature and pressure.
2 MVprojecty ⁴	At the Mariannhill site derived from the amount of landfill gas collected from the gas field, minus the amount of landfill gas collected from the baseline wells. At La Mercy site the amount of landfill gas collected from the gas field	m ³	m and c	continuous	100%	electronic	Duration of project crediting period	At Mariannhill measured by three flow meters. Total gas used for power generation plus gas flared (gas extracted from the field) minus gas collected from the baseline wells. At La Mercy site, measured by two flow meters. Data will be aggregated monthly and yearly. Temperature and pressure must also be measured with volume adjusted to standard temperature and pressure. In line with paragraph 35 (a) of the EB65 Meeting Report, the calculation of theoretical methane emissions using the first order decay model shall be conducted to confirm the methane calculated using the proposed approach for the parameter MVprojecty "amount of landfill gas collected from the project wells". The Calculation of the FOD model is explained in the section below this table.

⁴ Following guidance from the CDM EB after request for deviation submitted for the first monitored period and PDD submitted at the time, and also found online at <http://cdm.unfccc.int/Projects/deviations/96737>

This template shall not be altered. It shall be completed without modifying/adding headings or logo, format or font.



ID number	Data type	Data unit	Measured (m), calculated (c) or estimated (e)	Recording frequency	Proportion of data to be monitored	How will the data be archived? (electronic/ paper)	For how long is archived data to be kept?	Comment
3	Methane content of landfill gas ⁵	%	m and c	Continuous and periodic	100%	electronic	Duration of project crediting period	The monitoring of methane content combusted, and used for emission reduction calculations shall be continuous. The monitoring of the methane content in the baseline, for crosscheck purposes, shall be periodic.
4 ESy	Amount of net electricity sold to the grid	MWh	m	continuous	100%	electronic	Duration of the project crediting period	Measured by kWh meters for the imported and exported electricity. Data will be aggregated monthly and yearly.
5 EGy	Amount of electricity generated.	MWh	m	continuous	100%	electronic	Duration of the project crediting period	Measured by a kWh meter Data will be aggregated monthly and yearly
6	Combustion efficiency	%	m and c	Annual, monthly if unstable	n/a	electronic	Duration of the project crediting period	Methane content of engine/boiler exhausts gas.
7	LFG temperature and pressure	°C/Pa	m	periodic, daily	100%	electronic	Duration of the project crediting period	Device that provides data that can be used to determine the density of methane or provides for integration of measurement of temperature and pressure in order to provide a direct reading of the normalized gas flow.

⁵ Following guidance from the CDM EB after request for deviation submitted for the first monitored period and PDD submitted at the time, and also found online at <http://cdm.unfccc.int/Projects/deviations/96737>

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ID number	Data type	Data unit	Measured (m), calculated (c) or estimated (e)	Recording frequency	Proportion of data to be monitored	How will the data be archived? (electronic/paper)	For how long is archived data to be kept?	Comment
8	Flare working hours							When the flare temperature (parameter 9 below) is below 500 °C it is assumed that the flare is not operating and therefore during that time no ERs are claimed.
9	Flare temperature	°C	m	continuous	100% while flare is in operation	electronic	Duration of the project crediting period	Continuous measurement of operation hours based on measured flare temperature using a device such as a thermocouple. If there is no record of the temperature of the exhaust gas of the flare or if the recorded temperature is less than 500 °C for any particular hour, it shall be assumed that during that hour the flare efficiency is zero
10 HRy	Heat rate of the generator	Gj/MWh	m and c	Annual, monthly if unstable	N/A	electronic	Duration of crediting period	Data will be used to test and if necessary, correct the generator's name plate heat rate.
11 Wx	Total amount of waste disposed in year x	ton	m	Daily, aggregated monthly	100%	electronic	Duration of crediting period	Data will be used to conduct the calculation of the theoretical amount of methane generated from disposal of waste at the SWDS, as per the FOD model explained below. Data to be measured by a calibrated weighbridge as per the South African Metrology Act of 1973 requirements



ID number	Data type	Data unit	Measured (m), calculated (c) or estimated (e)	Recording frequency	Proportion of data to be monitored	How will the data be archived? (electronic/ paper)	For how long is archived data to be kept?	Comment
12. W _{j,x}	Amount of solid waste type <i>j</i> disposed or prevented from disposal in the SWDS in the year <i>x</i>	ton	m	Daily, aggregated monthly	100%	electronic	Duration of crediting period	Data will be used to conduct the annual calculation of the theoretical amount of methane generated from disposal of waste at the SWDS, as per the FOD model explained below. Data to be measured by a calibrated weighbridge as per the South African Metrology Act of 1973 requirements.
13. p _{j,x}	Waste composition in the year	%	c	annually	Calculated based on 100% monitored data	electronic	Duration of crediting period	Calculated based on parameters W _x and W _{j,x} and used as input data to the FOD spreadsheet model

Calculation of the First Order Decay (FOD) model⁶

The theoretical amount of methane generated from disposal of waste at the SWDS is calculated based on a first order decay (FOD) model, as follows:

$$BE_{CH_4,SWDS,y} = \phi_y \cdot (1 - f_y) \cdot GWP_{CH_4} \cdot (1 - OX) \cdot \frac{16}{12} \cdot F \cdot DOC_{f,y} \cdot MCF_y \cdot \sum_{x=1}^y \sum_j W_{j,x} \cdot DOC_j \cdot e^{-k_j(y-x)} \cdot (1 - e^{-k_j})$$

Where

- BE_{CH₄,SWDS,y} = Baseline methane emissions occurring in year *y* generated from waste disposal at a SWDS during a time period ending in year *y* (t CO₂e / yr)
- x* = Year during the crediting period: *x* runs from the first year when the site started receiving waste to the year *y* for which avoided emissions are calculated (*x* = *y*)
- y* = Year of the crediting period for which methane emissions are calculated (*y* is a

⁶ Following EB65 guidance, and applying the tool to calculate “Emissions from solid waste disposal sites” EB65, Annex 19, Application A.” This template shall not be altered. It shall be completed without modifying/adding headings or logo, format or font.



	=	consecutive period of 12 months)
$DOC_{f,y}$	=	Fraction of degradable organic carbon (DOC) that decomposes under the specific conditions occurring in the SWDS for year y (weight fraction)
$W_{j,x}$	=	Amount of solid waste type j disposed or prevented from disposal in the SWDS in the year x (t)
ϕ_y	=	Model correction factor to account for model uncertainties for year y
f_y	=	Fraction of methane captured at the SWDS and flared, combusted or used in another manner that prevents the emissions of methane to the atmosphere in year y
GWP_{CH_4}	=	Global Warming Potential of methane
OX	=	Oxidation factor (reflecting the amount of methane from SWDS that is oxidised in the soil or other material covering the waste)
F	=	Fraction of methane in the SWDS gas (volume fraction)
MCF_y	=	Methane correction factor for year y
DOC_j	=	Fraction of degradable organic carbon in the waste type j (weight fraction)
k_j	=	Decay rate for the waste type j (1 / yr)
j	=	Type of residual waste or types of waste in the MSW

As indicated by the tool, for application A, the time period under which waste disposal is to be considered in the calculation may begin before the start of the project activity and typically starts when the SWDS starts receiving waste. Hence this shall be applied and values for deposited waste will be included since the start of operations.

Determining the parameters required to apply the FOD model

The table below summarizes how the parameters required by the tool have been determined

Parameter	Value Applied	Reason
ϕ_y	0.75	As per the tool, default value option for baseline emissions under Application A
OX	0.1	Default value as per the tool
F	0.5	Default value as per the tool
$DOC_{f,y}$	0.5	Default value as per the tool
MCF_y	1.0	Default values (based on SWDS type); 1.0 for anaerobic managed solid waste disposal sites.



k_j	Waste type j	DSW Waste type categories	k_j	<p>Default values (based on waste type), for for tropical (MAT > 20°C) and wet (MAP > 1000m) conditions. Source: “Durban Climate Guide to the Average Weather & Temperatures” found online at http://www.climateemp.info/south-africa/durban.html</p> <p>Last updated 22/07/2011 Last accessed 12/01/2012</p>
	Pulp, paper, cardboard and textiles	-	0,070	
	Wood, wood products and straw	-	0,035	
	Other (non-food) organic putrescible garden and park waste	03	0,170	
	Food, food waste, sewage sludge, beverages and tobacco	01, 02	0,400	
DOC_j	Waste type j	DSW Waste type categories	DOC_j (% wet waste)	Default values (based on waste type)
	Wood and wood products	-	43	
	Pulp, paper and cardboard (other than sludge)	-	40	
	Food, food waste, beverages and tobacco (other than sludge)	01,02	15	
	Textiles	-	24	
	Garden, yard and park waste	03	20	
	Glass, plastic, metal, other inert waste	04,05,06,07,08, 09, 10, 11	0	
f_y	0			Estimated once; determined as 0 because the amount of LFG that would have been captured and destroyed is already accounted for by monitored parameter $MV_{baseline_y}$

All data will be archived during the crediting period and 2 years after. For a complete list of monitoring equipment please see tables in Annex 4.

Determining the amounts of waste types j disposed in the SWDS ($W_{j,x}$)

To conduct the annual calculation of the FOD model, the amounts of disposed waste by type and total (in tons) will be monitored and used as input data to the FOD model. As per the landfill records, types of waste have been monitored under the following waste type categories:

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- 01 – Domestic Solid Waste - Refers to all domestic municipal waste streams transported by DSW vehicles
02 – General Solid Waste- Refers to all domestic private waste streams from transporters other than DSW
03 – Garden Refuse- Refers to all garden waste, including Private & Municipal
04 – Builders Rubble- Refers to construction and cover material from Private transporters
05 – Mixed Loads- Refers to industrial, builder's and/or garden refuse from Private transporters
06 – Sand and cover material
07 – Purchased cover material
08 - Tyres- Refers to whole tyres
09 – Light Refuse- Refers to 'Light solid waste (being waste with a mass of approximately 40 kg per cubic metre)' and very light solid waste (being waste with a mass of approximately 20kg per cubic metre)
10 - Other - Refers to waste stream no categorized above
11 - Recyclables -Refers to glass, bottles, cans, metals, plastics

The above categories have been identified as the following waste types for use of the FOD model:

Waste Composition	Category
Pulp, paper, Cardboard (other than Sludge)	-
Textiles	-
Food and Food Waste, beverages and tobacco (other than sludge)	1,2
Garden,Yard and Park Waste	3
Wood & Wood Products	-
Innert/Inorganic waste	4, 5, 6, 7, 8, 9, 10, 11

Hence by monitoring both total amount of waste coming in (W_x), and amount of waste by types ($W_{j,x}$) throughout the year, the fractions for the composition of waste can be calculated, and entered as input data to the FOD spreadsheet model⁷.

$$p_{j,x} = W_{j,x} / W_x$$

⁷ An example FOD spreadsheet model has been provided to the DOE to illustrate how data will be entered. This template shall not be altered. It shall be completed without modifying/adding headings or logo, format or font.

**D.2.2.1. Data to be collected in order to monitor emissions from the project activity, and how this data will be archived:**

ID number (Please use numbers to ease cross-referencing to table D.3)	Data variable	Source of data	Data unit	Measured (m), calculated (c), estimated (e),	Recording frequency	Proportion of data to be monitored	How will the data be archived? (electronic/ paper)	Comment

The project does not cause any emissions of greenhouse gases other than negligible emissions associated with the construction works and the operation of the blower.

D.2.2.2. Description of formulae used to calculate project emissions (for each gas, source, formulae/algorithm, emissions units of CO₂ equ.):

Not applicable (see D.2.2.1).

D.2.3. Treatment of leakage in the monitoring plan**D.2.3.1. If applicable, please describe the data and information that will be collected in order to monitor leakage effects of the project activity.**

ID number (Please use numbers to ease cross-referencing to table D.3)	Data variable	Source of data	Data unit	Measured (m), calculated (c) or estimated (e)	Recording frequency	Proportion of data to be monitored	How will the data be archived? (electronic/ paper)	Comment

No increase in emissions outside the project boundary – leakage – is expected as a result of the project activity.

**D.2.3.2. Description of formulae used to estimate leakage (for each gas, source, formulae/algorithm, emissions units of CO₂ equ.)**

Not applicable (see D.2.3.1)

D.2.4. Description of formulae used to estimate emission reductions for the project activity (for each gas, source, formulae/algorithm, emissions units of CO₂ equ.)

Various formulas and calculations are needed to obtain the emission reductions from the project. On an aggregate level, emission reductions are calculated according to the formula:

$$ER_y = (MD_{project_y} - MD_{baseline_y}) \times GWP_{CH_4} + ES_y \times EI_{grid_y}$$

Where:

ER_y are the emission reductions in a year (tCO₂e/year).

$MD_{project_y}$ is the methane destroyed in a year (tCH₄/year).

$MD_{baseline_y}$ is the methane that would have been destroyed during a year in the absence of the project (tCH₄/year).

GWP is the approved Global Warming Potential for methane (21 tCO₂e/tCH₄)

ES_y is the quantity of net electricity sold to the grid (MWh).

EI_{grid_y} is the CO₂ emissions intensity of the grid (tCO₂e/MWh).

Section E5 contains a comprehensive step-by-step-diagram how the variables MD_{project} and MD_{baseline} are calculated from the measurements.

In order to estimate emission reductions *ex ante*, one has to calculate the prospective methane generation of the landfill sites. The IPCC First Order Decay Model or other landfill gas models can be used to this effect. In the case of the Mariannhill and the La Mercy sites, landfill gas generation has been simulated by the UK based company Enviros Ltd using the GasSim model.

The grid emission factor of the South African grid is not calculated by the project participants but by the South African national utility company Eskom.

Furthermore, once the project is operating and directly monitoring the emission reductions, calculations are needed to translate the various data measurements into the parameter values needed in the above formula. A comprehensive description as to how the parameter values are obtained from the data measurements is provided in E5 below.

**D.3. Quality control (QC) and quality assurance (QA) procedures are being undertaken for data monitored**

Data (Indicate table and ID number e.g. 3.-1.; 3.2.)	Uncertainty level of data (High/Medium/Low)	Explain QA/QC procedures planned for these data, or why such procedures are not necessary.
D 2.2 - 1 LFGy	Low	Flow meters will be subject to a regular maintenance regime to ensure accuracy
D.2.2- 2 EGy	Low	Electricity meters will be subject to a regular maintenance and testing regime to ensure accuracy. Their reading will be checked by the electricity distribution company.
D2.2 - 10 HRy	Low	Regular maintenance will ensure optimal operation of engines and generators. The heat rate will be checked annually, with monthly checks if the heat rate shows significant deviations from previous values.

Quality assurance procedures involve calculation of theoretical methane emissions using the first order decay model to confirm the methane calculated using the proposed approach for parameter MVprojecty "amount of landfill gas collected from the project wells"⁸.

D.4 Please describe the operational and management structure that the project operator will implement in order to monitor emission reductions and any leakage effects, generated by the project activity

DSW is the project operator. To ensure effective monitoring of the emission reductions, DSW will implement a well-defined management and operational system which includes data handling, staff training, reporting and quality assurance. Specifics of the management system are provided in the annexed Monitoring Plan.

In addition, DSW and the PCF are organizing an initial verification at the start of the project activity to ensure that the monitoring system is fully functional at the onset of the project.

D.5 Name of person/entity determining the monitoring methodology:

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Completion date: 2005-09-10

⁸ As recommended by the EB65th Meeting

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The revision to the monitoring plan has been completed by 03/03/2011 by
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**SECTION E. Estimation of GHG emissions by sources****E.1. Estimate of GHG emissions by sources:**

Emission reductions are estimated directly

E.2. Estimated leakage:

Not applicable

E.3. The sum of E.1 and E.2 representing the project activity emissions:

Emission reductions are estimated directly

E.4. Estimated anthropogenic emissions by sources of greenhouse gases of the baseline:

Emission reductions are estimated directly

E.5. Difference between E.4 and E.3 representing the emission reductions of the project activity:

The greenhouse gas emission reduction achieved by the project activity during a given year (ER_y) is the difference between the amount of methane actually destroyed/combusted during the year ($MD_{projecty}$) and the amount of methane that would have been destroyed/combusted during the year in the absence of the project activity ($MD_{baseliney}$), times the approved Global Warming Potential value for methane (GWP_{CH4}) plus the quantity of net electricity sold to the grid during the year (ES_y) multiplied by the CO_2 emissions intensity of the electricity displaced (EI_{gridy}).

$$ER_y = (MD_{projecty} - MD_{baseliney}) \times GWP_{CH4} + ES_y \times EI_{gridy}$$

The monitoring plan provides for the calculation of emission reductions from avoided methane emissions and from displaced grid electricity. The calculation formulas are contained both explicit and programmed in the annexed self-calculating Excel spreadsheets. The calculations are done in the following ways (please refer to the Monitoring Plan and the spreadsheets for details):

(1) Calculation method for emission reductions from landfill gas combustion ($MD_{projecty} - MD_{baseliney}$) x GWP_{CH4} :

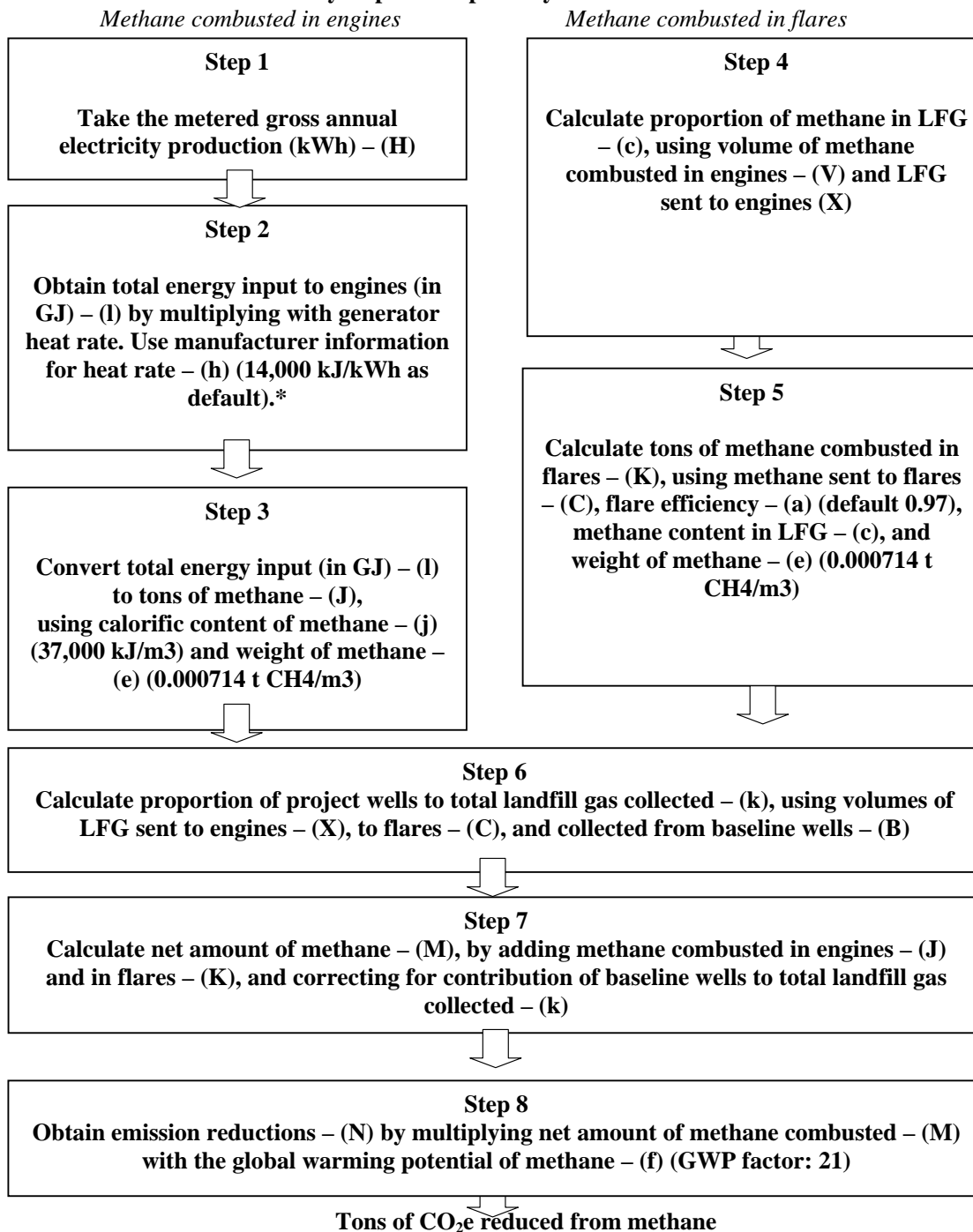
Two methods are used for the calculation of emission reduction from landfills. The first is based on down stream metering wherever possible, i.e. meters are placed as closely as possible to the location of combustion of methane gas or measure minor quantities thus avoiding sources of error. The second method relies on up-stream metering and continuous analysis of the methane content in landfill gas. This method is used as backup and for quality control purposes.

The primary method uses the monthly aggregates of the following four metered variables: Gross electricity production (kWh), volume of LFG sent to engines, volume of landfill gas flared, and volume of LFG extracted from baseline wells (all in m^3). The method first calculates the quantity of methane combusted in engines using engine kWh output and technical parameters (Steps 1 – 3 in Figure 2). Step 4 calculates the methane content in LFG using the quantity of LFG sent to engines, which is then used in Step 5 to derive methane combusted in flares from LFG quantity sent to flares. Step 6 calculates the proportion of LFG collected from project wells using the above information about LFG sent to engines



and flares as well as LFG collected from baseline wells. This proportion is used in Step 7 to calculate the net amount of methane combusted by the project activity and for which credits can be claimed. Step 8 concludes the calculation by multiplying with the global warming potential of methane.

Key steps of the primary calculation method



*Engine manufacturer to provide data on the heat rate figure for use in the calculation.

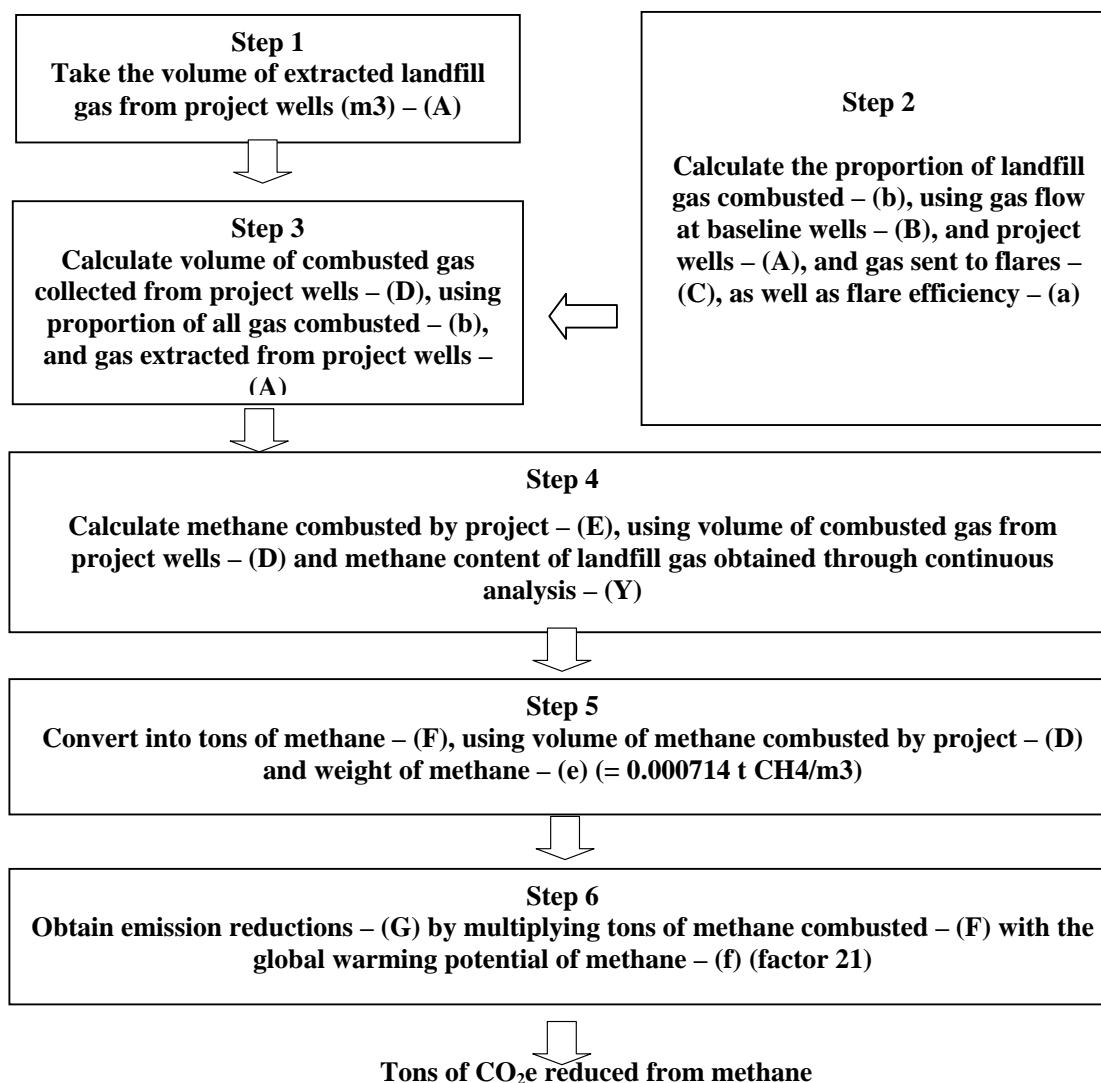


The confirmation method uses the monthly aggregates of the following three metered variables: Volume of landfill gas flared, volume of gas extracted from baseline wells, and volume of gas sent to the engines (all in m^3). The method also uses continuous analysis of the methane content in landfill gas. The method first calculates the proportion of LFG combusted using the above gas flow information together with the flare efficiency (Step 2). In Step 3, this proportion is used to derive the volume of combusted gas that is collected from project wells. Step 4 calculates the volume of methane combusted from the volume of combusted gas using continuous measurement of the methane content in LFG. Step 5 and 6 complete the calculation of emission reductions (CO_2equiv) by converting methane volume into tons of methane and multiplication with the global warming potential.

Key steps of the quality assurance method

from flow meters at project wells

*from flow meters at project wells,
baseline wells and flares*



**(2) Calculation method for emission reductions from grid electricity displacement (ESy x EIgridy):**

The project operator determines the applicable annual grid carbon emission factor based on Eskom reports and multiplies with the metered electricity delivered to the grid.

E.6. Table providing values obtained when applying formulae above:

The following projection of emission reductions is based on a variety of assumptions regarding waste volume and deposition rates, methane generation profile, LFG collection efficiency, methane content in LFG, flare efficiency, engine heat rates, and so forth. The generation of landfill gas at the two sites has been estimated by the UK based company Enviros Consulting Limited. The full report is made available to the validator.

The estimate has been updated in March 2011 due to the technical difficulties experienced at the La Mercy landfill site which led to the decommissioning of the site in June 2009, and the updated energy generation at the Mariannhill site with 1MW of installed capacity.

Emission reductions from the Mariannhill and La Mercy sites in tonnes CO₂e

Year ^a	Estimation of project activity emission reductions (tonnes of CO ₂ e) ^b	Estimation of baseline emission reductions (tonnes of CO ₂ e) ^b	Estimation of leakage (tonnes of CO ₂ e)	Estimation of emission reductions (tonnes of CO ₂ e)
2006			0	56,731
2007			0	71,671
2008			0	71,478
2009			0	66,136
2010			0	47,315
2011			0	45,711
2012			0	44,367
Total (tonnes of CO ₂ e)			0	403,408

^a As the starting date of the project activity is 1 July 2006, the years cover the period from 1 July to 30 June of the following year. However as the project registration date was 15th December 2006, the years cover the period from 15th December to 14th December of the following year.

^b Emission reductions are estimated directly; no breakdown available, see elaboration in Section E of this document.

SECTION F. Environmental impacts**F.1. Documentation on the analysis of the environmental impacts, including transboundary impacts:**

eThekwini Municipality sought legal advice and held a subsequent meeting with the competent authorities overseeing the application of ESIA legislation in KwaZulu Natal province, the conclusion of which was to confirm that a full ESIA process is required. The Bank team wished to ensure that the current ESIA team (Felehetsa Consultants) include expert and seasoned personnel regarding public consultation and conflict case mediation. The Manager of Environment for eThekwini Municipality



responded that she herself, and the Municipality more generally, would play a strong role in the preparation of the ESIA, and that other steps had been taken to ensure that such expertise was included in the ESIA team.

In order to assess the air quality impacts of the proposed landfill gas utilisation project at the Mariannhill and La Mercy Landfill sites in Durban, South Africa, Felehetsa Environmental (Pty) Ltd appointed Enviro Consulting (of the UK) on behalf of Durban Solid Waste to carry out an atmospheric dispersion modelling study of emissions from the landfill sites.

The atmospheric dispersion modelling results indicate that the predicted concentrations of the modelled substances for combustion and fugitive releases (landfill gas engines and flares), are within the relevant air quality standards.

On this basis, and despite adoption of some worst case assumptions in the modelling approach, emissions of these substances are predicted to have no significant effects on human health. Monitoring to verify the results of the modelling study is proposed.

Furthermore, utilisation of landfill gas to generate electricity, thereby displacing the use of other fuel will mean that a wider scale reduction in air pollution emissions will be achieved. This will offset the increase in combustion-related emissions associated with electricity generation. It is therefore considered that, as no air quality benchmarks are forecast to be exceeded, the use of landfill gas engines as planned comprises best practice for management of landfill gas.

F.2. If environmental impacts are considered significant by the project participants or the host Party, please provide conclusions and all references to support documentation of an environmental impact assessment undertaken in accordance with the procedures as required by the host Party:

The Durban La Mercy and Mariannhill Landfill Gas to Energy project has **positive effects on local air and groundwater quality and safety**. By displacing electricity from the grid the project reduces emissions related to coal-fired power production which include sulfur oxides, nitrogen oxides and particulates. It also reduces the adverse impacts related to transportation of coal and coal-mining (dust and acid mine drainage). Near the landfill sites the project improves local air quality by further reducing the amount of landfill gas released into the atmosphere and thus reducing the risk of dangerous methane gas concentrations and of exposure of neighboring residents to odor. This is particularly relevant for the Mariannhill landfill site which is located close to residential areas. All gas capturing wells to be installed will be equipped for leachate removal which contributes to the protection of groundwater. The provision of up to 2MW in electricity **will reduce local pollution from fossil-fuel plants**, the generation source for most electricity at present.

With regard to **local employment** the project will result in a small increase in the area of skilled jobs for operation and maintenance of the equipment at the landfill and the power generation units.

SECTION G. Stakeholders' comments

G.1. Brief description how comments by local stakeholders have been invited and compiled:

eThekweni Municipality and national legislation calls for the establishment and regular meeting of a Monitoring Committee, comprising interested and affected parties. This committee meets on a quarterly



basis. The proposed project was discussed in the Committee Meeting held in November 2002. Documentation to support this is available in the form of minutes. The environmental and social impacts of the construction and operation of the project were described.

In July 1997 the Mariannhill Landfill Site was commissioned to receive “General” (G) waste in accordance with a permit issued by the Department of Water Affairs and Forestry (DWAF, 1994 and updated 1998). The Mariannhill Landfill Monitoring Committee was formulated in 1996 and commenced meetings prior to the site opening, to ensure upon public ‘buy-in’ from the onset of disposal operations. 6 monthly audits became a legislation requirement as did regular 3-monthly meetings with the community, termed “the Monitoring Committee”.

The Monitoring Committee is a body established by all parties interested and/or affected by the landfill site which includes stakeholders, and meets on a regular basis to discuss issues related to the landfill at Mariannhill Landfill. Due to La Mercy’s isolated location in an uninhabited area no Monitoring Committee was established for this site, nor has it been called for by DWAF.

The Mariannhill Landfill Conservancy was established in 1998, and received National Conservancy Certification status in 2003.

The Mariannhill and La Mercy sites received positive Records of Decision (RODs) from the Provincial Department of Agriculture and Environmental Affairs (DAEA) on 9 July 2004, but an appeal was issued by a member of the public, Mr Allan Childs, on 2 August, 2004 (the details of which are summarised in G2). This appeal was rejected by the DAEA in early 2005, following a review period of some 5 months. However, the DAEA initially imposed conditions on this decision to reject the appeal that are detailed in G.3.

In order to assess the air quality impacts of the proposed landfill gas utilisation project at the Mariannhill and La Mercy Landfill sites in Durban, South Africa, Felehetso Environmental (Pty) Ltd appointed Enviro Consulting (of the UK) on behalf of Durban Solid Waste to carry out an atmospheric dispersion modelling study of emissions from the landfill sites.

G.2. Summary of the comments received:

Mr Allan Childs, a member of the public, submitted the following grounds for appeal against the RODs for the sites at Mariannhill and La Mercy:

a. Clauses in the Key Decision Factors of the RODs and the benefits of the projects to city residents

i. Mr Childs had no objection to the proposals overall but felt that they were aimed at increasing the prestige of the eThekweni Municipality rather than combating global warming. The benefits to residents of the city if any would be miniscule in his view. The appreciation of the Rand has already reduced the benefits by 20%.

b. Clauses related to design criteria and atmospheric impacts in the Key Decision Factors of the RODs

i. Clauses 8.6.2 and 8.6.3 of the ROD state that the spark ignition engines will be specified to the latest European design notably for exhaust emission but these actual specifications will not be finalized until the contracts are awarded. Clauses 8.8.1.2 requires an independent air monitoring exercise to be undertaken to assess the actual impact of any emissions and clause 8.8.1.3 says that the emission limits



will be set and the engines managed and monitored to ensure emission levels set (presumably as a result of the monitoring exercise) are not exceeded. Mr Childs found this to be unacceptable.

Setting the specification for exhaust based on the results of tests carried out after commissioning was equally unacceptable to Mr Childs.

Finally, he noted that there are no test facilities in South Africa for dioxin and furans. Consequently unless it is recognized that these materials could be present in the exhaust no effort will be made to test for them. He requested, therefore, that these requirements be specified in the ROD.

G.3. Report on how due account was taken of any comments received:

Based on the comments received above, and an expert analysis of the merit of those comments, the appeal submitted by Mr Childs was rejected, with the imposition of certain conditions. The projects on the Mariannhill and La Mercy landfill sites were initially granted authorization to proceed as pilot plants for a period of 2 years only.

Existing conditions of approval were amended and amplified as follows:

- The applicant (project sponsor) must undertake the air quality monitoring exercise stipulated in condition 9.2.2 of the ROD in consultation with the DAEA. The DAEA must be consulted with respect to the establishment, operation, assessment and analysis of the air quality monitoring systems.
- The air monitoring exercise prescribed in condition 9.2.2 of the ROD will constitute an initial assessment. The applicant must develop an ongoing air quality impact assessment program to monitor emissions over the 2 year period, as envisaged in conditions 9.2.8 and 9.2.9 of the ROD.
- The results of all air quality monitoring must be incorporated into the prescribed landfill site audits for the Mariannhill and La Mercy landfill sites, and these results must be presented to the monitoring committee forums for each site.
- The air quality impact assessments undertaken for each site must upon completion, be submitted to the DAEA's sub-directorate on air quality, and also to the applicant's own environmental health unit (air quality management section) for comments.
- The results of the ongoing air quality impact assessment process conducted over the 2 year period must be measured against the baseline condition 9.2.2 of the ROD, and results reported to the DAEA.
- Pending the establishment of South African air quality standards, the applicant will be obliged to ensure that their emission limits do not exceed those established in the "Guidance of Monitoring Landfill Gas Engines, United Kingdom Environment Agency, Draft for Consultation, 2002"
- At the end of the 2 year pilot period of the project the DAEA will consider the results of the air quality monitoring and assessment programmes to inform future decisions regarding the continued operation of the projects.



- EIA applications for the permanent operation of the LFG capture and electricity generation and distribution facilities on both the Mariannhill and La Mercy landfill sites were to be considered by the DAEA at the end of the 2 year pilot project period.

Following the study performed by Enviros Consulting, commissioned by Felehetsa Consultants on behalf of DSW, it was concluded that the atmospheric dispersion modelling results indicate that the predicted concentrations of the modelled substances for combustion and fugitive releases (landfill gas engines and flares), are within the relevant air quality standards.

On this basis, and despite adoption of some worst case assumptions in the modelling approach, emissions of these substances are predicted to have no significant effects on human health. Monitoring to verify the results of the modelling study is proposed.

Furthermore, utilisation of landfill gas to generate electricity, thereby displacing the use of other fuel will mean that a wider scale reduction in air pollution emissions will be achieved. This will offset the increase in combustion-related emissions associated with electricity generation. It is therefore considered that, as no air quality benchmarks are forecast to be exceeded, the use of landfill gas engines as planned comprises best practice for management of landfill gas.

DSW then submitted a request to the KwaZulu Natal Department of Agriculture and Environmental Affairs, requesting a review of the 'pilot project' conditions imposed up on the project's implementation. In an amended ROD, dated 16/11/2005, para 3.3.2 notes that "the content of the new information indicates that the air quality impacts associated with the landfill gas projects will not only be acceptable, but will apparently improve the ambient quality of the air." Para 3.4.3 notes that: "The department [Department of Agriculture and Environmental Affairs, KwaZulu-Natal] has notified the only appellant to the original RODs of your request, and submitted the new information to him for comment. The appellant was the only party concerned with the air quality impacts and the assessment thereof in the original EIA process. There are consequently no other parties who have an interest in the new information, nor will the silent majority's interests, health or well-being be adversely affected in any respects by the decision to amend the conditions, given that the air quality impacts that would have arisen should the projects have been commissioned after the original RODs were issued will in no respects change as a result of the new information or of this department's decision to amend the conditions."

Detailed background

Durban Solid Waste provided Enviros with some information on the site-specific parameters, and other input data for the modelling assessment was obtained from UK guidance. A number of key assumptions, taken from UK guidance, were made for the modelling assessment and a conservative approach was taken. The forecast levels of pollutants are based on UK data. Baseline air quality was taken from actual monitoring data where available and a number of sensitive receptors were identified. The atmospheric dispersion modelling results for the both scenarios indicate that the predicted concentrations of the modelled substances for combustion releases (landfill gas engines and flares), are within the relevant air quality standards.

The Emission Concentration Standard used for dioxins and furans from enclosed LFG flares is 0.18 ng/Nm³. This is a proposed German standard quoted in draft UK Environment Agency guidance (Ref 10), but not adopted as UK standard. (p18 of AQ study).



The Emission Concentration Standard used for dioxins and furans from landfill gas engines is 0.1 ng/Nm³. This is a German HMfUR standard quoted in draft UK Environment Agency guidance (Ref 14), but not adopted as UK standard. (p 20 of AQ study).

Dispersion modelling was undertaken at the receptor location where the highest pollutant concentrations are forecast. Lower concentrations were forecast at all other receptors. The maximum modelled concentration of dioxins and furans in the absence of the project is 4.5×10^{-10} µg/m³. **With the project the maximum modelled concentration is 1.1×10^{-9} µg/m³. (pp 28 and 29 of AQ study). This is still well below the allowed standard of 0.18 ng/Nm³.**

The actual dioxin and furan emissions from flare and engine exhaust emissions will be monitored using extractive sampling to sorbent tube separated by high resolution gas chromatography (HRGC), and measured by high resolution mass spectrometry (HRMS).

Annex 1**CONTACT INFORMATION ON PARTICIPANTS IN THE PROJECT ACTIVITY.**

Organization:	Durban Solid Waste
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E-Mail:	
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Represented by:	
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Direct FAX:	27 (0)31 263 13107
Direct tel:	27 (0)31 263 1371/2
Personal E-Mail:	lindsay@dmws.durban.gov.za

Organization:	eThekweni Municipality
Street/P.O.Box:	No address
Building:	
City:	
State/Region:	
Postfix/ZIP:	
Country:	South Africa
Telephone:	
FAX:	
E-Mail:	
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Represented by:	
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Annex 2

INFORMATION REGARDING PUBLIC FUNDING

No ODA is involved in the project

Annex 3**BASELINE INFORMATION****A: Factor used for converting methane to carbon dioxide equivalents¹**

Factor used (CO ₂ e/CH ₄)	Period Applicable	Source
21	1996-present	Revised 1996 IPCC Guidelines for National Greenhouse Gas Inventories

B: Conversion volume of methane to weight of methane

	Factor	Unit	Period Applicable	Description/Source
Methane Density	At standard temperature and pressure (0 degree Celsius and 1,013 bar) the density of methane is 0.0007143 tCH ₄ /m ³ CH ₄ tonnes	t CH ₄ /m ³ CH ₄	Default	Mark's Standard Handbook for Mechanical Engineers Ninth Edition McGraw-Hill Book Company page 4-30, Table 4.1.7*

* The density of methane is given in that table as: **0.0416 pounds per cubic foot at 68 degrees F and 14.70 pounds per square inch**. To convert that to kilograms per cubic meter at **1.013 bar and 0 degrees Centigrade**: 293 degrees Kelvin/273 degrees Kelvin = 1.0732 which is the weight addition ratio at a constant volume, therefore 0.0416 x 1.0732 = **0.0446 pounds per cubic foot**. 1 cubic meter = 35.31 cubic feet, therefore 0.446 x 35.31 = 1.5748 pounds per cubic meter / 2.2046 pounds per kilogram = **0.7143 kilograms per cubic meter**

C: Project power generation costs:

The total cost for the total integrated 3 site project⁹ is estimated at US\$12.20 million based on adjusted budget quotes.¹⁰ Because there are multiple sites in the integrated project this can be broken down to and estimated cost of US\$1.35 million per MW of electricity capacity installed at any of the 3 landfill sites. This total includes all development costs including the Environmental Impact Assessment (EIA) preparation, the generation system installed costs, the interconnection costs, the gas well costs (not including the baseline wells), the financing costs including interest during construction, and an appropriate contingency of less than 10%. The US\$ price per MW installed is an appropriate way to budget this project by DSW since it is simply a staged procurement process for a multi-component integrated project.

The project is being structured to enable contracting for a firm annual delivery of 67.8 GWh from all 3 sites or 7.5GWh per MW installed. It is possible that the integrated project will deliver more MWh per year if the buyer will accept it, but the (maximum annual) guaranteed amount will be 67.8 GWh per year.

⁹ The original investment plan includes landfill gas recovery on the Bisasar Road landfill.

¹⁰ As reported in the DSW project spreadsheets prepared by Engineer Lindsay Strachan. The budget quotes suggested a price of over US\$13 million but historically final prices have been lower than the budget quotes received from these suppliers, hence a small downward adjustment has been made.



The first order indicator of the cost of production per kWh in a case wherein the fuel is considered free (other than capital cost recovery for the wells) is the debt service requirement for 100% debt finance.

Assumptions:

1. The Power Purchase Agreement will be for 10 years with options for 2 additional 5 year extensions.
2. The debt period is assumed to be 8 years to meet risk management criteria of typical financing sources.
3. The interest rate is assumed as 10% in US\$ terms.

The annual debt service requirement (including repayment of principal) on a debt of US\$12.20 million with an 8 year loan at 10% interest would be US\$181,440 per million of debt or US\$2,213,568 per year. That translates into a debt service component in the cost of production of US\$0.0326 per kWh. A 10 year, 10% loan would reduce this down to US\$0.0283 per kWh for sensitivity purposes. Because the lifetime of the engines (which form the main component of investment costs) is around 10 years, it can be assumed that a new loan will come into effect to purchase replacement engines at about the time when the first loan is fully repaid. Alternatively, equity financing of continued operation (including replacement engines) would arrive at a similar result, when taking depreciation and a reasonable return on investment into account.

The O&M cost per long term use of the piston engine generators is estimated to be US\$0.008 per kWh produced including all labour and materials charges for routine maintenance and for major overhauls. Adding the O&M component cost to the debt service component cost results in an estimated cost of production of US\$0.0406 per kWh. Adding in an administrative and insurance burden of US\$0.0016 per kWh results in a total estimated cost of production of **US\$0.0422 per kWh**.

Since the project development process started there has been a significant change in the ratio of the South African Rand to the US\$. The August 15, 2005 value of 6.46 Rand = 1 US\$ has been used to re-evaluate the project costs and revenues. The majority of the generation equipment is imported but the majority of components for the gas side of the project are available locally. No expatriate expertise is required for the operations and maintenance of the equipment. A re-evaluation of the cost of generation shows an essentially equal projection under the revised monetary conditions, hence the above number remains valid.

While inputs such as equity can change the answer somewhat, this value is considered as an accurate, yet **conservative** indicator of the cost of production for the proposed facility. The cost calculation is considered conservative, in particular because it does not include considerations of risks associated with the operation of a landfill gas-to-electricity project such as technology and resource risks.

Cost items	
Annual generation (GWh)	67.8 GWh
Estimated total cost of project (mill. US\$)	12.2
Annual debt service payment (8-year loan, 10% interest) on a per kWh basis (US\$/kWh)	0.0326
Operations & Maintenance (US\$/kWh)	0.008
Administration & Insurance (US\$/kWh)	0.0016
Total generation cost (US\$/kWh)	0.0422



For the revaluation of the cost assessment, given that the La Mercy site needed to be decommissioned in mid 2009, the most conservative route was chosen to demonstrate that by isolating the Mariannhill site, the estimated generation cost under both scenarios: 1-Original assumptions and 2-Original assumptions with increased energy generation potential and updated information on wells installation, remains higher than the benchmark identified by the earlier registered version of the PDD. Therefore as per the EB guidelines, the analysis uses the original input data, and key parameters have been modified so that an isolation of the site has been the central piece for the cost estimate. The same assumptions explained above have therefore been kept and the result is that the total estimated cost of production is **US\$0.0476 per kWh** and **US\$0.0377 per kWh** respectively. Updated versions of the summary table for both scenarios are below.

Scenario 1: Original Assumptions, with isolation of Marinahill site

Cost Items	
Annual generation (GWh)	3.942
Capital cost (US\$m)	1.0
US\$/kWh	US\$/kWh
Annual debt service payment (8 year loan, 10% interest) on a per kWh basis	\$0.0467
Operation & Maintenance cost (US\$/kWh)	\$0.0007
Administration & Insurance (US\$/kWh)	\$0.0003
Total generation cost (US\$/kWh)	\$0.0476

Scenario 2: Original assumptions with change of key parameters: Increased energy generation Capacity and well implementation (actual project situation in 2011)

Cost Items	
Annual generation (GWh)	7.884
Capital cost (US\$m)	1.6
US\$/kWh	US\$/kWh
Annual debt service payment (8 year loan, 10% interest) on a per kWh basis	\$0.0365
Operation & Maintenance cost (US\$/kWh)	\$0.0010
Administration & Insurance (US\$/kWh)	\$0.0003
Total generation cost (US\$/kWh)	\$0.0377

D. Current power prices and LRMC of South African grid

The municipal electric company, eThekweni Electricity, purchases its electricity primarily from Eskom, the national electricity utility company. Eskom electricity is among the lowest cost sources of electricity in the world, and the vast majority of Eskom generated electricity is derived from fully depreciated, mine-mouth coal-fired power stations. Ninety percent (90%) of the MWh generated by Eskom are derived from coal-steam power plants.

As of August 2005, the 24 hour weighted average tariff Eskom charges eThekweni Electricity is about 9.7 Rand cent (US\$0.0150) per kWh with off peak tariffs being as low as US\$0.0092 at 6.46 Rand per US\$ and after a total Eskom tariff structure revision lowering peak hour tariffs and raising off-peak tariffs. This compares with the initial PDD weighted average value of 13.7 Rand per kWh (US\$0.0156) at 8.78 Rand per US\$ under the old Eskom tariff regime.

**Current tariff level (US\$/kWh):**

Off - peak	0.0092
Weighted averaged	0.0150

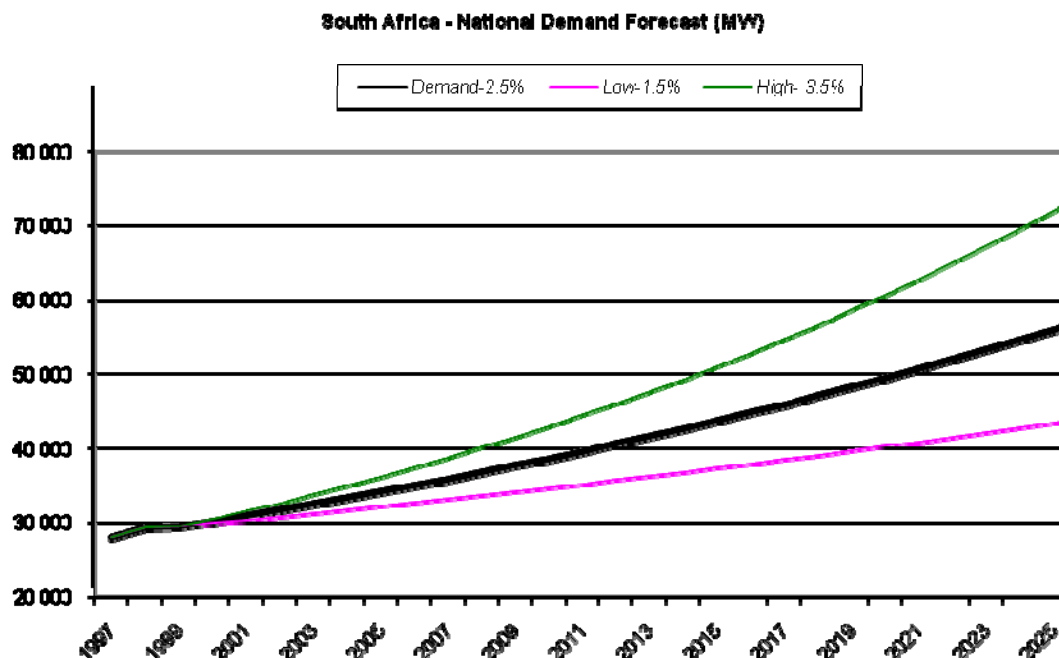
In order to estimate the long-term market price for electricity one needs to look at the development of the long run generation costs. If generation costs go up so will the price charged to customers. It is assumed, that Eskom will meet the demand for electricity at least cost. The least cost technology that can satisfy the projected demand over the project crediting period thus gives an indication for the development of the market price.

Supply and demand forecast

Today, South Africa's power generation capacity exceeds demand due to a decline in economic activity starting in the late 1980s and South Africa's large investment in power capacity in the 1970s and early 1980s. Assuming reasonable growth of 2.5%, the demand for electricity can be met by existing capacity over the next eight to nine years. South Africa has about 30,000 MW operating capacity and another 10,000 MW fully amortized excess capacity consisting of moth-balled coal-fired steam power plants which are being reactivated as needed. As South Africa is currently investing in new gas pipeline capacity, it is possible that, at the time when demand has caught up with capacity (anticipated to occur in eight or nine years), the country would accelerate the building of new gas-fired power capacity to meet the growing demand. Alternatively, the coal-fired power generation capacity could be expanded or some mixture of gas and coal derived power could be added.

According to Eskom's annual reports and statistical reports the 4 year average electricity demand growth from 1996 –2000 was only 1.5%, but the 1 year growth between 1999-2000 was 2.8%. Eskom's forecast of electricity demand is based on three scenarios of economic growth at 3.5%, 2.5% and 1.5%. With actual annual GDP growth of 2.7% (treasury department), the middle scenario was deemed the most likely for demand projections. Recent year (through 2004) growth statistics suggest that a middle to high range is more likely.

Electricity demand forecast, South Africa 1997-2025



Source: NER

1. Long run marginal costs with excess supply

The long run marginal costs of the South African grid are determined by the generating costs of the existing capacity up to the point where investment in new capacity is required. That is, until existing capacity is exhausted and new capacity must be installed, the long-run marginal costs in South Africa are equivalent to the short-run marginal costs. The current generation costs per kWh in a fully depreciated Eskom power plant are estimated to be US\$0.004. Depending on coal price, heating content and plant efficiency this could range from US\$0.003 to US\$0.005 per kWh. The reactivation of the moth-balled power plants is not at this time leading to even slightly higher generation costs. For the World Bank Renewable Energy Program being developed in South Africa, the current Eskom generation costs are conservatively assumed to be US\$0.0105 per kWh rising to no more than US\$0.0225 – in 5 to 7 years at the soonest – including the reactivation of moth-balled capacity and some new gas-fired capacity.¹¹

2. Long run marginal costs to meet growing future demand

Natural Gas from Mozambique is a possible least cost expansion option for Eskom to develop within South Africa after the electricity demand has outgrown existing capacity, including the moth-balled coal-fired capacity. No political obstacles are to be expected since South African firms are already controlling many gas fields in Mozambique. This assumes that no new coal-fired capacity would be developed in South Africa. However, South Africa maintains the option to increase coal-fired power capacity and may pursue this option, if such coal-based capacity results in lower power generation costs than the use of

¹¹ See World Bank (2002) South Africa: Renewable Energy Market Transformation, Project Concept Document (PCD) Africa Regional Office, AFTEG



pipeline gas. The coal-based option therefore serves as a low-cost fall back option, e.g. if gas prices increase significantly. Assuming gas-fired power expansion, with which landfill gas-derived electricity would have to compete, appears therefore as a conservative assumption.

The most likely US\$ value for the gas transmitted by pipeline from the relatively nearby gas fields would be in the vicinity of US\$2.00 – 2.50 per million Btu, before considering the petroleum product market price impact on gas pricing. At the value assumed that would put it close to the point where a Combined Cycle plant would be competitive with a Simple Cycle plant. For purposes herein, both cases will be considered as will gas prices of \$2.00 and \$2.50 per million Btu, based on the calculation given in table 3. The financing term is a 10 years period.

Generation costs of a simple and a combined cycle gas turbine

	Simple Cycle	Combined Cycle
Capital Cost – US\$/MW	0.55	0.85
Efficiency - %	38	49
Heat Rate – Btu/kWh	8,980	6,965
Fuel Cost/kWh (\$2 gas) - \$/kWh	0.0179	0.0139
Fuel Cost/kWh (\$2.5 gas) - \$/kWh	0.0224	0.0174
O&M + admin... Cost - \$/kWh	0.0025	0.0030
Debt Service - \$/kWh	0.0104	0.0161
Estimated LRM	US\$0.0308 – 0.0353	US\$0.0330 – 0.0365

Source: Own calculations

The projected increase in power demand over time and the options to meet this demand results in an increase over time of generation costs in the South African power system (Table 3). The Table shows in Line (1) the current demand, which is met by existing mostly coal-based capacity in a situation of excess generation capacity, and the associated costs (mainly operating and maintenance costs). Line (2) shows the costs at a time when demand growth has caught up with existing capacity (projected in eight to nine years). And Line (3) shows the long-run marginal costs that include the addition of new capacity to the system in order to meet further growing demand.

LRMC in relation to MW demand

System condition	Demand	LRMC in US\$ per kWh
(1) Current demand	Up to 30.000 MW	0.004-0.0105
(2) Demand catches up with existing capacity	Up to 40.000 MW	0.0225
(3) New capacity added	> 40.000 MW	0.0308-0.0365

Source: Own calculations based on World Bank (2002) South Africa: Renewable Energy Market Transformation, Project Concept Document (PCD) Africa Regional Office, AFTEG and Table 2.

There seems to be no shortage with respect to South Africa's natural gas purchase from Mozambique and Namibia, and coal as a fall-back option is abundant and low cost in South Africa. It is thus safe to assume that over the project lifetime, long run marginal costs of the South African grid will not exceed US\$0.0365. For the period until 2012 the generation costs will not likely exceed US\$0.0225 and current Eskom tariff trends confirm this hypothesis.

E. Grid Emission Factor

0.895 kg of CO₂ per kWh (2003 Eskom Annual Report)



Annex 4

MONITORING PLAN

This annex explains the steps to be followed to monitor the parameters necessary to calculate the GHG emissions from the La Mercy and Mariannhill Landfill Gas to Electricity Project in Durbin, South Africa.

The monitoring equipment described herein, may be modified to meet operational requirements or system upgrades. Any modifications will take into account the monitoring requirements specified in the applied methodology and will be subject to review in the verification process.

Applied methodology

AM0010 Approved Monitoring Methodology “Landfill gas capture and electricity generation projects where landfill gas capture is not mandated by law” – Version 01.

Brief description of the methodology

The monitoring methodology is based on direct measurement of the amount of landfill gas collected at the “baseline” wells, if any and the amount of methane used to generate electricity.

The amount of methane destroyed by generating electricity (MDprojecty) is determined by monitoring the:

- Amount of landfill gas collected (m3) using a continuous flow meter and monitoring temperature and pressure.
- Percentage of landfill gas that is methane (% - using a continuous gas analyzer).

The amount of electricity sold to the grid (MWh) will be metered continuously.

In addition, the methane content of the boiler/engine emissions will be analyzed quarterly to determine the fraction of the methane destroyed.

Data to be collected or used in order to monitor emissions from the project activity and how this data will be archived

The information for this heading is provided in the table below. The data to be collected will be done in accordance with AM0010 Version 1.



ID number	Data type	Data unit	Measured (m), calculated (c) or estimated (e)	Recording frequency	Proportion of data to be monitored	How will the data be archived? (electronic/ paper)	For how long is archived data to be kept?	Comment
1. MV baseliney	Amount of landfill gas collected from baseline wells	m ³	m	continuous	100%	electronic	Duration of project crediting period	Measured by flow meter. Data will be aggregated monthly and yearly. Temperature and pressure will also be measured with volume adjusted to standard temperature and pressure.
2 MVprojecty ¹²	At the Mariannhill site derived from the amount of landfill gas collected from the gas field, minus the amount of landfill gas collected from the baseline wells. At La Mercy site the amount of landfill gas collected from the gas field	m ³	m and c	continuous	100%	electronic	Duration of project crediting period	At Mariannhill measured by three flow meters. Total gas used for power generation plus gas flared (gas extracted from the field) minus gas collected from the baseline wells. At La Mercy site, measured by two flow meters. Data will be aggregated monthly and yearly. Temperature and pressure must also be measured with volume adjusted to standard temperature and pressure.

¹² Following guidance from the CDM EB after request for deviation submitted for the first monitored period and PDD submitted at the time, and also found online at <http://cdm.unfccc.int/Projects/deviations/96737>

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3	Methane content of landfill gas ¹³	%	m and c	continuous and periodic	100%	electronic	Duration of project crediting period	The monitoring of methane content combusted, and used for emission reduction calculations shall be continuous. The monitoring of the methane content in the baseline, for crosscheck purposes, shall be periodic.
4 ESy	Amount of net electricity sold to the grid	MWh	m	continuous	100%	electronic	Duration of the project crediting period	Measured by kWh meters, for the imported and exported electricity. Data will be aggregated monthly and yearly.
5. EGy	Amount of electricity generated.	MWh	m	continuous	100%	electronic	Duration of the project crediting period	Measured by a kWh meter Data will be aggregated monthly and yearly
6	Combustion efficiency	%	m and c	annual, monthly if unstable	n/a	electronic	Duration of the project crediting period	Methane content of engine/boiler exhausts gas.
7	LFG temperature and pressure	oC/Pa	c	periodic, daily	100%	electronic	Duration of the project crediting period	Device that provides data that can be used to determine the density of methane or provides for integration of measurement of temperature and pressure in order to provide a direct reading of the normalized gas flow.

¹³ Following guidance from the CDM EB after request for deviation submitted for the first monitored period and PDD submitted at the time, and also found online at <http://cdm.unfccc.int/Projects/deviations/96737>

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8	Flare working hours							When the flare temperature (parameter 9 below) is below 500 °C it is assumed that the flare is not operating and therefore during that time no ERs are claimed.
9	Flare temperature	oC	m	continuous	100% while flare is in operation	electronic	Duration of the project crediting period	Continuous measurement of operation hours based on measured flare temperature using a device such as a thermocouple. If there is no record of the temperature of the exhaust gas of the flare or if the recorded temperature is less than 500 °C for any particular hour, it shall be assumed that during that hour the flare efficiency is zero
10 HRy	Heat rate of the generator	Gj/M Wh	m and c	annual, monthly if unstable	N/A	electronic	Duration of crediting period	Data will be used to test and if necessary, correct the generator's name plate heat rate.
11 Wx	Total amount of waste disposed in year x	ton	m	Daily, aggregated monthly	100%	electronic	Duration of crediting period	Data will be used to conduct the calculation of the theoretical amount of methane generated from disposal of waste at the SWDS, as per the FOD model explained in section D.2.2 above. Data to be measured by a calibrated weighbridge as per the South African Metrology Act of 1973 requirements



12. $W_{j,x}$	Amount of solid waste type j disposed or prevented from disposal in the SWDS in the year x	ton	m	Daily, aggregated monthly	100%	electronic	Duration of crediting period	Data will be used to conduct the annual calculation of the theoretical amount of methane generated from disposal of waste at the SWDS, as per the FOD model explained below. Data to be measured by a calibrated weighbridge as per the South African Metrology Act of 1973 requirements
13. $p_{j,x}$	Waste composition in the year	%	c	annually	Calculated based on 100% monitored data	electronic	Duration of crediting period	Calculated based on parameters W_x and $W_{j,x}$ and used as input data to the FOD spreadsheet model



CER INSTRUMENTATION LIST: LA MERCY								
	Instrument Name/Description	Manufacturer/Supplier	Model	Type / SN	Range	Accuracy	Used to measure:	Calibration Requirement
	<u>Fixed Instrumentation used to measure Parameters</u>							
1	Temperature Transmitter	WIKA	TR200	46002570	0 to 100 °C	0.75% of full scale	Flare Temperature x2	n/a (replace as required)
2	Pressure Gauge	Dresser Ashcroft	N5500	n/a	-250 to 0 mbar	1.6% of full scale	Suction pressure	n/a (replace as required)
3	Pressure Gauge	Dresser Ashcroft	N5500	n/a	0 to 250mb	1.6% of full scale	Delivery Pressure	n/a (replace as required)
4	Thermal Mass Flow Meter	Kurz Instruments	Series 454FT	FD13164A	0-18000SFPM	+/-0.75% of Rate	Flare Flow	n/a (replace as required)
5	Thermal Mass Flow Meter	Kurz Instruments	Series 454FT	FD13165A	0-18000SFPM	+/-0.75% of Rate	Engine Flow	n/a (replace as required)
6	Stationary Gas Monitor - Methane	Madur	MaMoS-200 NDIR CH4	7082149	0 to 100%	+/-2% reading and 1% range	CH4	annual
7	Stationary Gas Monitor - CO2	Madur	MaMoS-200 NDIR CO2	7082150	0 to 50%	+/-3% reading and 1.5% range	CO2	annual
8	Stationary Gas Monitor - Methane	Edinburgh Instruments*	Gascard II	25747	0 to 100%	2%	CH4	annual
9	Stationary Gas Monitor - CO2	Edinburgh Instruments*	Gascard II	25695	1 to 100%	2%	CO2	annual
10	Oxygen Analyzer	City Technology	T70X	11077314117	0 to 25%	+/- 0.5%	O2	n/a (replace as required)
11	Atmospheric Pressure Sensor	GE Sensing	PTX1400	n/a	800 to 1200mb	0.15%	Atmospheric Pressure	n/a (replace as required)
12	3 Phase 3 Wire Meter	Landis + Gyr	7005405M	n/a	0 to 5A	0.10%	11000V Meter Export check	10 yrs
13	3 Phase 4 Wire Meter	Landis + Gyr	Dialog	ZMD405CT44.2407 S2	0 to 5A	0.10%	11000V Meter Export kW	10 yrs
14	3 Phase 4 Wire Meter	Landis + Gyr	Dialog	ZMD310CT44.0007 S2a	0 to 120A	0.10%	400V Meter Import kW	10 yrs
	<u>Hand Held Instrumentation</u>							
15	Hand Held Gas Analyzer	Geotechnical Instruments	GA2000	GA08915	0 to 60% CH4	3% CH4,CO2 and 1% O2	CH4, CO2, O2	Annual

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INSTRUMENTATION LIST: MARIANNHILL								
	Instrument Name/Description	Manufacturer/Supplier	Model	Type / SN	Range	Accuracy	Used to measure:	Calibration requirement
	<u>Fixed Instrumentation used to measure Parameters</u>							
1	Temperature Transmitter	WIKA	TR200	46002570	0 to 100 °C	0.75% of full scale	gas temperature	n/a
2	Pressure Transmitter	GE Sensing - Druck	PTX 510-1176	2343640	-250 to 0 mbar	+/- 0.15% full scale	Suction pressure	n/a
3	Pressure Transmitter	GE Sensing - Druck	PTX 7900-3399	2345399	0 to 250mb	+/- 0.25% full scale	Delivery Pressure	n/a
4	Pressure Gauge	Dresser Ashcroft	N5500	n/a	-250 to 0 mbar	1.6% of full scale	Suction Pressure	n/a
5	Pressure Gauge	Dresser Ashcroft	N5500	n/a	0 to 250mb	1.6% of full scale	Delivery Pressure	n/a
6	Thermal Mass Flow Meter	Kurz Instruments	Series 454FT	FD20272A	0-18000SFPM	+/-0.75% of Rate	Flare Flow	annual
7	Thermal Mass Flow Meter	Kurz Instruments	Series 454FT	FD20273A	0-18000SFPM	+/-0.75% of Rate	Engine Flow	annual
8	Thermal Mass Flow Meter	Kurz Instruments	Series 454FT	FD20271A	0-18000SFPM	+/-0.75% of Rate	Baseline Flow	annual
9	Stationary Gas Monitor - Methane *	Edinburgh Instruments	Gascard II	25746	0 to 100%	+/- 2% of range	CH4	annual
10	Stationary Gas Monitor - CO2 *	Edinburgh Instruments	Gascard II	25696	0 to 50%	+/- 2%of range	CO2	annual
11	Oxygen Analyzer	City Technology	T70X	12150830048	0 to 25%	+/- 0.5%	O2	n/a
12	Atmospheric Pressure Sensor	GE Sensing - Druck	PTX1400		800 to 1200mb	0.15%	Atmospheric Pressure	n/a
13	3 Phase 4 Wire Meter	Landis + Gyr	Dialog		0 to 5A	0.10%	11000V Meter Export check	10 yrs
14	3 Phase 4 Wire Meter	Landis + Gyr	Dialog		0 to 5A	0.10%	11000V Meter Export kW	10 yrs
15	3 Phase 4 Wire Meter	Landis + Gyr	Dialog		1 to 120A	0.10%	400V Meter Import kW	10 yrs
	<u>Hand Held Instrumentation</u>							
16	Hand Held Gas Analyzer	Geotechnical Instruments	GA2000	GA08915	0 to 60% CH4	3% CH4,CO2 and 1% O2	CH4, CO2, O2	annual

**Instrumentation and calibration**

Maintenance and instrumentation calibration will be carried out in accordance with manufacturer's requirements. The QC/QA procedures are described in the table below.

Quality control (QC) and quality assurance (QA) procedures are being undertaken for data monitored		
Data (Indicate table and ID number e.g. 3.-1.; 3.2.)	Uncertainty level of data (High/Medium/Low)	Explain QA/QC procedures planned for these data, or why such procedures are not necessary.
Table D 2.2 - 1 LFGy	Low	Flow meters will be subject to a regular maintenance regime to ensure accuracy
Table D.2.2- 2 EGy	Low	Electricity meters will be subject to a regular maintenance and testing regime to ensure accuracy. Their reading will be checked by the electricity distribution company.
Table D2.2 - 10 HRy	Low	Regular maintenance will ensure optimal operation of engines and generators. The heat rate will be checked semi-annually, with monthly checks if the heat rate shows significant deviations from previous values.
Table D.2.2 -11 Wx	Low	Regular maintenance for the weighbridge, calibrate as required by the South African Metrology Act of 1973, and Government Notice 649, dated 20 July 2007.
Table D.2.2 -11 Wj,x	Low	Regular maintenance for the weighbridge, calibrate as required by the South African Metrology Act of 1973, and Government Notice 649, dated 20 July 2007.

**Data collection:**

Some data are collected automatically through a data logger such as, gas flow, gas quality and flare temperature.

A daily visual inspection is carried out by a designated / trained landfill employee. During this daily inspection, the employee will check the instrumentation and monitoring data such as gas quality, gas flow, vacuum, and flare temperature. Also the employee will analyze the data and adjust the applied vacuum within the landfill to maintain a steady gas quality and flow.

Gas quality and vacuum levels also will be periodically checked directly at each gas well, using a portable meter. This routine monitoring allows to identify underperforming gas wells and to take necessary corrective actions. The combination of these two inspections optimises the landfill gas collection efficiency.

Data Storage:

Data will be monitored and archived as described in the AM0010 monitoring methodology. As specified, data will be kept for the duration of the crediting period and two years after.

Project Management Responsibility:

The project implementation and operation will be under the direct Supervision of the Landfill Manager. Table 1 summarizes the roles and responsibilities of project sponsor with regard to the monitoring system for the project.

Table 1– MP Management and Operation System

Task	
Monitoring system	<ul style="list-style-type: none"> Develop and establish management and operations system Establish and maintain monitoring and reporting system and implement MP Prepare for initial verification and start of project operation
Data Collection	<ul style="list-style-type: none"> Establish and maintain data measurement, collection and record keeping systems for landfill gas collection and power supply Check data quality, collection and record keeping procedures regularly
Data computation	<ul style="list-style-type: none"> Complete MP workbook Or develop and use equivalent recording, calculation and reporting tool for ERs
Data storage systems	<ul style="list-style-type: none"> Implement record maintenance system Store and maintain records (paper trail) Implement sign-off system for records and completed worksheets
Performance monitoring and reporting	<ul style="list-style-type: none"> Analyze data and compare project performance with project targets Analyze system problems and implement improvements (performance management) Prepare and forward annual report and worksheets to WB CFU
Quality assurance and verification	<ul style="list-style-type: none"> Establish and maintain quality assurance system with a view to ensuring transparency and allowing for audits and verification Prepare for, facilitate and co-ordinate audits and verification process

Training of monitoring personnel:



Once a year the monitoring personnel will be trained internally or externally.

Training will include:

- Landfill gas collection system balancing
- Calibration of monitoring equipment
- Impact of the monitoring on the CDM activity

Procedure in case of Failure:

If there is an equipment (flow meter, gas analyser, gauge, etc.) failure, the equipment supplier will be immediately notified. If possible, repairs will be carried out. If the damaged equipment cannot be repaired, it will be replaced by the same or an equivalent unit as soon as possible. In some cases, portable tools will be used in order to carry out daily monitoring of the missing parameter(s). These data will be recorded on paper.

If the flare is not operational, landfill gas will not be combusted and therefore no credits will be claimed during this period. The running hours of the flares will be monitored as part of the monitoring procedures.

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