

**MONITORING REPORT FORM (F-CDM-MR)**  
**Version 02.0****MONITORING REPORT**

|  |   |
|--|---|
| <b>Title of the project activity</b>   | Catalytic N <sub>2</sub> O Abatement Project in the Tail Gas of the Nitric Acid Plant of the Hanwha Corporation (HWC) in Ulsan, Republic of Korea                               |
| <b>Reference number of the project activity</b>  | 0922  |
| <b>Version number of the monitoring report</b>   | 3.0   |
| <b>Completion date of the monitoring report</b>  | 20/09/2012  |
| <b>Registration date of the project activity</b>   | 03/05/2007  |
| <b>Monitoring period number and duration of this monitoring period</b>   | The 6th monitoring period: 01/01/2012 - 30/06/2012  |
| <b>Project participant(s)</b>  | •Hanwha Corporation (HWC)<br>•Mitsubishi Corporation (Korea) Ltd.<br>•Mitsubishi Corporation  |
| <b>Host Party(ies)</b>   | Republic of Korea   |
| <b>Sectoral scope(s) and applied methodology(ies)</b>  | •Category 5: Chemical industries.<br>•AM0028 version 3: “Catalytic N <sub>2</sub> O destruction in the tail gas of Nitric Acid or Caprolactam production plants --- version 3”. |
| <b>Estimated amount of GHG emission reductions or net anthropogenic GHG removals by sinks for this monitoring period in the registered PDD</b> | 281,272 tCO <sub>2</sub> e / year (365 days)<br>[equivalent to 140,251 tCO <sub>2</sub> e / 182 days]   |
| <b>Actual GHG emission reductions or net anthropogenic GHG removals by sinks achieved in this monitoring period</b>                            | 153,562 tCO <sub>2</sub> e / 182 days   |

**SECTION A. Description of project activity****A.1. Purpose and general description of project activity**

&gt;&gt;

1. Purpose of the project activity and the measures taken to reduce greenhouse gas emissions :  
Hanwha Corporation owns Nitric Acid Plant in Ulsan City, Republic of Korea and produces nitric acid and based on which Hanwha Corporation further produces explosives mainly. From the plant, Nitrous Oxide ( $N_2O$ ), which is an undesired by-product of the nitric acid production process, is released into the atmosphere.  
Hanwha Corporation has one production line. The aim of the project activity is to reduce  $N_2O$  emissions by installation of De $N_2O$  Unit before the Stack, which is called Tertiary Catalyst System or Tail Gas System.
2. Brief description of the installed technology and equipments :  
For the  $N_2O$  abatement project, Tertiary Catalyst System has been installed in the Nitric Acid Production Line, which consists of the catalyst, supplied by N.E.Chemcat Corporation, Japan as well as the reactor, supplied by Sumitomo Metal Mining Engineering Corporation, Japan. In order to monitor the  $N_2O$  reduction, the Automated Measuring Systems (AMS), including non-dispersion infrared absorption analyzer (NDIR) was installed, which is applicable to European standards and norms (EN 14181) or equivalent standards.
3. Total emission reductions achieved in this monitoring period (01/01/2012 – 30/06/2012) :  
153,562 ton:  
Remarks: Actual emission reductions achieved in this monitoring period is 154,545 tCO<sub>2</sub>e.  
The emission reduction amount for which Request for Issuance is applied for this monitoring period is claimed as 153,562 tCO<sub>2</sub>e, 983 tCO<sub>2</sub>e deducted from 154,545 tCO<sub>2</sub>e. This is because total emission reductions amount of the 4th monitoring period which has been already issued is 239,482 tCO<sub>2</sub>e where we applied the wrong Pg data ( $7.022 \sim 8.806 \times 10^5$  Pa.g).  
The revised emission reductions amount of the 4th monitoring period is 238,499 tCO<sub>2</sub>e where the right default value ( $7.071 \sim 8.767 \times 10^5$  Pa.g ) is applied. There was 983 tCO<sub>2</sub>e in excess. Therefore, for this monitoring period 153,562 tCO<sub>2</sub>e is applied for Request for Issuance.  
Note: Such wrong Pg data were used for both 4th and 5th monitoring periods. But there is no effect on the 5th monitoring period.

**A.2. Location of project activity**

&gt;&gt;

- (a) Host Party(ies);  
Republic of Korea
- (b) Region/ State/ Province, etc.;  
----- (N/A)
- (c) City/ Town/ Community, etc.;;  
753-22 nsan eup, Ulju gun, Ulsan city, 689-892
- (d) Physical/ Geographical location.  
35.2043, 129.1223 (Latitude 35.2043 north and Longitude +129.1223 east)

**A.3. Parties and project participant(s)**

| Party involved<br>(host) indicates a host Party) | Private and/or public<br>entity(ies) project participants<br>(as applicable)                         | Indicate if the Party involved<br>wishes to be considered as<br>project participant (Yes/No) |
|--|--|--|
| Republic of<br>Korea (host)                      | <b>Hanwha Corporation (HWC)</b><br>[owner and operator of the nitric<br>acid plant]                  | No.  |
|  | <b>Mitsubishi Corporation<br/>(Korea) Ltd.</b><br>[developer and co-financer of<br>this CDM project] | No.  |
| Japan  | <b>Mitsubishi Corporation</b><br>[developer and co-financer of<br>this CDM project]                  | No.  |
| Switzerland                                      | <b>Hanwha Corporation</b>  | No.  |

**A.4. Reference of applied methodology**

&gt;&gt;

(a) The applied methodology(ies)

AM0028 version 3: “Catalytic N<sub>2</sub>O destruction in the tail gas of Nitric Acid or Caprolactam production plants --- version 3”.

(b) Any tools and other methodologies to which the applied methodology(ies) refers

Tool for demonstration and assessment of additionality" (Version 01)

**A.5. Crediting period of project activity**

&gt;&gt;

The start date of Crediting period is 27/06/2007 (changed by post-registration request).

7 year crediting period with twice renewal (total 21 years) was selected for the project activity.

It was changed from July 1, 2007 – June 30, 2014 and such change was approved by UNFCCC on January 29, 2008.

**SECTION B. Implementation of project activity****B.1. Description of implemented registered project activity**

&gt;&gt;

1. The starting date of operation of the project activity.

Starting date of the project activity: 27/06/2007

2. The information regarding the actual operation of the project activity during this monitoring period, including information on special events, for example overhaul times, downtimes of equipment, exchange of equipment, etc.

Please see the “Daily Events” mentioned in Annex-2.

3. A brief description of: (i) events or situations that occurred during the monitoring period, which may impact the applicability of the methodology, and (ii) how the issues resulting from these events or situations are being addressed.

N/A

## **B.2. Post registration changes**

### **B.2.1. Temporary deviations from registered monitoring plan or applied methodology**

>>

No deviations from registered monitoring plan.

### **B.2.2 Corrections**

>>

No corrections.

### **B.2.3. Permanent changes from registered monitoring plan or applied methodology**

>>

No permanent changes from registered monitoring plan

### **B.2.4. Changes to project design of registered project activity**

>>

No changes to project design of registered project activity.

### **B.2.5. Changes to start date of crediting period**

>>

The start date of Crediting period is 27/06/2007 (changed by post-registration request).

7 year crediting period with twice renewal (total 21 years) was selected for the project activity.

It was changed from July 1, 2007 – June 30, 2014 and such change was approved by UNFCCC on January 29, 2008.

### **B.2.6. Types of changes specific to afforestation or reforestation project activity**

>>

No.

## **SECTION C. Description of monitoring system**

>>

### **1. Monitoring plan and methodology**

The approved monitoring methodology AM0028 version 3 “Catalytic N<sub>2</sub>O destruction in the tail gas of Nitric Acid or Caprolactam Production Plants” was applied to this project activity. This approved monitoring methodology is applicable to the project activities that abate N<sub>2</sub>O emissions either by catalytic decomposition or catalytic reduction of N<sub>2</sub>O in the tail gas of nitric acid plants (i.e. tertiary destruction). The present project activity satisfies applicability conditions.

### **2. Data collection procedure**

Please see the figure below for position of monitoring parameters for the project. Respective data from each monitoring points are generated, aggregated, recorded, calculated and reported as follows.

Data collection flow of the monitoring system is as per the chart below :



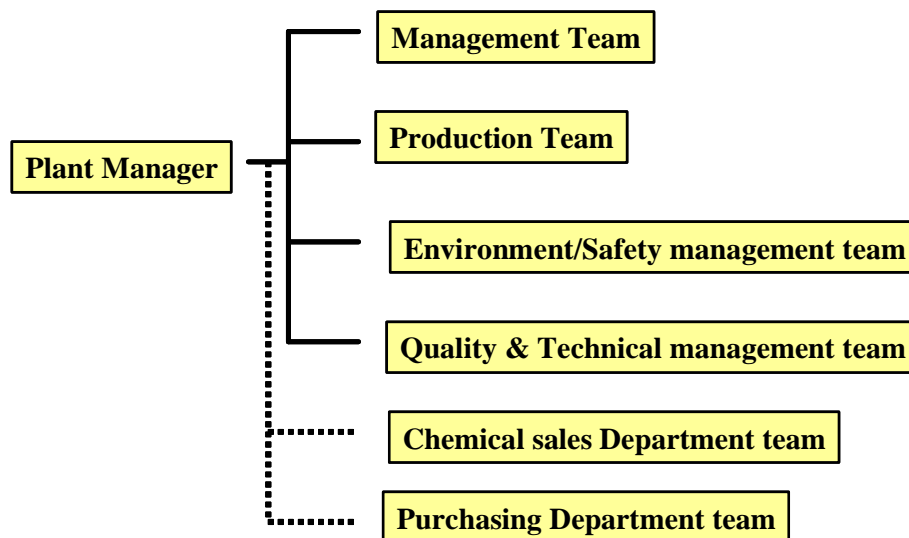
| Parameter                        | Data description   | Data generation                                  | Measured by  | Aggregation/Recording                   | Calculation                             | Reporting                |
|----------------------------------|--|--|--|---|---|--------------------------|
| $CI_{N_2O,i}$                    | N <sub>2</sub> O concentration at destruction facility inlet.    | Inlet of DeN <sub>2</sub> O                      | Non-dispersion infrared absorption analyzer  | ABB data logging system                 | Excel spreadsheet (According to AM0028) | By Hanwha and Mitsubishi |
| $F_{TLi}$                        | Volume flow rate at the inlet of the destruction facility        |  | Multiple-point sampling tube type flow meter with D/P Transmitter, Absolute pressure transmitter and Resistance Temperature Detector |   |   |                          |
| $CO_{N_2O,i}$                    | N <sub>2</sub> O concentration at destruction facility outlet.   | Outlet of DeN <sub>2</sub> O                     | Non-dispersion infrared absorption analyzer  |   |   |                          |
| $F_{TEi}$                        | Volume flow rate at the exit of the destruction facility         |  | Multiple-point sampling tube type flow meter with D/P Transmitter, Absolute pressure transmitter and Resistance Temperature Detector |   |   |                          |
| $Q_{NG}$                         | Hydrocarbon (Natural gas) input                                  | DeN <sub>2</sub> O                               | Integral Orifice flow meter with temperature, pressure measuring unit for auto compensation  | ⇒                                       | ⇒                                       | ⇒                        |
| Natural gas contents information |  |  | Ingredients label by the natural gas supplier  | by handling                             |   |                          |
| $P_{product,y}$                  | Plant output of HNO <sub>3</sub>                                 | Outlet of absorption tower                       | Magnetic flow meter with Resistance Temperature Detector   | DCS system (distributed control system) |   |                          |
| $A_{OR,d}$                       | Actual ammonia flow rate to the ammonia oxidation reactor        | Inlet of AOR                                     | Orifice type flow meter with D/P Transmitter, Absolute pressure transmitter and Resistance Temperature Detector                      |   |   |                          |
| $T_g$                            | Actual operating temperature of the ammonia oxidation reactor    | Inside AOR                                       | Thermocouple (Type "R") with temperature transmitter   |   |   |                          |
| $P_g$                            | Actual operating pressure of the ammonia oxidation reactor       | Between air compressor/NH <sub>3</sub> air mixer | Pressure Transmitter   |   |   |                          |
| $E_{IRCS,y}$                     | Additional electricity input for running DeN <sub>2</sub> O unit | DeN <sub>2</sub> O unit operating panel          | Electricity accumulator (Wattmeter)  | Hand writing                            |   |                          |

### 3. Organization structure of Hanwha's project team, including the role and responsibility of the personnel

Hanwha has been operating the nitric acid plants since the commissioning of the plant in 1992 and has sufficient and well-experienced staffs. Hanwha has been in production of the nitric acid for number of years and measurement of various production parameters including operation of analyzers which are managed by production team. The monitoring of the N<sub>2</sub>O for the project is responsible by production team. The operation and maintenance of the N<sub>2</sub>O monitoring system incorporates the ISO 9001-2008 standard procedures. The monitoring of the relevant data is done by the N<sub>2</sub>O monitoring system and recorded onto the electric media.

Production team is appointed and responsible for the operation of the N<sub>2</sub>O monitoring system. Production team follows the monitoring plan and reports the data on regular intervals to management team and plant manager in ascending order.

An illustrative scheme of the operational and management structure is as follows:



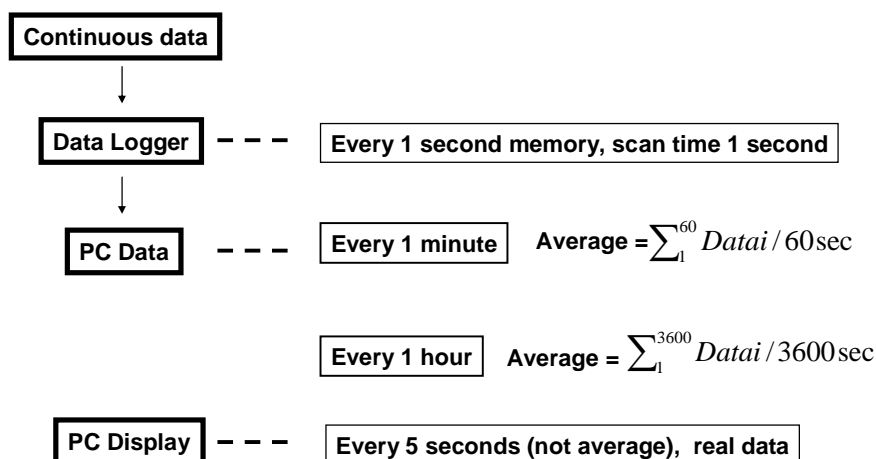
#### 4. Emergency procedures for the monitoring system

In case of emergency or any deviation in the monitoring data is found, production team engineer shall study the operating parameters of the nitric acid plant to identify the reason for the deviation and take remedial measures. If there is no change in the operating parameter of nitric acid plant, the monitoring system shall be examined. Once the default is identified, quality & technical management team and environment & safety management team shall introduce a correction to the default. Production team engineer shall report such irregular event to plant manager.

For others concerning good monitoring practice and performance characteristics including such as EN14181 or equivalent standards available in the Republic of Korea specified in AM0028 version03.

#### 5. Monitoring and calculation details of N<sub>2</sub>O concentration & tail gas measurement

Following method is applied :



## 6. Calibration and maintenance

All measuring and analytical instruments are calibrated as defined in the approved methodology AM0028 version 3. Calibration procedures have been incorporated in Hanwha Corporation's quality management system and procedures.

The measurement equipments are calibrated on regular intervals as recommended by the manufacturers. Additionally, selected staffs from Hanwha Corporation participate in initial training and are trained to operate measurement system.

For other concerning good monitoring practice and performance characteristics including such as EN14181 or equivalent standards available in Republic of Korea specified in AM0028 version 3, which is mentioned in Annex 4 of concerned PDD.

Information of calibration of each equipment is as below:

| Instrument Overview: Hanwha              |                  |
|--|------------------|
| Instrument                               | TAG Number       |
| Destruction Facility Inlet Analyzer      | 10-AT-061(A1061) |
| Destruction Facility Outlet Analyzer     | 10-AT-062(A1062) |
| Inlet Tail Gas Flow                      | 10-FT-561(F1561) |
| Outlet Tail Gas Flow                     | 10-FT-562(F1562) |
| Natural Gas Flow to Destruction Facility | 10-FT-563(F1563) |
| Ammonia Flow to AOR                      | 10-FT-502(F1502) |
| Pressure in AOR                          | 10-PT-304(P1304) |
| Temperature in AOR                       | 10-TT-115(T1115) |
| HNO <sub>3</sub> (Nitric Acid) Flow      | 10-FT-512(F1512) |

More information of calibration of each instrument is available in Annex-3

## SECTION D. Data and parameters

### D.1. Data and parameters fixed ex ante or at renewal of crediting period

|                           |  |
|---------------------------|--|
| <b>Data / Parameter</b>   | <b><math>GWP_{N_2O}</math></b>               |
| <b>Unit</b>               | tCO <sub>2</sub> e/tN <sub>2</sub> O         |
| <b>Description</b>        | Global warming potential of the nitric oxide |
| <b>Source of data</b>     | IPCC, The Second Assessment Report           |
| <b>Value(s) applied</b>   | 310, as specified in the methodology         |
| <b>Purpose of data</b>    | Baseline/Project                             |
| <b>Additional comment</b> | N/A  |

|                           |   |
|---------------------------|---|
| <b>Data / Parameter</b>   | <b><math>GWP_{CH_4}</math></b>          |
| <b>Unit</b>               | tCO <sub>2</sub> e/tCH <sub>4</sub>     |
| <b>Description</b>        | Global warming potential of the methane |
| <b>Source of data</b>     | IPCC, The Second Assessment Report      |
| <b>Value(s) applied</b>   | 21, as specified in the methodology     |
| <b>Purpose of data</b>    | Project                                 |
| <b>Additional comment</b> | N/A                                     |

|                           |  |
|---------------------------|--|
| <b>Data / Parameter</b>   | <b><math>Reg_{NO_x}</math></b>   |
| <b>Unit</b>               | tNO <sub>x</sub> /m <sup>3</sup>   |
| <b>Description</b>        | National regulation on NO <sub>x</sub> emissions to be checked and applied   |
| <b>Source of data</b>     | National environmental legislation in the Republic of Korea  |
| <b>Value(s) applied</b>   | 2.92 * 10 <sup>-7</sup> (tNO <sub>x</sub> /m <sup>3</sup> )<br>Clean Air Conservation Act of the Republic of Korea<br>Currently, NO <sub>x</sub> regulation requires limiting the emissions below 200 ppmv.  |
| <b>Purpose of data</b>    | Baseline   |
| <b>Additional comment</b> | In Hanwha Onsan plant, NO/NO <sub>2</sub> ratio of the tail gas before NH <sub>3</sub> SCR installation was 2.1 : 1. But after NH <sub>3</sub> SCR installation, NO/NO <sub>2</sub> average ratio has been 4.9 : 1.<br>Therefore, NO <sub>x</sub> 200ppmv equals to NO 166ppmv plus NO <sub>2</sub> 34ppmv.<br>NO 166ppmv is 2.22 * 10 <sup>-7</sup> tonNO/m <sup>3</sup> and NO <sub>2</sub> 34ppmv is 0.70 * 10 <sup>-7</sup> tonNO <sub>2</sub> /m <sup>3</sup> .<br>And the Sum of NO and NO <sub>2</sub> equals to 2.92 * 10 <sup>-7</sup> tonNO <sub>x</sub> /m <sup>3</sup> . |

|                         |  |
|-------------------------|--|
| <b>Data / Parameter</b> | <b><math>P_{product, max}</math></b>                           |
| <b>Unit</b>             | tHNO <sub>3</sub> /yr  |
| <b>Description</b>      | Design capacity of nitric acid production of the targeted line |
| <b>Source of data</b>   | Manufacturer's specification                                   |
| <b>Value(s) applied</b> | 107,100 tHNO <sub>3</sub> /yr                                  |
| <b>Purpose of data</b>  | Baseline   |



|                           |   |
|---------------------------|---|
| <b>Additional comment</b> | <p>It is in accordance with the methodology.</p> <p>Based on the past record, Hanwha's maximum daily production is 306ton/day, which was recorded in 1992 and maximum operating days is 350day, which was recorded in 2002.</p> <p>Therefore, yearly maximum is as follows;</p> <p>306 [HNO<sub>3</sub>/day]*350[day/yr]</p> <p>The amount of emission reductions is capped by <math>P_{\text{product,max}}</math>.</p> |
|---------------------------|---|

|                           |   |
|---------------------------|---|
| <b>Data / Parameter</b>   | $T_{g,hist}$  |
| <b>Unit</b>               | °C  |
| <b>Description</b>        | Historical operating temperature range of the ammonia oxidation reactor   |
| <b>Source of data</b>     | <p>Production reports</p> <p>Daily average temperature from hourly snapshot data.</p>   |
| <b>Value(s) applied</b>   | <p>867.4–905.2 °C</p> <p>As specified in the methodology, the permitted range of operating temperatures is set based on historical data (Jan.2000-Nov.2003 and Jan.2005-Oct.2006).</p> <p>The lower limit is 2.5% lower value of these available data and the upper limit is 2.5% upper value of them.</p> <p>If the actual average daily operating temperature in the ammonia oxidation reactor (<math>T_g</math>) is outside this “permitted range”, the baseline N<sub>2</sub>O emissions for that period are capped at 4.5kgN<sub>2</sub>O/tonne of nitric acid conservatively applying the IPCC default value.</p> |
| <b>Purpose of data</b>    | Baseline  |
| <b>Additional comment</b> | N/A   |

|                         |   |
|-------------------------|---|
| <b>Data / Parameter</b> | $P_{g,hist}$  |
| <b>Unit</b>             | Pa  |
| <b>Description</b>      | Historical operating pressure range of the ammonia oxidation reactor  |
| <b>Source of data</b>   | <p>Production reports</p> <p>Daily average pressure from hourly snapshot data.</p>  |
| <b>Value(s) applied</b> | <p>8.084-9.780 *10<sup>5</sup> Pa abs</p> <p>(7.071–8.767 *10<sup>5</sup> Pa gauge)</p> <p>Specified in the methodology.</p> <p>The permitted range of operating pressures is set based on historical data (Jan.2000-Nov.2003 and Jan.2005-Oct.2006).</p> <p>Operating pressure is measured at two points. One is between air compressor and NH<sub>3</sub> air mixer (since Jan.2000), and another is between NH<sub>3</sub> air mixer and NH<sub>3</sub> air filter (since Jan.2005). The permitted range is determined based on data measured at the former which the number of acquisition records is larger.</p> <p>The lower limit is 2.5% lower value of these available data and the upper limit is 2.5% upper value of them.</p> <p>If the actual average daily operating pressure in the ammonia oxidation reactor (<math>P_g</math>) is outside this “permitted range”, the baseline N<sub>2</sub>O emissions for that period are capped at 4.5kgN<sub>2</sub>O/tonne of nitric acid conservatively applying the IPCC default value.</p> |
| <b>Purpose of data</b>  | Baseline  |

|                           |  |
|---------------------------|--|
| <b>Additional comment</b> | In order to maintain consistency in the 3 <sup>rd</sup> verification by DOE's instruction, the monitoring report was revised in accordance with the PDD. But, the wrong value was filled out along the way because it differs from the revised monitoring plan. And we applied the wrong data (7.022~8.806 x 105 Pa.g) from the 4th monitoring period. To correct this inconsistency, we apply the right default value (7.071~8.767 x 105 Pa.g on the 4th and 5th monitoring data. Consequently 983 tonnes should be deducted from the 4th monitoring period. But there is no effect on the 5th monitoring period. |
|---------------------------|--|

|                           |   |
|---------------------------|---|
| <b>Data / Parameter</b>   | $G_{sup, hist}$   |
| <b>Unit</b>               | -   |
| <b>Description</b>        | Historical supplier's information of the ammonia oxidization catalyst |
| <b>Source of data</b>     | Ammonia oxidization catalyst supplier                                 |
| <b>Value(s) applied</b>   | Name of the supplier:<br>Johnson Matthey                              |
| <b>Purpose of data</b>    | Baseline  |
| <b>Additional comment</b> | N/A   |

|                           |  |
|---------------------------|--|
| <b>Data / Parameter</b>   | $G_{com, hist}$  |
| <b>Unit</b>               | %  |
| <b>Description</b>        | Historical composition of the ammonia oxidization catalyst |
| <b>Source of data</b>     | Ammonia oxidization catalyst supplier                      |
| <b>Value(s) applied</b>   | Pt: 95%, Rh: 5%  |
| <b>Purpose of data</b>    | Baseline   |
| <b>Additional comment</b> | N/A  |

|                           |  |
|---------------------------|--|
| <b>Data / Parameter</b>   | $SE_{N_2O}$  |
| <b>Unit</b>               | kgN <sub>2</sub> O/tHNO <sub>3</sub>   |
| <b>Description</b>        | N <sub>2</sub> O emission rate per ton of nitric acid  |
| <b>Source of data</b>     | Pre-publication Draft 2006 IPCC Guidelines accepted by the 21 <sup>st</sup> Session of the IPCC  |
| <b>Value(s) applied</b>   | 4.5 kgN <sub>2</sub> O/tHNO <sub>3</sub><br>Specified in the methodology.<br>This value is the conservative IPCC default value of Nitric Acid Plants which is based on the default emission factor for low-pressure plants.<br>(5kgN <sub>2</sub> O/tonne of nitric acid, accounting for 10% uncertainty factor) |
| <b>Purpose of data</b>    | Baseline   |
| <b>Additional comment</b> | N/A  |

|                         |  |
|-------------------------|--|
| <b>Data / Parameter</b> | $A_{OR, hist}$   |
| <b>Unit</b>             | tNH <sub>3</sub> /day  |
| <b>Description</b>      | Maximum of historical ammonia flow rate of the ammonia oxidization reactor |
| <b>Source of data</b>   | Production reports   |

|                           |  |
|---------------------------|--|
| <b>Value(s) applied</b>   | <p>88 tNH<sub>3</sub>/day</p> <p>Specified in the methodology.</p> <p>This is a maximum value of daily ammonia flow rates based on historical data (Jan.2000-Nov.2003 and Jan.2005-Oct.2006).</p> <p>If the daily ammonia input to the oxidation reactor (<math>A_{OR,d}</math>) exceeds maximum historical ammonia input to oxidation reactor (<math>A_{OR,hist}</math>), the baseline of N<sub>2</sub>O emissions for that period are capped at 4.5kgN<sub>2</sub>O/tonne of nitric acid conservatively applying the IPCC default value.</p> |
| <b>Purpose of data</b>    | Baseline   |
| <b>Additional comment</b> | <p>Regarding NH<sub>3</sub> density we were used, it was acknowledged by technology transfer. And now there is no documentary evidence to make it prove. To clarify this issue, we intend to use 0.7708 kg/cm<sup>3</sup> as the density of NH<sub>3</sub> from the Physics handbook. This new value is lower than the before. So, even though this value is to be changed, the CER's volume has no change.</p>  |

|                           |  |
|---------------------------|--|
| <b>Data / Parameter</b>   | $M_i$  |
| <b>Unit</b>               | Hour   |
| <b>Description</b>        | Measuring interval   |
| <b>Source of data</b>     | Defined in the technical specifications of data logging system   |
| <b>Value(s) applied</b>   | <p>1 hour</p> <p>QA/QC procedures will be applied by regular maintenance of the data logging system.</p> |
| <b>Purpose of data</b>    | Baseline, Project  |
| <b>Additional comment</b> | N/A  |

|                           |  |
|---------------------------|--|
| <b>Data / Parameter</b>   | $OXID_{NMHC}$  |
| <b>Unit</b>               | %  |
| <b>Description</b>        | Oxidization factor of the hydrocarbon (Non-methane part of the natural gas)  |
| <b>Source of data</b>     | AM0028 version03   |
| <b>Value(s) applied</b>   | <p>100%</p> <p>Specified in the methodology.</p> <p>For this project, fraction of methane not converted will not be measured due to unreasonable costs, so 100% is applied for this parameter based on AM0028 version03. It is very minor contribution</p> |
| <b>Purpose of data</b>    | Project  |
| <b>Additional comment</b> | N/A  |

|                         |  |
|-------------------------|--|
| <b>Data / Parameter</b> | $OXID_{CH_4}$  |
| <b>Unit</b>             | %  |
| <b>Description</b>      | Oxidization factor of methane (Methane part of the natural gas)  |
| <b>Source of data</b>   | AM0028 version03   |
| <b>Value(s) applied</b> | <p>0%</p> <p>Specified in the methodology.</p> <p>For this project, fraction of methane not converted will not be measured due to unreasonable costs, so 0% is applied for this parameter based on AM0028 version03.</p> |
| <b>Purpose of data</b>  | Project  |



|                           |  |
|---------------------------|--|
| <b>Additional comment</b> | N/A  |
| <b>Data / Parameter</b>   | $EF_{RCS}$   |
| <b>Unit</b>               | tCO <sub>2</sub> e/MWh   |
| <b>Description</b>        | Emission factor of the electricity for running the DeN <sub>2</sub> O unit   |
| <b>Source of data</b>     | 2000~2004 Statistics of electric power in Korea (The Korea Electrical Power Corporation (KEPCO), <a href="http://www.kepco.co.kr">http://www.kepco.co.kr</a> )   |
| <b>Value(s) applied</b>   | 0.62 (tCO <sub>2</sub> e/MWh) for national power grid in the Republic of Korea.<br>The emission factor is referring to baseline emissions factor described in PDD of “Youngduk Wind Park Project” which was already registered as CDM ( <a href="http://cdm.unfccc.int/UserManagement/FileStorage/XH4MZ6TAOURT6745ZMBZEGWQH6QVUS">http://cdm.unfccc.int/UserManagement/FileStorage/XH4MZ6TAOURT6745ZMBZEGWQH6QVUS</a> ).<br>And it is calculated by combined margin (CM) based on data in 2000~2004 shown by source the yearly book of KEPCO 2001~2005.<br>The value is calculated as ACM0002 option 1, ex-ante based.<br>It is very minor contribution. |
| <b>Purpose of data</b>    | Project  |
| <b>Additional comment</b> | N/A  |

**D.2. Data and parameters monitored**

|  |  |
|--|--|
| <b>Data/Parameter</b>                  | $F_{TL,i}$   |
| <b>Unit</b>                            | Nm <sup>3</sup>  |
| <b>Description</b>                     | Volume flow rate at the inlet of the destruction facility  |
| <b>Measured/Calculated/Default</b>     | Measured   |
| <b>Source of data</b>                  | Multiple-point sampling tube type flow meter with Resistance Temperature Detector and D/P Transmitter                          |
| <b>Value(s) of monitored parameter</b> | 163,015,272 Nm <sup>3</sup><br>(total volume from 01/01/2012 to 30/06/2012, from the actual data)<br>Refer to the spread sheet |



|  |  |
|--|--|
| <b>Monitoring equipment</b>                  | <ul style="list-style-type: none"> <li>Type :<br/>Multiple-point sampling tube type flow meter (Maker/Model : Honeywell, STD924-E1H-00000-S2) with Resistance Temperature Detector (Maker/Model : WISE controls, R221+MTM) and Absolute Pressure Transmitter (Maker/Model : Honeywell, STG 944-E1G-00000-S1)</li> <li>Serial Number :<br/>Multiple-point sampling tube type flow meter :<br/>0712 07030214001 (Instrument No. 10-FT-561)<br/>Resistance Temperature Detector : WS-7M139 (Instrument No.10-TT-161)<br/>Absolute Pressure Transmitter : 0712 07030214004(Instrument No. 10-PT-361)</li> <li>Accuracy class : According to the supplier's specification<br/>Multiple-point sampling tube type flow meter : <math>\pm 0.075\%</math> , of full scale<br/>Resistance Temperature Detector : <math>\pm 0.3\%</math> , of full scale<br/>Absolute Pressure Transmitter : <math>\pm 0.065\%</math> , of full scale</li> <li>Calibration frequency : Based on EN14181 and frequency is as below<br/>Multiple-point sampling tube type flow meter : 15 months<br/>Resistance Temperature Detector : 15 months<br/>Absolute Pressure Transmitter : 15 months</li> <li>Date of last calibrations :<br/>Multiple-point sampling tube type flow meter : July 7, 2011<br/>Resistance Temperature Detector : July 15, 2011<br/>Absolute Pressure Transmitter : July 7, 2011</li> <li>Validity :<br/>Multiple-point sampling tube type flow meter : October 6, 2012<br/>Resistance Temperature Detector : October 14, 2012<br/>Absolute Pressure Transmitter : October 6, 2012<br/>Based on EN14181, variability test and validity of the calibration function is annually crosschecked by AST</li> <li>Measuring point : At the tail gas duct before DeN<sub>2</sub>O unit<br/>Measuring range : 0-60,000 Nm<sup>3</sup>/hr</li> </ul> |
| <b>Measuring/Reading/Recording frequency</b> | <ul style="list-style-type: none"> <li>Measuring frequency : Continuously</li> <li>Reading frequency : Continuously</li> <li>Recording frequency : Continuously (Hourly average)</li> </ul>  |
| <b>Calculation method (if applicable)</b>    | N/A  |
| <b>QA/QC procedures</b>                      | <p>Calibration frequency: refer to the above.</p> <p>Both <math>F_{TE}</math> and <math>F_{TI}</math> parameters shall be cross-checked to ensure that no leak of N<sub>2</sub>O is taking place.</p> <p>In case of discrepancy, conservative calculation of emission reduction shall be provided.</p>   |
| <b>Purpose of data</b>                       | Baseline   |
| <b>Additional comment</b>                    | N/A  |

|                       |   |
|-----------------------|---|
| <b>Data/Parameter</b> | $CI_{N_2O,i}$   |
| <b>Unit</b>           | tN <sub>2</sub> O/m <sup>3</sup>                              |
| <b>Description</b>    | N <sub>2</sub> O concentration at destruction facility inlet. |



|  |   |
|--|---|
| <b>Measured/Calculated/Default</b>           | Measured  |
| <b>Source of data</b>                        | Non-dispersion infrared absorption analyzer (NDIR)  |
| <b>Value(s) of monitored parameter</b>       | 3.525415 E-06 tN <sub>2</sub> O/Nm <sup>3</sup> (=1,795 ppmv*44/22.4)<br>(average concentration from 01/01/2012 to 30/06/2012, from the actual data)<br>Refer to the spread sheet   |
| <b>Monitoring equipment</b>                  | <ul style="list-style-type: none"> <li>Type : Non-dispersion infrared absorption analyzer.<br/>(Maker/Model: ABB/ AO2040/Uras26)</li> <li>Serial number : 3.346997.7 (Instrument No. 10-AT-061)</li> <li>Accuracy class : ±0.02% of full scale, according to the supplier's specification</li> <li>Calibration frequency :<br/>QAL2:three years<br/>AST:12 months<br/>QAL3: every 10 days</li> <li>Date of last calibrations :<br/>QAL2: January 17~21, 2011<br/>AST: January 17~18, 2012<br/>QAL3: June 23, 2012<br/>Other QAL3 tests within this monitoring period were conducted every 10 days on average within the validity.</li> <li>Validity :<br/>QAL2:<br/>QAL2 on January 17~21, 2011: valid until January 20, 2014<br/>AST: valid until January 17, 2013<br/>QAL3: valid until July 3, 2012<br/>QAL2/AST/QAL3 were valid throughout this monitoring period from January 1, 2012 to June 30, 2012.<br/>Based on EN14181, variability test and validity of the calibration function is annually crosschecked by AST</li> <li>Measuring point : At the tail gas duct before DeN<sub>2</sub>O unit</li> <li>Measuring range : 0-3,000ppmv</li> </ul> |
| <b>Measuring/Reading/Recording frequency</b> | <ul style="list-style-type: none"> <li>Measuring frequency : Continuously</li> <li>Reading frequency : Continuously</li> <li>Recording frequency : Continuously (Hourly average)</li> </ul>   |
| <b>Calculation method (if applicable)</b>    | Concentration*44/22.4   |
| <b>QA/QC procedures</b>                      | <p>ABB AO2040 Uras26 which is fitted with integral calibration check cell is used. Calibration is done manually and is recorded on the data logging system. The calibration is carried out every 10 days. Calibration is intended to be done by the plant operator with routine procedure for QAL-3 certification of the system.</p> <p>In case Non-dispersion infrared absorption analyzer is used, it shall be checked by gas chromatography periodically.</p> <p>QA/QC for the analyzer shall be subjected to the EN14181 or equivalent standards available in the Republic of Korea.</p>  |
| <b>Purpose of data</b>                       | Baseline  |
| <b>Additional comment</b>                    | N/A   |

|                       |                 |
|-----------------------|-----------------|
| <b>Data/Parameter</b> | $F_{TE,i}$      |
| <b>Unit</b>           | Nm <sup>3</sup> |



|  |  |
|--|--|
| <b>Description</b>                           | Volume flow rate at the exit of gas the destruction facility   |
| <b>Measured/Calculated/Default</b>           | Measured   |
| <b>Source of data</b>                        | Multiple-point sampling tube type flow meter with Resistance Temperature Detector and D/P Transmitter  |
| <b>Value(s) of monitored parameter</b>       | 167,975,214 Nm <sup>3</sup><br>(total volume from 01/01/2012 to 30/06/2012, from the actual data)<br>Refer to the spread sheet   |
| <b>Monitoring equipment</b>                  | <ul style="list-style-type: none"> <li>● Type :<br/>Multiple-point sampling tube type flow meter (Maker/Model : Honeywell, STD924-W1H-00000-S2) with Resistance Temperature Detector (Maker/Model : WISE controls, R221+MTM) and Absolute Pressure Transmitter (Maker/Model : Honeywell, STG 944-E1G-00000-S1)</li> <li>● Serial Number :<br/>Multiple-point sampling tube type flow meter : 0712 07030214002 (Instrument No. 10-FT-562)<br/>Resistance Temperature Detector : WS-7M140 (Instrument No.10-TT-162)<br/>Absolute Pressure Transmitter : 9853 00002001004 (Instrument No. 10-PT-362)</li> <li>● Accuracy class : (according to the supplier's specification)<br/>Multiple-point sampling tube type flow meter : <math>\pm 0.075\%</math> , of full scale<br/>Resistance Temperature Detector : <math>\pm 0.3\%</math> , of full scale<br/>Absolute Pressure Transmitter : <math>\pm 0.065\%</math> , of full scale</li> <li>● Calibration frequency : Based on EN14181 and frequency is as below<br/>Multiple-point sampling tube type flow meter: 15 months<br/>Resistance Temperature Detector : 15 months<br/>D/P Transmitter : 15 months</li> <li>● Date of last calibrations :<br/>Multiple-point sampling tube type flow meter : July 7, 2011<br/>Resistance Temperature Detector : and July 8, 2011<br/>D/P Transmitter : and July 7, 2011</li> <li>● Validity :<br/>Multiple-point sampling tube type flow meter : October 6, 2012<br/>Resistance Temperature Detector : October 7, 2012<br/>Absolute Pressure Transmitter : October 6, 2012<br/>Based on EN14181, variability test and validity of the calibration function is annually crosschecked by AST</li> <li>● Measuring point : At the tail gas duct after DeN<sub>2</sub>O unit</li> <li>● Measuring range : 0-60,000 Nm<sup>3</sup>/hr</li> </ul> |
| <b>Measuring/Reading/Recording frequency</b> | <ul style="list-style-type: none"> <li>● Measuring frequency : Continuously</li> <li>● Reading frequency : Continuously</li> <li>● Recording frequency : Continuously (Hourly average)</li> </ul>  |
| <b>Calculation method (if applicable)</b>    | N/A  |
| <b>QA/QC procedures</b>                      | <p>Calibration frequency: refer to the above.</p> <p>Both <math>F_{TE}</math> and <math>F_{TI}</math> parameters shall be cross-checked to ensure that no leak of N<sub>2</sub>O is taking place.</p> <p>In case of discrepancy, conservative calculation of emission reduction shall be provided.</p>   |



|  |  |
|--|--|
| <b>Purpose of data</b>                       | Project  |
| <b>Additional comment</b>                    | N/A  |
| <b>Data/Parameter</b>                        | $CO_{N_2O,i}$  |
| <b>Unit</b>                                  | tN <sub>2</sub> O/Nm <sup>3</sup>  |
| <b>Description</b>                           | N <sub>2</sub> O concentration at destruction facility outlet.   |
| <b>Measured/Calculated/Default</b>           | Measured   |
| <b>Source of data</b>                        | Non-dispersion infrared absorption analyzer (NDIR)   |
| <b>Value(s) of monitored parameter</b>       | 4.057487 E-07 tN <sub>2</sub> O/Nm <sup>3</sup> (=207 ppmv*44/22.4)<br>(average concentration from 01/01/2012 to 30/06/2012, from the actual data)<br>Refer to the spread sheet  |
| <b>Monitoring equipment</b>                  | <ul style="list-style-type: none"> <li>Type : Non-dispersion infrared absorption analyzer : Maker/Model: ABB/AO2040/Uras26)</li> <li>Serial number : 3.346996.7 (Instrument No. 10-AT-062)</li> <li>Accuracy class : ±0.02% of full scale, according to the supplier's specification</li> <li>Calibration frequency :<br/>QAL2:three years<br/>AST:12 months<br/>QAL3: every 10 days</li> <li>Date of last calibrations :<br/>QAL2: January 17~21, 2011 -<br/>AST: January 17~18, 2012 -<br/>QAL3: June 23, 2012<br/>Other QAL3 tests within this monitoring period were conducted every 10 days on average within the validity.</li> <li>Validity :<br/>QAL2:<br/>-<br/>QAL2 on January 17~21, 2011: valid until January 20, 2014<br/>AST: valid until January 17, 2013<br/>QAL3:valid until July 3, 2012<br/>QAL2/AST/QAL3 were valid throughout this monitoring period from January 1, 2012 to June 30, 2012.<br/>Based on EN14181, variability test and validity of the calibration function is annually crosschecked by AST</li> <li>Measuring point : At the tail gas duct after DeN<sub>2</sub>O unit</li> <li>Measuring range : 0-500ppmv</li> </ul> |
| <b>Measuring/Reading/Recording frequency</b> | <ul style="list-style-type: none"> <li>Measuring frequency : Continuously</li> <li>Reading frequency : Continuously</li> <li>Recording frequency : Continuously(Hourly average)</li> </ul>   |
| <b>Calculation method (if applicable)</b>    | Concentration*44/22.4  |





|                           |   |
|---------------------------|---|
| <b>QA/QC procedures</b>   | <p>ABB AO2040 Uras26 which is fitted with integral calibration check cell is used. Calibration is done manually and will be recorded on the data logging system. The calibration is carried out every 10 days. Calibration is intended to be done by the plant operator with routine procedure for QAL-3 certification of the system.</p> <p>In case Non-dispersion infrared absorption analyzer is used, it shall be checked by gas chromatography periodically.</p> <p>QA/QC for the analyzer shall be subjected to the EN14181 or equivalent standards available in the Republic of Korea.</p> |
| <b>Purpose of data</b>    | Project   |
| <b>Additional comment</b> | N/A   |

|  |  |
|--|--|
| <b>Data/Parameter</b>                        | $P_{\text{product},y}$   |
| <b>Unit</b>                                  | tHNO <sub>3</sub>  |
| <b>Description</b>                           | Plant output of HNO <sub>3</sub> .   |
| <b>Measured/Calculated/Default</b>           | Measured   |
| <b>Source of data</b>                        | magnetic flow meter  |
| <b>Value(s) of monitored parameter</b>       | <p>52,013.84tHNO<sub>3</sub></p> <p>(total volume from 01/01/2012 to 30/06/2012, from the actual data)</p> <p>Refer to Annex-2, item-5 of the monitoring report and also the spread sheet</p>  |
| <b>Monitoring equipment</b>                  | <ul style="list-style-type: none"> <li>● Type : Magnetic flow meter(Maker/Model : Rosemount/Emerson/8705TPA020S1W0N0G3B3Q4)</li> <li>● Serial number : 06011102 (Instrument No. 10-FT-512)</li> <li>● Accuracy class : <math>\pm 0.5\%</math> and <math>\pm 0.675\%</math> of full scale, according to the supplier's specification</li> <li>● Calibration frequency : 15 months</li> <li>● Date of last calibrations : June 29, 2011</li> <li>● Validity : September 28, 2012</li> <li>● Measuring point : At the product line before storage tanks</li> <li>● Measuring range : 0-20 m<sup>3</sup>/hr</li> </ul> |
| <b>Measuring/Reading/Recording frequency</b> | <ul style="list-style-type: none"> <li>● Measuring frequency : Continuously</li> <li>● Reading frequency : Continuously</li> <li>● Recording frequency : Continuously(Hourly average)</li> </ul>   |
| <b>Calculation method (if applicable)</b>    | <p>Refer to Annex-2, item 5. This parameter is calculated as follows :</p> $P_{\text{product},y} = Q_{\text{HNO}_3} * CH_{\text{HNO}_3} / 100 * DH_{\text{HNO}_3}$ <p>Where:</p> <p><math>Q_{\text{HNO}_3}</math> : Total flow rate of produced nitric acid monitored (not converted to 100% base) in a year y (m<sup>3</sup>)</p> <p><math>CH_{\text{HNO}_3}</math> : Average mass concentration of produced nitric acid (not pure) (%)</p> <p><math>DH_{\text{HNO}_3}</math> : Average density of produced nitric acid (not pure) (t/ m<sup>3</sup>)</p>   |
| <b>QA/QC procedures</b>                      | Cross – check of production, marketing and stock change data. Measurement devices such as weighbridge can be subjected to QA /QC scheme consistent with the procedures in $T_g$ , $P_g$ , $F_{\text{TL},i}$ , $F_{\text{TE},i}$ , $C_{\text{ON}_2\text{O},i}$ , $CI_{\text{N}_2\text{O},i}$ , $M_i$ , $Q_{\text{HC},y}$ and $SE_{\text{N}_2\text{O}}$ , with respect to equipment certification, installation and performance.   |
| <b>Purpose of data</b>                       | Baseline   |
| <b>Additional comment</b>                    | N/A  |

|                       |       |
|-----------------------|-------|
| <b>Data/Parameter</b> | $T_g$ |
|-----------------------|-------|



|  |   |
|--|---|
| <b>Unit</b>                                  | °C  |
| <b>Description</b>                           | Actual operating temperature of the ammonia oxidation reactor   |
| <b>Measured/Calculated/Default</b>           | Measured  |
| <b>Source of data</b>                        | Thermo-couple (Type “R”)  |
| <b>Value(s) of monitored parameter</b>       | Maximum temperature : 903.67 °C (June 30, 2012)<br>Minimum temperature : 887.03 °C (January 13, 2012)<br>** Permitted range : 867.4-905.2 °C<br>Refer to the spread sheet and default data  |
| <b>Monitoring equipment</b>                  | <ul style="list-style-type: none"> <li>● Type : Thermocouple (Maker/Model : YOKOGAWA/YTA 110)</li> <li>● Serial number : C2E104013502 (Instrument No. 10-TT-115)</li> <li>● Accuracy class : <math>\pm 1.5</math> deg C of full scale, according to the supplier’s specification</li> <li>● Calibration frequency : 15 months</li> <li>● Date of last calibrations : July 8, 2011</li> <li>● Validity : October 7, 2012</li> <li>● Measuring point : At the oxidation reactor</li> <li>● Measuring range : 0-1,200°C</li> </ul> |
| <b>Measuring/Reading/Recording frequency</b> | <ul style="list-style-type: none"> <li>● Measuring frequency : Continuously</li> <li>● Reading frequency : Continuously</li> <li>● Recording frequency : Continuously (Hourly average)</li> </ul>   |
| <b>Calculation method (if applicable)</b>    | If the average daily operating temperature in the ammonia oxidation reactor ( $T_g$ ) is outside the permitted range ( $T_{g,hist}$ ), the baseline $N_2O$ emission for that period are capped at 4.5kg $N_2O$ /tonne of nitric acid conservatively applying the IPCC default value.  |
| <b>QA/QC procedures</b>                      | Hanwha’s maintenance and testing regime including calibration based on the vendor requirement.  |
| <b>Purpose of data</b>                       | Baseline  |
| <b>Additional comment</b>                    | N/A   |

|  |   |
|--|---|
| <b>Data/Parameter</b>                  | $P_g$   |
| <b>Unit</b>                            | Pa  |
| <b>Description</b>                     | Actual operating pressure ammonia of the oxidation reactor  |
| <b>Measured/Calculated/Default</b>     | Measured  |
| <b>Source of data</b>                  | Pressure transmitter  |
| <b>Value(s) of monitored parameter</b> | Maximum pressure : 843,308.12 Pa.g (March 7, 2012) = $(8.43 * 10^5 \text{ Pa gauge})$<br>Minimum pressure : 720,273.12 Pa.g (March 02, 2012) = $(7.20 * 10^5 \text{ Pa gauge})$<br>** Permitted range : $8.084\text{--}9.780 * 10^5 \text{ Pa abs}$ ( $7.071\text{--}8.767 * 10^5 \text{ Pa gauge}$ )<br>Refer to the spread sheet and default data |



|  |   |
|--|---|
| <b>Monitoring equipment</b>                  | <ul style="list-style-type: none"> <li>Type : Pressure transmitter (Maker/Model : Honeywell/STG 944-E1G-00000-S1)</li> <li>Serial number : 0729 07062904012 (Instrument No. 10-PT-304)</li> <li>Accuracy class : <math>\pm 0.065\%</math> of full scale, according to the supplier's specification</li> <li>Calibration frequency : 15 months</li> <li>Date of last calibrations : July 7, 2011</li> <li>Validity : October 6, 2012</li> <li>Measuring point : two points, one is between air compressor and <math>\text{NH}_3</math> air mixer (since Jan.2000) and another is between <math>\text{NH}_3</math> air mixer and <math>\text{NH}_3</math> air filter (since Jan.2005). <math>P_{g,hist}</math> is based on data measured at the former which the number of acquisition record is larger.</li> <li>Measuring range : 0-16 bar gauge</li> </ul> |
| <b>Measuring/Reading/Recording frequency</b> | <ul style="list-style-type: none"> <li>Measuring frequency : Continuously</li> <li>Reading frequency : Continuously</li> <li>Recording frequency : Continuously (Hourly average)</li> </ul>   |
| <b>Calculation method (if applicable)</b>    | If the average daily operating pressure in the ammonia oxidation reactor ( $P_g$ ) is outside the permitted range ( $P_{g,hist}$ ), the baseline $\text{N}_2\text{O}$ emission for that period are capped at $4.5\text{kgN}_2\text{O/tonne}$ of nitric acid conservatively applying the IPCC default value.   |
| <b>QA/QC procedures</b>                      | Hanwha's maintenance and testing regime including calibration based on the vendor requirement.  |
| <b>Purpose of data</b>                       | Baseline  |
| <b>Additional comment</b>                    | N/A   |

|  |  |
|--|--|
| <b>Data/Parameter</b>                        | $G_{sup}$  |
| <b>Unit</b>                                  | -  |
| <b>Description</b>                           | Supplier's information of the ammonia oxidization catalyst |
| <b>Measured/Calculated/Default</b>           | Measured   |
| <b>Source of data</b>                        | Ammonia oxidization catalyst supplier                      |
| <b>Value(s) of monitored parameter</b>       | Name of supplier: Johnson Matthey                          |
| <b>Monitoring equipment</b>                  | N/A  |
| <b>Measuring/Reading/Recording frequency</b> | During the monitoring period                               |
| <b>Calculation method (if applicable)</b>    | N/A  |
| <b>QA/QC procedures</b>                      | Not needed   |
| <b>Purpose of data</b>                       | Baseline   |
| <b>Additional comment</b>                    | N/A  |

|                                    |   |
|------------------------------------|---|
| <b>Data/Parameter</b>              | $G_{com}$                                       |
| <b>Unit</b>                        | %   |
| <b>Description</b>                 | Composition of the ammonia oxidization catalyst |
| <b>Measured/Calculated/Default</b> | Measured  |



|  |   |
|--|---|
| <b>Source of data</b>                        | Ammonia oxidization catalyst supplier   |
| <b>Value(s) of monitored parameter</b>       | Pt: 95 %, Rh: 5 %<br>Hanwha has been using the Pt 95%, Rh 5% catalyst of Johnson Matthey. Hanwha uses the catalyst which is common practice in the region and supplied by a reputable manufacturer or which composition is reported as being in use in the relevant literature. |
| <b>Monitoring equipment</b>                  | N/A   |
| <b>Measuring/Reading/Recording frequency</b> | During the monitoring period  |
| <b>Calculation method (if applicable)</b>    | N/A   |
| <b>QA/QC procedures</b>                      | Not needed  |
| <b>Purpose of data</b>                       | Baseline  |
| <b>Additional comment</b>                    | N/A   |

|  |  |
|--|--|
| <b>Data/Parameter</b>                  | $A_{OR,d}$   |
| <b>Unit</b>                            | tNH <sub>3</sub> /day  |
| <b>Description</b>                     | Actual ammonia flow rate to the ammonia oxidation reactor  |
| <b>Measured/Calculated/Default</b>     | Measured   |
| <b>Source of data</b>                  | Orifice flow meter and differential pressure transmitter   |
| <b>Value(s) of monitored parameter</b> | Maximum flow rate : 87.47 tNH <sub>3</sub> /day (March 14, 2012)<br>Minimum flow rate : 70.90 tNH <sub>3</sub> /day (February 13, 2012)<br>** Permitted range : 88 tNH <sub>3</sub> /day maximum<br>Refer to the spread sheet and default data |

|  |  |
|--|--|
| <b>Monitoring equipment</b>                  | <ul style="list-style-type: none"> <li>Type : Orifice flow meter and differential pressure transmitter (Maker/Model : Rosemount/Emerson, 3051CD2A02A1AM5E5S5Q4) with Resistance Temperature Detector (Maker/Model : WISE controls, R221) and Absolute Pressure Transmitter (Maker/Model : Rosemount/Emerson, 3051TG3A2B21AB4E5M5Q4)</li> <li>Serial number :<br/>Orifice flow meter and differential pressure transmitter : 01564836 (Instrument No. 10-FT-502)<br/>Resistance Temperature Detector : 04014993 (Instrument No. 10-TT-102)<br/>Absolute Pressure Transmitter : 01624987 (Instrument No. 10-PT-302)</li> <li>Accuracy class : according to the supplier's specification<br/>Orifice flow meter and differential pressure transmitter: <math>\pm 0.10\%</math> of full scale<br/>Resistance Temperature Detector : <math>\pm 0.55</math> deg C<br/>Absolute Pressure Transmitter : <math>\pm 0.065\%</math> of full scale</li> <li>Calibration frequency : 15 months</li> <li>Date of last calibrations :<br/>Orifice flow meter and differential pressure transmitter: July 7, 2011<br/>Resistance Temperature Detector : July 8, 2011<br/>Absolute Pressure Transmitter: July 7, 2011</li> <li>Validity :<br/>Orifice flow meter and differential pressure transmitter: October 6, 2012<br/>Resistance Temperature Detector : October 7, 2012<br/>Absolute Pressure Transmitter : October 6, 2012</li> <li>Measuring point : NH<sub>3</sub> air mixer</li> <li>Measuring range : 0-6,000 Nm<sup>3</sup>/hr</li> </ul> |
| <b>Measuring/Reading/Recording frequency</b> | <ul style="list-style-type: none"> <li>Measuring frequency : Continuously</li> <li>Reading frequency : Continuously</li> <li>Recording frequency : Continuously (Hourly average)</li> </ul>  |
| <b>Calculation method (if applicable)</b>    | If the daily ammonia input to oxidation reactor ( $A_{OR,d}$ ) exceeds maximum historical ammonia input to oxidation reactor ( $A_{OR,hist}$ ), the baseline N <sub>2</sub> O emissions for that period are capped at 4.5kg N <sub>2</sub> O/tonne of nitric acid conservatively applying the IPCC default value.  |
| <b>QA/QC procedures</b>                      | Hanwha's maintenance and testing regime including calibration based on the vendor requirement.   |
| <b>Purpose of data</b>                       | Baseline   |
| <b>Additional comment</b>                    | N/A  |

|  |  |
|--|--|
| <b>Data/Parameter</b>                  | $EI_{RCS,y}$   |
| <b>Unit</b>                            | MWh/yr   |
| <b>Description</b>                     | Additional electricity input for running the DeN <sub>2</sub> O unit |
| <b>Measured/Calculated/Default</b>     | Measured   |
| <b>Source of data</b>                  | Wattmeter or electricity accumulator                                 |
| <b>Value(s) of monitored parameter</b> | 170,844KWh (01/01/2012-30/06/2012)<br>Refer to the spread sheet      |



|  |  |
|--|--|
| <b>Monitoring equipment</b>                  | <ul style="list-style-type: none"> <li>Type : (Maker/Model : LS Industrial System/WL32STE, LD3310CP-005-TES )</li> <li>Serial number : 0297218</li> <li>Accuracy class : 1.0 grade</li> <li>Calibration frequency : 15 months</li> <li>Date of last calibrations : August 23, 2011</li> <li>Validity : November 22, 2012</li> <li>Measuring point : At the control panel of DeNO2 Unit</li> <li>Measuring range : 3,000 rev/kWh, 10,000 Pulse/kWh</li> </ul> |
| <b>Measuring/Reading/Recording frequency</b> | <ul style="list-style-type: none"> <li>Measuring frequency : Continuously</li> <li>Reading frequency : Continuously</li> <li>Recording frequency : Daily</li> </ul>  |
| <b>Calculation method (if applicable)</b>    | N/A  |
| <b>QA/QC procedures</b>                      | Instead of calibration, it is replaced by certified new one before to be finished its validity.  |
| <b>Purpose of data</b>                       | Leakage  |
| <b>Additional comment</b>                    | N/A  |

|  |  |
|--|--|
| <b>Data/Parameter</b>                        | $Q_{NG,y}$   |
| <b>Unit</b>                                  | Nm <sup>3</sup>  |
| <b>Description</b>                           | Hydrocarbon (natural gas) input  |
| <b>Measured/Calculated/Default</b>           | Measured   |
| <b>Source of data</b>                        | Integral Orifice meter with temperature, pressure compensation   |
| <b>Value(s) of monitored parameter</b>       | 89,202.70 Nm <sup>3</sup> (01/01/2012-30/06/2012)<br>Refer to the spread sheet   |
| <b>Monitoring equipment</b>                  | <ul style="list-style-type: none"> <li>Type : Differential pressure transmitter with pressure,/temperature application for compensation(Maker/Model : Rosemount/Emerson, 3095MFCCS020N040T32BA1AQ4I5M5)</li> <li>Serial number : 02357885 (Insrtument No. 10-FT-563)</li> <li>Accuracy class : <math>\pm 1.00809\%</math>, <math>\pm 0.78\%</math> of full scale, according to the supplier's specification</li> <li>Calibration frequency : 15 months,</li> <li>Date of last calibrations : May 12, 2011</li> <li>Validity : August 11, 2012</li> <li>Measuring point : At the Burner Inlet of DeN2O unit</li> <li>Measuring range : 0~100 Nm<sup>3</sup>/hr</li> </ul> |
| <b>Measuring/Reading/Recording frequency</b> | <ul style="list-style-type: none"> <li>Measuring frequency : Continuously</li> <li>Reading frequency : Continuously</li> <li>Recording frequency : Continuously (Hourly average)</li> </ul>  |
| <b>Calculation method (if applicable)</b>    | N/A  |
| <b>QA/QC procedures</b>                      | Hanwha's maintenance and testing regime including calibration based on the vendor requirement.   |
| <b>Purpose of data</b>                       | Project  |
| <b>Additional comment</b>                    | N/A  |

|                       |           |
|-----------------------|-----------|
| <b>Data/Parameter</b> | $C_{HNC}$ |
|-----------------------|-----------|



|  |   |
|--|---|
| <b>Unit</b>                                  | %   |
| <b>Description</b>                           | Methane content of hydrocarbon (natural gas)  |
| <b>Measured/Calculated/Default</b>           | Measured  |
| <b>Source of data</b>                        | Hydrocarbon supplier  |
| <b>Value(s) of monitored parameter</b>       | 91.525091 %   |
| <b>Monitoring equipment</b>                  | Data from local supplier, Kyungdong City Gas Corporation  |
| <b>Measuring/Reading/Recording frequency</b> | <ul style="list-style-type: none"> <li>● Measuring frequency : Monthly</li> <li>● Reading frequency : N/A</li> <li>● Recording frequency : N/A</li> </ul> |
| <b>Calculation method (if applicable)</b>    | N/A   |
| <b>QA/QC procedures</b>                      | N/A   |
| <b>Purpose of data</b>                       | Project   |
| <b>Additional comment</b>                    | N/A   |

|  |   |
|--|---|
| <b>Data/Parameter</b>                        | $Q_{NMHC,y}$  |
| <b>Unit</b>                                  | Nm <sup>3</sup>   |
| <b>Description</b>                           | Hydrocarbon (Non-methane part of the natural gas) input                                 |
| <b>Measured/Calculated/Default</b>           | Calculated  |
| <b>Source of data</b>                        | Calculated by the flow rate and the methane content of the natural gas                  |
| <b>Value(s) of monitored parameter</b>       | 7,559.85 Nm <sup>3</sup>  |
| <b>Monitoring equipment</b>                  | N/A   |
| <b>Measuring/Reading/Recording frequency</b> | N/A   |
| <b>Calculation method (if applicable)</b>    | This parameter is calculated as follows;<br>$Q_{NMHC,y} = Q_{NG,y} * (1 - C_{HNC}/100)$ |
| <b>QA/QC procedures</b>                      | N/A   |
| <b>Purpose of data</b>                       | Project   |
| <b>Additional comment</b>                    | N/A   |

|  |  |
|--|--|
| <b>Data/Parameter</b>                  | $Q_{HNC,y}$  |
| <b>Unit</b>                            | Nm <sup>3</sup>  |
| <b>Description</b>                     | Methane (Methane part of the natural gas) used                         |
| <b>Measured/Calculated/Default</b>     | Calculated   |
| <b>Source of data</b>                  | Calculated by the flow rate and the methane content of the natural gas |
| <b>Value(s) of monitored parameter</b> | 81,642.85 Nm <sup>3</sup>  |



|  |  |
|--|--|
| <b>Monitoring equipment</b>                  | N/A  |
| <b>Measuring/Reading/Recording frequency</b> | N/A  |
| <b>Calculation method (if applicable)</b>    | This parameter is calculated as follows;<br>$Q_{HNC,y} = Q_{NG,y} * C_{HNC} / 100$ $\{89,202.70 * (91.525091/100)\}$ |
| <b>QA/QC procedures</b>                      | N/A  |
| <b>Purpose of data</b>                       | Project  |
| <b>Additional comment</b>                    | N/A  |

|  |   |
|--|---|
| <b>Data/Parameter</b>                        | $\rho_{NG}$   |
| <b>Unit</b>                                  | t/Nm <sup>3</sup>   |
| <b>Description</b>                           | Density of the hydrocarbon (natural gas).   |
| <b>Measured/Calculated/Default</b>           | Measured  |
| <b>Source of data</b>                        | Hydrocarbon supplier  |
| <b>Value(s) of monitored parameter</b>       | 0.0007965 t/Nm <sup>3</sup>   |
| <b>Monitoring equipment</b>                  | Data from local supplier, Kyungdong City Gas Corporation  |
| <b>Measuring/Reading/Recording frequency</b> | <ul style="list-style-type: none"> <li>● Measuring frequency : Monthly</li> <li>● Reading frequency : N/A</li> <li>● Recording frequency : N/A</li> </ul> |
| <b>Calculation method (if applicable)</b>    | N/A   |
| <b>QA/QC procedures</b>                      | N/A   |
| <b>Purpose of data</b>                       | Project   |
| <b>Additional comment</b>                    | N/A   |

|  |   |
|--|---|
| <b>Data/Parameter</b>                        | $\rho_{HNC}$  |
| <b>Unit</b>                                  | t/Nm <sup>3</sup>   |
| <b>Description</b>                           | Density of the hydrocarbon (Methane part of the natural gas).   |
| <b>Measured/Calculated/Default</b>           | Calculated  |
| <b>Source of data</b>                        | Theoretical calculation   |
| <b>Value(s) of monitored parameter</b>       | 0.000714 t/Nm <sup>3</sup>  |
| <b>Monitoring equipment</b>                  | N/A   |
| <b>Measuring/Reading/Recording frequency</b> | N/A   |
| <b>Calculation method (if applicable)</b>    | 0.000714 t/Nm <sup>3</sup> (=16gCH <sub>4</sub> /22.4)<br>This parameter is shown by the density in normal condition (0 °C, 1atm) |
| <b>QA/QC procedures</b>                      | N/A   |
| <b>Purpose of data</b>                       | Project   |
| <b>Additional comment</b>                    | N/A   |



|  |  |
|--|--|
| <b>Data/Parameter</b>                        | $\rho_{\text{NMHC}}$   |
| <b>Unit</b>                                  | t/Nm <sup>3</sup>  |
| <b>Description</b>                           | Density of the hydrocarbon (Non-methane part of the natural gas).  |
| <b>Measured/Calculated/Default</b>           | Calculated   |
| <b>Source of data</b>                        | Calculated by data of the natural gas and methane  |
| <b>Value(s) of monitored parameter</b>       | 0.001687462 t/Nm <sup>3</sup>  |
| <b>Monitoring equipment</b>                  | N/A  |
| <b>Measuring/Reading/Recording frequency</b> | N/A  |
| <b>Calculation method (if applicable)</b>    | This parameter is calculated as follows;<br>$\rho_{\text{NMHC}} = (\rho_{\text{NG}} - \rho_{\text{HNC}} * C_{\text{HNC}}/100) / (1 - (C_{\text{HNC}}/100))$ $(0.0007965 - 0.000714 * 0.91525091) / (1 - 0.91525091)$ |
| <b>QA/QC procedures</b>                      | N/A  |
| <b>Purpose of data</b>                       | Project  |
| <b>Additional comment</b>                    | N/A  |

|  |   |
|--|---|
| <b>Data/Parameter</b>                        | $NCV_{\text{NG}}$   |
| <b>Unit</b>                                  | Kcal/Nm <sup>3</sup>  |
| <b>Description</b>                           | Net calorific value of the natural gas  |
| <b>Measured/Calculated/Default</b>           | Measured  |
| <b>Source of data</b>                        | Hydrocarbon supplier  |
| <b>Value(s) of monitored parameter</b>       | 10,404.03 kcal/Nm <sup>3</sup>  |
| <b>Monitoring equipment</b>                  | N/A   |
| <b>Measuring/Reading/Recording frequency</b> | <ul style="list-style-type: none"> <li>● Measuring frequency : Monthly</li> <li>● Reading frequency : N/A</li> <li>● Recording frequency : N/A</li> </ul> |
| <b>Calculation method (if applicable)</b>    | N/A   |
| <b>QA/QC procedures</b>                      | N/A   |
| <b>Purpose of data</b>                       | Project   |
| <b>Additional comment</b>                    | N/A   |

|                                    |  |
|------------------------------------|--|
| <b>Data/Parameter</b>              | $EF_{\text{NG}}$   |
| <b>Unit</b>                        | tCO <sub>2</sub> /tNG  |
| <b>Description</b>                 | Emission factor of the hydrocarbon   |
| <b>Measured/Calculated/Default</b> | Calculated   |
| <b>Source of data</b>              | IPCC 2006 GHG Inventory Guidelines and data provided by the natural gas supplier |



|  |  |
|--|--|
| <b>Value(s) of monitored parameter</b>       | 3.067489525 tCO <sub>2</sub> /tNG  |
| <b>Monitoring equipment</b>                  | N/A  |
| <b>Measuring/Reading/Recording frequency</b> | N/A  |
| <b>Calculation method (if applicable)</b>    | This parameter is calculated as follows;<br><br>$EF_{NG} = COEF_{NG} * 44/12 * NCV_{NG} * 4.18605 / \rho_{NG} * 10^{-9}$ where<br>$COEF_{NG}$ : Hydrocarbon emission factor [tCO <sub>2</sub> /TJ]<br>56.1[tCO <sub>2</sub> /TJ] by IPCC 2006 GHG Inventory Guidelines<br>( 56.1 x 10404.03 x 4.18605 / 0.0007965 x 10 <sup>-9</sup> ) |
| <b>QA/QC procedures</b>                      | N/A  |
| <b>Purpose of data</b>                       | Project  |
| <b>Additional comment</b>                    | N/A  |

|  |  |
|--|--|
| <b>Data/Parameter</b>                        | $EF_{HNC}$   |
| <b>Unit</b>                                  | tCO <sub>2</sub> /tCH <sub>4</sub>   |
| <b>Description</b>                           | Emission factor of methane   |
| <b>Measured/Calculated/Default</b>           | Calculated   |
| <b>Source of data</b>                        | Theoretical calculation  |
| <b>Value(s) of monitored parameter</b>       | 2.75(tCO <sub>2</sub> /tCH <sub>4</sub> )  |
| <b>Monitoring equipment</b>                  | N/A  |
| <b>Measuring/Reading/Recording frequency</b> | N/A  |
| <b>Calculation method (if applicable)</b>    | 2.75(tCO <sub>2</sub> /tCH <sub>4</sub> )<br>=(44 gCO <sub>2</sub> /16gCH <sub>4</sub> ) |
| <b>QA/QC procedures</b>                      | N/A  |
| <b>Purpose of data</b>                       | Project  |
| <b>Additional comment</b>                    | N/A  |

|  |  |
|--|--|
| <b>Data/Parameter</b>                        | $EF_{NMHC}$  |
| <b>Unit</b>                                  | tCO <sub>2</sub> /tNMHC  |
| <b>Description</b>                           | Emission factor of hydrocarbon (Non-methane part of the natural gas) |
| <b>Measured/Calculated/Default</b>           | Calculated   |
| <b>Source of data</b>                        | Calculated by data of the natural gas and methane                    |
| <b>Value(s) of monitored parameter</b>       | 4.51826tCO <sub>2</sub> /tNMHC                                       |
| <b>Monitoring equipment</b>                  | N/A  |
| <b>Measuring/Reading/Recording frequency</b> | N/A  |



|   |   |
|---|---|
| <b>Calculation method (if applicable)</b> | This parameter is calculated as follows;<br>$EF_{NMHC} = (EF_{NG} * \rho_{NG} - EF_{HNC} * \rho_{HNC} * C_{HNC}/100) / (1 - C_{HNC}/100) / \rho_{NMHC}$ $((56.1 * 10404.03 * 4.18605 / 0.0007965 / 1000000000 * 0.0007965) - (2.75 * 0.000714 * 0.91525091)) / (1 - 0.91525091) / ((0.0007965 - 0.000714 * 0.91525091) / (1 - 0.91525091))$ |
| <b>QA/QC procedures</b>                   | N/A   |
| <b>Purpose of data</b>                    | Project   |
| <b>Additional comment</b>                 | N/A   |

|  |  |
|--|--|
| <b>Data/Parameter</b>                        | <b>Type<sub>HC</sub></b>                                 |
| <b>Unit</b>                                  | -  |
| <b>Description</b>                           | Hydrocarbon (natural gas) supplier information           |
| <b>Measured/Calculated/Default</b>           | Measured   |
| <b>Source of data</b>                        | Hydrocarbon supplier                                     |
| <b>Value(s) of monitored parameter</b>       | Data from local supplier, Kyungdong City Gas Corporation |
| <b>Monitoring equipment</b>                  | N/A  |
| <b>Measuring/Reading/Recording frequency</b> | N/A  |
| <b>Calculation method (if applicable)</b>    | N/A  |
| <b>QA/QC procedures</b>                      | N/A  |
| <b>Purpose of data</b>                       | Project  |
| <b>Additional comment</b>                    | N/A  |

|                                    |   |
|------------------------------------|---|
| <b>Data/Parameter</b>              | <b>QR<sub>N2O,y</sub></b>   |
| <b>Unit</b>                        | tN <sub>2</sub> O   |
| <b>Description</b>                 | Regulation based on annual quantity N <sub>2</sub> O limited  |
| <b>Measured/Calculated/Default</b> | Measured  |
| <b>Source of data</b>              | National environmental legislation in the Republic of Korea<br>In case national regulations concerning N <sub>2</sub> O emissions are implemented during the crediting period, the impact on baseline N <sub>2</sub> O emissions is considered without any delay by adjusting the measured N <sub>2</sub> O emissions at the time the regulation has to be implemented. |

|  |   |
|--|---|
| <b>Value(s) of monitored parameter</b>       | <p>N/A</p> <p>Baseline N<sub>2</sub>O emissions are limited by the absolute quantity of N<sub>2</sub>O emissions given by the regulation.</p> <p>If the measured baseline N<sub>2</sub>O emissions are exceeding the regulatory limit, then measured baseline N<sub>2</sub>O emissions are substituted by the regulatory limit.</p> <p>If, <math>QI_{N_2O,y} &gt; QR_{N_2O,y}</math> then,</p> $BE_{N_2O,y} = QR_{N_2O,y}$ <p>else,</p> $BE_{N_2O,y} = \min \text{ of } [QI_{N_2O,y}, SE_{N_2O,y} * P_{\text{product,max}}]$ <p>where:</p> <p><math>QI_{N_2O,y}</math> : Quantity of N<sub>2</sub>O emissions at the inlet of the destruction facility in year y (tN<sub>2</sub>O)</p> <p><math>QR_{N_2O,y}</math> : Regulatory limit of N<sub>2</sub>O emissions in year y (tN<sub>2</sub>O)</p> <p><math>BE_{N_2O,y}</math> : Baseline emissions of N<sub>2</sub>O in year y (tN<sub>2</sub>O)</p> <p><math>SE_{N_2O,y}</math> : Specific N<sub>2</sub>O emissions per unit of output of nitric acid in year y (tN<sub>2</sub>O/tHNO<sub>3</sub>)</p> <p><math>P_{\text{product,y}}</math> : Production of nitric acid in year y (tHNO<sub>3</sub>)</p> <p>The quantity of N<sub>2</sub>O emissions at the inlet of the N<sub>2</sub>O destruction facility (DF) is calculated based on continuous measurement of the tail gas volume flow rate and the N<sub>2</sub>O concentration at the inlet of the N<sub>2</sub>O destruction facility.</p> |
| <b>Monitoring equipment</b>                  | N/A   |
| <b>Measuring/Reading/Recording frequency</b> | N/A   |
| <b>Calculation method (if applicable)</b>    | N/A   |
| <b>QA/QC procedures</b>                      | N/A   |
| <b>Purpose of data</b>                       | Baseline  |
| <b>Additional comment</b>                    | N/A   |

|                                    |  |
|------------------------------------|--|
| <b>Data/Parameter</b>              | <b><math>RSE_{N_2O,y}</math></b>   |
| <b>Unit</b>                        | tN <sub>2</sub> O/tHNO <sub>3</sub>  |
| <b>Description</b>                 | Regulation based on N <sub>2</sub> O emissions per unit of nitric acid   |
| <b>Measured/Calculated/Default</b> | Measured   |
| <b>Source of data</b>              | <p>National environmental legislation in the Republic of Korea</p> <p>In case national regulations concerning N<sub>2</sub>O emissions are implemented during the crediting period, the impact on baseline N<sub>2</sub>O emissions is considered without any delay by adjusting the measured N<sub>2</sub>O emissions at the time the regulation has to be implemented.</p> |



|  |  |
|--|--|
| <b>Value(s) of monitored parameter</b>       | <p>N/A</p> <p>Regulation setting of a threshold for specific N<sub>2</sub>O emissions per unit of product</p> <p>If, <math>SE_{N_2O,y} &gt; RSE_{N_2O}</math> then,</p> $BE_{N_2O,y} = \min \text{ of } [RSE_{N_2O} * P_{\text{product},y}, SE_{N_2O,y} * P_{\text{product},\max}]$ <p>else,</p> $BE_{N_2O,y} = \min \text{ of } [QI_{N_2O,y}, SE_{N_2O,y} * P_{\text{product},\max}]$ <p>where:</p> <p><math>SE_{N_2O,y}</math> : Specific N<sub>2</sub>O emissions per unit of output of nitric acid in year y (tN<sub>2</sub>O/tHNO<sub>3</sub>)</p> <p><math>RSE_{N_2O}</math> : Regulatory limit of N<sub>2</sub>O emissions per unit of output of nitric acid (tN<sub>2</sub>O/tHNO<sub>3</sub>)</p> <p><math>BE_{N_2O,y}</math> : Baseline emissions of N<sub>2</sub>O in year y (tN<sub>2</sub>O)</p> <p><math>P_{\text{product},y}</math> : Production of nitric acid in year y (tHNO<sub>3</sub>)</p> <p><math>QI_{N_2O,y}</math> : Quantity of N<sub>2</sub>O emissions at the inlet of the destruction facility in year y (tN<sub>2</sub>O)</p> <p>The specific N<sub>2</sub>O emissions per unit of output of nitric acid is defined as:</p> $SE_{N_2O,y} = QI_{N_2O,y} / P_{\text{product},y}$ <p>where:</p> <p><math>SE_{N_2O,y}</math> : Specific N<sub>2</sub>O emissions per unit of output of nitric acid in year y (tN<sub>2</sub>O/tHNO<sub>3</sub>)</p> <p><math>QI_{N_2O,y}</math> : Quantity of N<sub>2</sub>O emissions at the inlet of the destruction facility in year y (tN<sub>2</sub>O)</p> <p><math>P_{\text{product},y}</math> : Production of nitric acid in year y (tHNO<sub>3</sub>)</p> <p>The quantity of N<sub>2</sub>O emissions at the inlet of the N<sub>2</sub>O destruction facility is calculated based on continuous measurement of the tail gas volume flow rate and the N<sub>2</sub>O concentration at the inlet of the N<sub>2</sub>O destruction facility.</p> |
| <b>Monitoring equipment</b>                  | N/A  |
| <b>Measuring/Reading/Recording frequency</b> | N/A  |
| <b>Calculation method (if applicable)</b>    | N/A  |
| <b>QA/QC procedures</b>                      | N/A  |
| <b>Purpose of data</b>                       | Baseline   |
| <b>Additional comment</b>                    | N/A  |

|                                    |  |
|------------------------------------|--|
| <b>Data/Parameter</b>              | $CR_{N_2O,y}$  |
| <b>Unit</b>                        | tN <sub>2</sub> O/m <sup>3</sup>   |
| <b>Description</b>                 | Regulation based on N <sub>2</sub> O concentration in tail gas limited   |
| <b>Measured/Calculated/Default</b> | Measured   |
| <b>Source of data</b>              | <p>National environmental legislation in the Republic of Korea</p> <p>In case national regulations concerning N<sub>2</sub>O emissions are implemented during the crediting period, the impact on baseline N<sub>2</sub>O emissions is considered without any delay by adjusting the measured N<sub>2</sub>O emissions at the time the regulation has to be implemented.</p> |

|  |   |
|--|---|
| <b>Value(s) of monitored parameter</b>       | <p>N/A</p> <p>Regulation setting of a threshold for N<sub>2</sub>O concentration in the tail gas.</p> <p>If, <math>C_{N_2O,y} &gt; CR_{N_2O}</math> then</p> $BE_{N_2O,y} = \sum_{i=1}^n C_{N_2O,i} * [F_{TG,i} * M_i]$ <p>where <math>C_{N_2O,i}</math> is min [<math>C_{N_2O,y}</math>, <math>CR_{N_2O}</math>, and <math>\{(SE_{N_2O,y} * P_{product,max}) / (\sum(F_{TE,i} * M_i))\}</math>]</p> <p>else,</p> $BE_{N_2O,y} = QI_{N_2O,y}$ <p>where:</p> <p><math>C_{N_2O,i}</math> : N<sub>2</sub>O concentration a destruction facility inlet during interval i (tN<sub>2</sub>O/m<sup>3</sup>)</p> <p><math>CR_{N_2O,i}</math> : Regulatory limit for specific N<sub>2</sub>O concentration during interval i (tN<sub>2</sub>O/m<sup>3</sup>)</p> <p><math>BE_{N_2O,y}</math> : Baseline emissions of N<sub>2</sub>O in year y (tN<sub>2</sub>O)</p> <p><math>F_{TE,i}</math> : Volume flow rate at the exit of the destruction facility during interval i (m<sup>3</sup>/h)</p> <p><math>M_i</math> : Length of measuring interval i (h)</p> <p>i : interval</p> <p>n : number of intervals during the year</p> <p><math>QI_{N_2O,y}</math> : Quantity of N<sub>2</sub>O emissions at the inlet of the destruction facility in year y (tN<sub>2</sub>O)</p> <p>The quantity of N<sub>2</sub>O emissions at the inlet of the N<sub>2</sub>O destruction facility is calculated based on continuous measurement of the tail gas volume flow rate and the N<sub>2</sub>O concentration at the inlet of the N<sub>2</sub>O destruction facility.</p> |
| <b>Monitoring equipment</b>                  | N/A   |
| <b>Measuring/Reading/Recording frequency</b> | N/A   |
| <b>Calculation method (if applicable)</b>    | N/A   |
| <b>QA/QC procedures</b>                      | N/A   |
| <b>Purpose of data</b>                       | Baseline  |
| <b>Additional comment</b>                    | N/A   |

### D.3. Implementation of sampling plan

&gt;&gt;

N/A

## SECTION E. Calculation of emission reductions or GHG removals by sinks

### E.1. Calculation of baseline emissions or baseline net GHG removals by sinks

&gt;&gt;

It has been checked that there are no Korean regulation in place that would limit the quality of N<sub>2</sub>O that can be taken into account for the calculation of baseline emissions.

Baseline emissions of the project activity are determined based on the quantity of N<sub>2</sub>O emitted in the baseline scenario, taking national regulations, production levels and operating conditions into consideration. The quantity of N<sub>2</sub>O is determined based on the measurement of the N<sub>2</sub>O at the inlet of DeNOx unit, which results in a conservative estimation of baseline emissions.

Baseline emissions are limited to the design capacity of the nitric acid plant, According to AM0028 version 3, the design capacity is measured in tons of nitric acid per year. The actual nitric acid production in the covered monitoring period does not exceed the design capacity.

$$BE_y = \text{Minimum}(P_{\text{product,max}} P_{\text{product,y}}) / P_{\text{product,y}} * \sum_{i=1}^n [F_{\text{TL},i} * CI_{\text{N}_2\text{O},i} * M_i * GWP_{\text{N}_2\text{O}}]$$

- i : Interval,  
n : Number of intervals during the year (1/yr),  
 $F_{\text{TL},i}$  : Volume flow rate at the inlet of the destruction facility during interval i ( $\text{Nm}^3/\text{h}$ ),  
 $CI_{\text{N}_2\text{O},i}$  :  $\text{N}_2\text{O}$  concentration a destruction facility inlet during interval i ( $\text{tN}_2\text{O}/\text{Nm}^3$ ),  
 $M_i$  : Measuring interval (1 hour)  
 $GWP_{\text{N}_2\text{O}}$  : Global warming potential of  $\text{N}_2\text{O}$ ,  
 $P_{\text{product,max}}$  : Design capacity ( $\text{tHNO}_3/\text{yr}$ ), and  
 $P_{\text{product,y}}$  : Production of nitric acid in a year y ( $\text{tHNO}_3/\text{yr}$ ).

If the actual average daily operating temperature and/or pressure in the ammonia oxidation reactor ( $T_g$  and  $P_g$ ) are outside a “permitted range” of operating temperatures and/or pressures ( $T_{g,\text{hist}}$  and  $P_{g,\text{hist}}$ ), or the daily ammonia input to the oxidation reactor ( $A_{\text{OR},d}$ ) exceeds maximum historical ammonia input to oxidation reactor ( $A_{\text{OR},\text{hist}}$ ), the baseline  $\text{N}_2\text{O}$  emissions for that period are capped at  $4.5\text{kgN}_2\text{O}/\text{tonne}$  of nitric acid conservatively applying the IPCC default value.

Furthermore, as for composition of ammonia oxidation catalyst, the plant operator is allowed to use compositions of ammonia oxidation catalysts that are common practice in the region or have been used in the nitric acid production plant during the last three years without limitation of  $\text{N}_2\text{O}$  baseline emissions.

In case the nitric acid production plant operator wishes to change to a composition not used during the last three years, but is common practice in the region and supplied by a reputable manufacturer, or if it corresponds to a composition that is reported as being in use in the relevant literature, the plant operator is allowed to use these ammonia oxidation catalysts without limitation of  $\text{N}_2\text{O}$  baseline emissions.

In case the nitric acid production plant operator changes the composition of ammonia oxidation catalysts and the composition is not common practice in the region and not reported as being in use in the relevant literature, the project applicant has to demonstrate (either by economic or other arguments) that the choice of the new composition was based on considerations other than an attempt to increase the rate of  $\text{N}_2\text{O}$  production. If the project applicant can demonstrate appropriate and verifiable reasons, the plant operator is allowed to use new ammonia oxidation catalysts without limitation of  $\text{N}_2\text{O}$  baseline emissions.

The first composition of ammonia oxidation catalyst used during the crediting period shall be of the same kind of catalyst composition already in operation in the specific nitric acid production plant. This is to avoid gaming at the beginning of the project activity.

In case the nitric acid production plant operator changes the composition of ammonia oxidation catalysts and the composition is not common practice in the region and not reported as being in use in the relevant literature, and the project applicant cannot demonstrate appropriate and verifiable reasons for this baseline emissions are limited to the maximum specific  $\text{N}_2\text{O}$  emissions of previous periods ( $\text{tN}_2\text{O}/\text{tHNO}_3$ ), documented in the verified monitoring reports.

Required monitoring parameters:

- $G_{sup}$  : Supplier of the ammonia oxidation catalyst
- $G_{sup,hist}$  : Historical supplier of the ammonia oxidation catalyst
- $G_{com}$  : Composition of the ammonia oxidation catalyst
- $G_{com,hist}$  : Historical composition of the ammonia oxidation catalyst
- $SE_{N_2O,y}$ : Specific  $N_2O$  emissions per ton  $HNO_3$  of product of nitric acid in year y ( $tN_2O/tHNO_3$ )

In the event that  $N_2O$  concentrate of outlet of  $DeN_2O$  facility is not within the monitoring range, we apply the IPCC default value for that period.

In the event that the monitoring system is down, the lowest between the conservative default value established in the methodology or the last measured by-product rate (whichever the lower) will be valid and applied for the downtime period for the baseline emission factor, and the highest measured by-product rate during the project activity will be applied for the downtime period for the campaign emission factor.

$$BE_y = \text{Minimum}(P_{\text{product,max}} P_{\text{product,y}}) / P_{\text{product,y}} * \sum_{i=1}^n [F_{Ti,i} * CI_{N_2O,i} * M_i * GWP_{N_2O}]$$

$$= 176,553.45 \text{ tCO}_2\text{e}$$

## E.2. Calculation of project emissions or actual net GHG removals by sinks

>>

The emissions due to the project activity are composed of (a) the emission of not destroyed  $N_2O$  and (b) emissions from auxiliary hydrocarbons input resulting from the operation of the nitric acid plant.  $N_2O$  emissions not destroyed by the project activity are calculated based on the continuous measurement of the  $N_2O$  concentration in the tail gas of the nitric acid plant and the volume flow rate of the tail gas stream. The emissions related to the operation of the  $N_2O$  destruction facility are given by on-site emissions due to the hydrocarbons used as input to the nitric acid plant.

Project emissions are limited to the design capacity of the nitric acid plant. According to AM0028 version 3, the design capacity is measured in tons of nitric acid per year. The actual nitric acid production in the covered monitoring period does not exceed the design capacity.

$$PE_y = PE_{ND,y} + PE_{DF,y}$$

$$= PE_{ND,y} + HCE_{C,y} + HCE_{NC,y}$$

$PE_{ND,y}$ : Project emissions from  $N_2O$  not destroyed in year y ( $tCO_2\text{e/yr}$ ),

$PE_{DF,y}$ : Project emissions related to the operation of the destruction facility in year y ( $tCO_2\text{e/yr}$ )

$HCE_{C,y}$ : Converted hydrocarbon emissions in year y ( $tCO_2\text{e/yr}$ ),

$HCE_{NC,y}$ : Methane emissions in year y ( $tCO_2\text{e/yr}$ )

$$PE_{ND,y} = \sum_{i=1}^n [F_{TE,i} * CO_{N_2O,i} * M_i * GWP_{N_2O}]$$

i : Interval,

n : Number of intervals during the year (1/yr)

$F_{TE,i}$  : Volume flow rate at the exit of the destruction facility during interval i ( $Nm^3/h$ ),



$CO_{N_2O,i}$  :  $N_2O$  concentration in the tail gas of the  $N_2O$  destruction facility during interval  $i$  ( $tN_2O/Nm^3$ ),

$M_i$  : Length of measuring interval  $i$  (h),

$GWP_{N_2O}$  : Global warming potential of  $N_2O$ .

$$PE_{ND,y} = \sum_{i=1}^n [F_{TE,i} * CO_{N_2O,i} * M_i * GWP_{N_2O}]$$
$$= 20,620.37 \text{ tCO}_2\text{e}$$

In the event that the monitoring system is down, the highest measured by-product rate during the project activity will be applied for the downtime period for the campaign emission factor.

$$HCE_{C,y} = \rho_{NMHC} * Q_{NMHC,y} * OXID_{NMHC}/100 * EF_{NMHC} + \rho_{HNC} * Q_{HNC,y} * OXID_{CH_4}/100 * EF_{HNC}$$
$$= \rho_{NMHC} * Q_{NMHC,y} * EF_{NMHC}$$

$$HCE_{NC,y} = \rho_{HNC} * Q_{HNC,y} * (1 - OXID_{CH_4}/100) * GWP_{CH_4}$$
$$= \rho_{HNC} * Q_{HNC,y} * GWP_{CH_4}$$

$\rho_{NMHC}$  : Hydrocarbon (Non-methane part of the natural gas) density ( $tNMHC/Nm^3$ ),

$Q_{NMHC,y}$  : Hydrocarbon (Non-methane part of the natural gas) input in year  $y$  ( $Nm^3$ ),

$OXID_{NMHC}$  : Oxidation factor of hydrocarbon (Non-methane part of the natural gas) (%),

$EF_{NMHC}$  : Carbon emissions factor of hydrocarbon (Non-methane part of the natural gas) ( $tCO_2/tNMHC$ ),

$\rho_{HNC}$  : Methane (Methane part of the natural gas) density ( $tCH_4/Nm^3$ ),

$Q_{HNC,y}$  : Methane (Methane part of the natural gas) used in year  $y$  ( $Nm^3$ )

$EF_{HNC}$  : Carbon emissions factor of methane (Methane part of the natural gas) ( $tCO_2/tCH_4$ ),

$OXID_{CH_4}$  : Oxidation factor of methane (Methane part of the natural gas) (%), and

$GWP_{CH_4}$  : Global warming potential of methane.

For this project, fraction of Methane not converted is not being measured due to unreasonable costs. So, 0% is applied to  $OXID_{CH_4}$  and 100% is applied to  $OXID_{NMHC}$ .

$$HCE_{C,y} = \rho_{NMHC} * Q_{NMHC,y} * OXID_{NMHC}/100 * EF_{NMHC} + \rho_{HNC} * Q_{HNC,y} * OXID_{CH_4}/100 * EF_{HNC}$$
$$= \rho_{NMHC} * Q_{NMHC,y} * EF_{NMHC}$$
$$= 57.64 \text{ tCO}_2\text{e (non-methane)}$$

$$HCE_{NC,y} = \rho_{HNC} * Q_{HNC,y} * (1 - OXID_{CH_4}/100) * GWP_{CH_4}$$
$$= \rho_{HNC} * Q_{HNC,y} * GWP_{CH_4}$$
$$= 1,224.15 \text{ tCO}_2\text{e (methane)}$$

Therefore, total value of Project Emission is calculated as follows :

$$PE_y = PE_{ND,y} + PE_{DF,y}$$
$$= PE_{ND,y} + HCE_{C,y} + HCE_{NC,y}$$
$$= 20,620.37 + 57.64 + 1,224.15$$
$$= 21,902.16 \text{ tCO}_2\text{e}$$

### E.3. Calculation of leakage

>>

Additional power such as DeN<sub>2</sub>O unit running will be needed by the project implementation. The CO<sub>2</sub> emission related to the electricity consumption is insignificant, but monitored and counted as leakage in conservative manner.

$$LE_y = EI_{RCS,y} * EF_{RCS}$$

$EI_{RCS,y}$  : Additional electricity input for running the DeN<sub>2</sub>O unit (MWh/yr), and

$EF_{RCS}$  : Emissions factor for running the DeN<sub>2</sub>O unit.

$$LE_y = EI_{RCS,y} * EF_{RCS}$$

$$= 105.92 \text{ tCO}_2\text{e}$$

### E.4. Summary of calculation of emission reductions or net anthropogenic GHG removals by sinks

| Time Period | Baseline emissions or baseline net GHG removals by sinks (tCO <sub>2</sub> e) | Project emissions or actual net GHG removals by sinks (tCO <sub>2</sub> e) | Leakage (tCO <sub>2</sub> e) | Emission reductions or net anthropogenic GHG removals by sinks (tCO <sub>2</sub> e)  |
|-------------|---|--|------------------------------|--|
| Total       | 176,553.45 tCO <sub>2</sub> e   | 21,902.16 tCO <sub>2</sub> e   | 105.92 tCO <sub>2</sub> e    | 154,545.37 tCO <sub>2</sub> e<br>.....<br>The emission reduction amount for which Request for Issuance is applied for this monitoring period: 153,562 tCO <sub>2</sub> e (See Remarks below) |

Remarks: Actual emission reductions achieved in this monitoring period is 154,545 tCO<sub>2</sub>e.

The emission reduction amount for which Request for Issuance is applied for this monitoring period is claimed as 153,562 tCO<sub>2</sub>e, 983 tCO<sub>2</sub>e deducted from 154,545 tCO<sub>2</sub>e. This is because total emission reductions amount of the 4th monitoring period which has been already issued is 239,482 tCO<sub>2</sub>e where we applied the wrong Pg data (7.022~8.806 x 10<sup>5</sup> Pa.g). The revised emission reductions amount of the 4th monitoring period is 238,499 tCO<sub>2</sub>e where the right default value (7.071~8.767 x 10<sup>5</sup> Pa.g ) is applied. There was 983 tCO<sub>2</sub>e in excess. Therefore, for this monitoring period 153,562 tCO<sub>2</sub>e is applied for Request for Issuance.

Note: Such wrong Pg data were used for both 4th and 5th monitoring periods. But there is no effect on the 5th monitoring period.

### E.5. Comparison of actual emission reductions or net anthropogenic GHG removals by sinks with estimates in registered PDD

| Item  | Values estimated in ex-ante calculation of registered PDD | Actual values achieved during this monitoring period   |
|---|---|--|
| Emission reductions or GHG removals by sinks (tCO <sub>2</sub> e) | 281,272 tCO <sub>2</sub> e/year(365 days)                 | <p><b>153,562 tCO<sub>2</sub>e / 182 days</b><br/>(*)</p> <p>.....</p> <p>For reference:<br/>Actual emission reductions achieved during this monitoring period is ;</p> <p><b>154,545 tCO<sub>2</sub>e/182 days</b><br/><b>equivalent to</b><br/><b>309,939 tCO<sub>2</sub>e/year(365 days)</b><br/>.....</p> <p>The emission reduction amount for which Request for Issuance is applied for this monitoring period is claimed as 153,562 tCO<sub>2</sub>e, 983 tCO<sub>2</sub>e deducted from 154,545 tCO<sub>2</sub>e. (See Remarks (*) below)</p> |

Remarks (\*): Actual emission reductions achieved in this monitoring period is 154,545 tCO<sub>2</sub>e.

The emission reduction amount for which Request for Issuance is applied for this monitoring period is claimed as 153,562 tCO<sub>2</sub>e, 983 tCO<sub>2</sub>e deducted from 154,545 tCO<sub>2</sub>e. This is because total emission reductions amount of the 4th monitoring period which has been already issued is 239,482 tCO<sub>2</sub>e where we applied the wrong Pg data (7.022~8.806 x 10<sup>5</sup> Pa.g). The revised emission reductions amount of the 4th monitoring period is 238,499 tCO<sub>2</sub>e where the right default value (7.071~8.767 x 10<sup>5</sup> Pa.g ) is applied. There was 983 tCO<sub>2</sub>e in excess. Therefore, for this monitoring period 153,562 tCO<sub>2</sub>e is applied for Request for Issuance.

Note: Such wrong Pg data were used for both 4th and 5th monitoring periods. But there is no effect on the 5th monitoring period.

### E.6. Remarks on difference from estimated value in registered PDD

>>

Compared to PDD, value of emission reductions was increased around 10.19% from 281,272 tCO<sub>2</sub>e/year (365 days) to 309,939 tCO<sub>2</sub>e/year (365 days equivalent).

NOTE for avoiding any confusion:

PDD value: 281,272 tCO<sub>2</sub>e/year (365 days)

[For reference, it is equivalent to 140,251 tCO<sub>2</sub>e / 182 days.]

Actual emission reduction for this monitoring period (182 days) before deduction due to correction on 4<sup>th</sup> monitoring period: 154,545 tCO<sub>2</sub>e/year(182 days) equivalent to 309,939 tCO<sub>2</sub>e/year(365 days)



This is because of the following reasons:

(a) Increase of operation rate during this monitoring period as shown below :

|                   | 6 <sup>th</sup> monitoring period | Estimated values of PDD |
|-------------------|-----------------------------------|-------------------------|
| Monitoring Period | 182 days                          | 365 days                |
| Operation days    | 178 days + 18 hours               | 330 days                |
| Operation rate    | 98.21 %                           | 90.41 %                 |

and

(b) Increase of the nitric acid production rate during this monitoring period upto 97.5% of the designed capacity of production, which is about 7.5% higher than the expected production of PDD (97,020tHNO<sub>3</sub>/year : Page 8, Section A.4.4) where the value of inlet flow rate ( $F_{TI}$ ) is higher than PDD value.

= End =

#### History of the document

| Version   | Date                           | Nature of revision   |
|---|--------------------------------|--|
| 02.0  | EB 66<br>13 March 2012         | Revision required to ensure consistency with the "Guidelines for completing the monitoring report form" (EB 66, Annex 20). |
| 01  | EB 54, Annex 34<br>28 May 2010 | Initial adoption.  |
| <b>Decision Class:</b> Regulatory<br><b>Document Type:</b> Form<br><b>Business Function:</b> Issuance |                                |  |

## **Annex-1 Environmental issues**

### **1. Environmental Impacts**

According to the national Environmental Law in Korea, Environmental Impacts are :

Gaseous matter : There is no additional pollution. The  $\text{N}_2\text{O}$  destructed into harmless  $\text{N}_2$  and  $\text{O}_2$ .

Particular matter : There is no additional pollution.

Water matter : Not applicable. The destruction reaction occurs in gaseous phase.

Spent catalyst : The catalyst over its lifetime is recycled to get precious components and then reproduced to new catalyst. The catalyst has a long lifetime.

No transboundry impacts are expected.

### **2. $\text{N}_2\text{O}$ Regulation in Korea**

No national regulation for  $\text{N}_2\text{O}$  emission. We periodically visit the web-site of the concerned ministry in Korea and check the regulation. In case the regulation is updated, we will follow it accordingly.

By the way, Framework ACT Low Carbon Green Growth is not applicable for this Hanwha project activity.

### **3. $\text{NO}_x$ Regulation in Korea**

National regulation for  $\text{NO}_x$  emission is Clean Conservation Act (CCA) of the Republic of Korea.

According to CCA, currently,  $\text{NO}_x$  regulation requires to limit the emission below 200ppmv. We are periodically visiting the web-site of CCA and check the regulation. In case the regulation is updated, we will follow it accordingly. During the period of 01/01/2012 to 30/06/2012, the average value of  $\text{NO}_x$  is 47.94 ppmv the maximum value 142.06 ppmv (on 11/04/2012).

**Annex-2 Daily events, checking against baseline requirements****1. Operating Temperature**

The actual average daily operating temperature in the ammonia oxidation reactor was within the permitted range for all days covered by this monitoring report.

**2. Operating Pressure**

The actual average daily operating pressure in the ammonia oxidation reactor was within the permitted range for all days covered by this monitoring report except for one day of 15/02/ 2012.

**3. Composition of the Ammonia Oxidation Catalyst**

The composition of the ammonia oxidation catalyst is the same kind of catalyst composition already in operation prior to the start of the project activity.

**4. Ammonia Flow Rate to the Ammonia Oxidation Reactor**

The daily ammonia input to the ammonia oxidation reactor does not exceed the maximum permitted daily ammonia input.

**5. Production of Nitric Acid**

Production volume of Nitric Acid during the project period is 52,013.84tons, which is calculated as

---  $80,021.29 \text{ ton} \times 65/100 = 52,013.84\text{tons}$

--- 80,021.29 ton is the production mass of  $\text{HNO}_3$  which includes  $\text{H}_2\text{O}$  as 35%. Therefore we shall exclude  $\text{H}_2\text{O}$  and come to the pure  $\text{HNO}_3$  production volume. 52,013.84tons

whereas,  $P_{\text{product,max}}$  specified in the PDD, based on the manufacturer's specification is 107,100tons, which is  $306 [\text{HNO}_3/\text{day}] \times 350[\text{day}/\text{yr}]$ . Therefore, during the period, maximum production is calculated as  $306 \times 350 = 107,100\text{tons}$ .

The monitoring period is 182 days from 01/01/2012 to 30/06/2012.

The production volume of Nitric Acid during this period (182 days) is converted to 104,313.47 tons (365 days) where  $52,013.84 \text{ tons} \times 365 / 182$  as annual basis.

Thus actual production of 104,313.47tons is less than 107,100tons compared as annual basis.

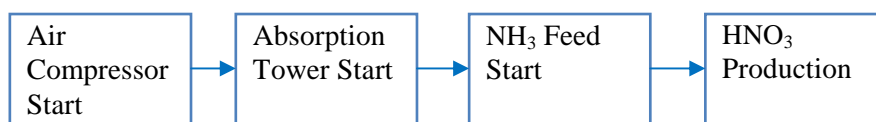
Daily basis production during the period was also within the permitted range, mentioned in the PDD.

Meantime, the operation of Nitric Acid Plant was stopped about 1 day and 1 hour during the following period as below (Time is rounded) :

**<Shutdown of the nitric acid plant during this monitoring period>**

|   | Downtime - Start |      | Downtime - End |      | Description of downtime reason     |
|---|------------------|------|----------------|------|------------------------------------|
|   | Date             | Time | Date           | Time |                                    |
| 1 | 12/03/2012       | 12   | 12/03/2012     | 16   | Malfunction of instrument (boiler) |
| 2 | 10/04/2012       | 05   | 11/04/2012     | 02   | Replacement of primary catalyst    |

(Remarks) The start-up process of the Nitric Acid Plant operation is as follows in brief.



So, the end time of shutdown is to present the air compressor's start to operate the Nitric Acid Plant.

On the other hand, the operation of DeN<sub>2</sub>O unit was stopped about 3 days and 6 hours during the following period as below (Time is rounded):

<Shutdown of DeN<sub>2</sub>O unit during this monitoring period>

|   | Downtime - Start |      | Downtime - End |      | Description of downtime reason  |
|---|------------------|------|----------------|------|---|
|   | Date             | Time | Date           | Time |   |
| 1 | 12/03/2012       | 13   | 13/03/2012     | 01   | Shutdown of DeN <sub>2</sub> O unit due to the malfunction of instrument (boiler) of the nitric acid plant  |
| 2 | 10/04/2012       | 04   | 11/04/2012     | 09   | Shutdown of DeN <sub>2</sub> O unit due to the replacement of the primary catalyst of the nitric acid plant |
| 3 | 16/04/2012       | 06   | 17/04/2012     | 19   | Rotary valve trip of DeN <sub>2</sub> O unit  |

## 6. Shutdown of De N<sub>2</sub>O unit

The De N<sub>2</sub>O unit was operated well to reduce the N<sub>2</sub>O gas from nitric acid plant, except for 3 days and 6 hours including the shutdowns and any abnormal situation of N<sub>2</sub>O concentration.



## Annex-3 Details of monitoring instrument

Information of monitoring instrument is as below :

(1) AOR  
instrument

Information of monitoring instrument ( 2012 / 6th Verification )

| No.                   | Application   | Tag No.   | Instrument Type                                | Range  | Accuracy              | Measuring Frequency | Report Frequency | Year of Manufacture | Information of Instrument   | Latest Cal./ Validity  | Information of Calibration                                  | Confirmation of Calibration   |
|-----------------------|---|-----------|--|--|-----------------------|---------------------|------------------|---------------------|---|--|---|---|
| <b>AOR Instrument</b> |   |           |  |  |                       |                     |                  |                     |   |  |   |   |
| 1                     | Actual ammonia input to oxidation reactor (tNH <sub>3</sub> /day) *reported in tons | 10-FT-502 | Differential Pressure Transmitter              | 0 - 1,600 mmH <sub>2</sub> O<br>Compensated Flow range<br>0- 6,000 Nm <sup>3</sup> /hr | ±0.065% of full scale | Continuous          | Daily            |                     | Manufacturer : Rosemount/Emerson<br>Model No. : 3051TG3A2B21A4M5E5S5Q4<br>Instrument No. : 01564836 | July 07 / 2011 -<br>Oct 06 / 2012  | Interval : 15 months<br>External Entity :<br>Hyupsung HISCO | Dual Installation (10-FT-503)   |
|                       |   | 10-PT-302 | Absolute Pressure Transmitter                  | 0 - 16 bar   | ±0.065% of full scale | Continuous          |                  |                     | Manufacturer : Rosemount/Emerson<br>Model No. : 3051TG3A2B21A4M5E5S5Q4<br>Instrument No. : 01624987 | July 07 / 2011 -<br>Oct 06 / 2012  | Interval : 15 months<br>External Entity :<br>Hyupsung HISCO | Dual Installation (10-PT-303)   |
|                       |   | 10-TT-102 | RTD(Pt100 ohm) Resistance Temperature Detector | 0 - 500 deg C  | ±0.55 deg C           | Continuous          |                  |                     | Manufacturer : WISE controls<br>Model No. : RZ21<br>Instrument No. : 04014993                       | July 08 / 2011 -<br>Oct 07 / 2012  | Interval : 15 months<br>External Entity :<br>Hyupsung HISCO | Dual Installation (10-TT-103)   |
| 2                     | Actual ammonia oxidation temperature  | 10-TT-115 | T/C (Type R) Thermocouple ((+)/PtRh - (-)/Pt)  | 0 - 1,200 deg C  | ±1.5 deg C            | Continuous          | Daily            | 2007                | Manufacturer : YOKOGAWA<br>Model No. : YTA 110<br>Instrument No. : C2E104013 502                    | July 08 / 2011 -<br>Oct 07 / 2012  | Interval : 15 months<br>External Entity :<br>Hyupsung HISCO | Dual Installation (10-TT-116)   |
| 3                     | Actual operating pressure   | 10-PT-304 | Absolute Pressure Transmitter                  | 0 - 16 bar   | ±0.065% of full scale | Continuous          | Daily            | 2007                | Manufacturer : Honeywell<br>Model No. : STG 944-E1G-00000-S2<br>Instrument No. : 0729 07062904012   | July 07 / 2011 -<br>Oct 06 / 2012  | Interval : 15 months<br>External Entity :<br>Hyupsung HISCO | Dual Installation (10-PT-305)   |
| 4                     | Ammonia oxidation catalyst  | -         | PtRh catalyst                                  | Composition<br>96% Pt, 5% Rh   |                       |                     |                  |                     | Manufacturer : Johnson Matthey  | Dec 7 / 2011 (Invoice No. : SD6919)<br>Apr 10 / 2012 (Invoice No. : SD67095) |   | Commercial invoice of cat. gauzes made available to verify the gauze composition. |
| 5                     | Plant output of Nitric Acid   | 10-FT-512 | Magnetic flow meter                            | 0 - 20 m <sup>3</sup> /hr  | ±0.675% of full scale | Continuous          | Daily            | 2007                | Manufacturer : Rosemount/Emerson<br>Model No. : 8705TPA020S1W0NDG3B3Q4<br>Instrument No. : 06011102 | Jun 29 / 2011 -<br>Sep 28 / 2012   | Interval : 15 months<br>External Entity :<br>FM Tech        |   |

(2) AMS  
instrument

|   |   |           |  |   |                       |            |        |                                    |   |  |  |   |
|---|---|-----------|--|---|-----------------------|------------|--------|------------------------------------|---|--|--|---|
| <b>AMS (Auto Measuring System) Instrument</b> |   |           |  |   |                       |            |        |                                    |   |  |  |   |
| 1   | N <sub>2</sub> O concentration at destruction facility inlet              | 10-AT-061 | NDIR N <sub>2</sub> O Analyzer   | 0 - 3,000 ppmv  | ±0.02% of full scale  | Continuous | Hourly | 2007                               | Manufacturer : ABB<br>Model No. : AQ2040 / Uras 26<br>Instrument No. : 3 346997.7                       | QAL2<br>Jan 25,2008~Jan 24,2011<br>Jan 20,2011~Jan 19,2014<br>AST<br>Jan 19,2010~Jan 18,2011<br>Jan 17,2012~Jan 16,2013<br>QAL3<br>Jun 23,2012~Jul 03,2012<br>other QAL3 tests within monitoring period were conducted every 10 days | QAL2<br>three years<br>AST<br>12 months<br>QAL3<br>every 10 days | QAL3 interval every 10 days<br>Main work :<br>1. Zero/Span check by standard gas<br>2. Leak check<br>3. Replacement of consummable<br>Gas Chromatography analysis : every 3 months        |
| 2   | Volume flow of tailgas at N <sub>2</sub> O destruction facility inlet     | 10-FT-561 | Differential Pressure Transmitter  | 0 - 275 mmH <sub>2</sub> O<br>Compensated Flow range<br>0- 60,000 Nm <sup>3</sup> /hr | ±0.075% of full scale | Continuous | Hourly | Probe : 2007<br>Transmitter : 2005 | Manufacturer : Honeywell<br>Model No. : STD924-E1H-00000-S2<br>Instrument No. : 0712 07030214001        | July 07 / 2011 -<br>Oct 06 / 2012  | Interval : 15 months<br>External Entity :<br>Hyupsung HISCO      | Confirmation of compensated flow<br>1. Interval : in 15 months<br>2. Air Tec(TUV Sud)<br>3. Compare with standard reference measurement(SRM)  |
|   |   | 10-PT-361 | Absolute Pressure Transmitter  | 0 - 16 bar  | ±0.065% of full scale | Continuous | Hourly | 2007                               | Manufacturer : Honeywell<br>Model No. : STG 944-E1G-00000-S1<br>Instrument No. : 0712 07030214004       | July 07 / 2011 -<br>Oct 06 / 2012  | Interval : 15 months<br>External Entity :<br>Hyupsung HISCO      |   |
|   |   | 10-TT-161 | RTD(Pt100 ohm) Resistance Temperature Detector   | 0 - 500 deg C   | ±0.3% of full scale   | Continuous |        | 2008                               | Manufacturer : WISE controls<br>Model No. : RZ21+MTM<br>Instrument No. : WS-7M139                       | July 15 / 2011 -<br>Oct 14 / 2012  | Interval : 15 months<br>External Entity :<br>Hyupsung HISCO      |   |
| 3   | N <sub>2</sub> O concentration at destruction facility outlet             | 10-AT-062 | NDIR N <sub>2</sub> O Analyzer   | 0 - 300 ppmv  | ±0.02% of full scale  | Continuous | Hourly | 2007                               | Manufacturer : ABB<br>Model No. : AQ2040 / Uras 26<br>Instrument No. : 3 346996.7                       | QAL2<br>Jan 25,2008~Jan 24,2011<br>Jan 20,2011~Jan 19,2014<br>AST<br>Jan 19,2010~Jan 18,2011<br>Jan 17,2012~Jan 16,2013<br>QAL3<br>Dec 26,2010~Jan 05,2011<br>other QAL3 tests within monitoring period were conducted every 10 days | QAL2<br>three years<br>AST<br>12 months<br>QAL3<br>every 10 days | Maintenance interval every 10 days<br>Main work :<br>1. Zero/Span check by standard gas<br>2. Leak check<br>3. Replacement of consummable<br>Gas Chromatography analysis : every 3 months |
| 4   | Volume flow of tailgas at N <sub>2</sub> O destruction facility outlet    | 10-FT-562 | Differential Pressure Transmitter  | 0 - 190 mmH <sub>2</sub> O<br>Compensated Flow range<br>0- 60,000 Nm <sup>3</sup> /hr | ±0.075% of full scale | Continuous | Hourly | Probe : 2007<br>Transmitter : 2005 | Manufacturer : Honeywell<br>Model No. : STD924-E1H-00000-S2<br>Instrument No. : 0712 07030214002        | July 07 / 2011 -<br>Oct 06 / 2012  | Interval : 15 months<br>External Entity :<br>Hyupsung HISCO      | Confirmation of compensated flow<br>1. Interval : in 15 months<br>2. Air Tec(TUV Sud)<br>3. Compare with standard reference measurement(SRM)  |
|   |   | 10-PT-362 | Absolute Pressure Transmitter  | - 0.1 - 0.1 bar   | ±0.065% of full scale | Continuous | Hourly | 2007                               | Manufacturer : Honeywell<br>Model No. : STG 944-E1G-00000-S1<br>Instrument No. : 9853 0000201004        | July 07 / 2011 -<br>Oct 06 / 2012  | Interval : 15 months<br>External Entity :<br>Hyupsung HISCO      |   |
|   |   | 10-TT-162 | RTD(Pt100 ohm) Resistance Temperature Detector   | 0 - 500 deg C   | ±0.3% of full scale   | Continuous |        | 2008                               | Manufacturer : WISE controls<br>Model No. : RZ21+MTM<br>Instrument No. : WS-7M140                       | July 08 / 2011 -<br>Oct 07 / 2012  | Interval : 15 months<br>External Entity :<br>Hyupsung HISCO      |   |
| 5   | Volume flow of hydrocarbon into the N <sub>2</sub> O destruction facility | 10-FT-563 | Differential Pressure Transmitter with pressure/temperature application for compensation | 0 - 2,500 in H <sub>2</sub> O<br>Compensated Flow range<br>0- 100 Nm <sup>3</sup> /hr | ±0.78% of full scale  | Continuous | Hourly | 2011                               | Manufacturer : Rosemount/Emerson<br>Model No : 3095MFC3020N040T32BA1A04EM5<br>Instrument No. : 02357885 | May 12 / 2011 -<br>Aug 11 / 2012   | Interval : 15 months<br>External Entity :<br>Hyupsung HISCO      | Dual measurement (Kyungdong citygas company)  |

\* Hydrocarbon were supplied as the regulated pressure (0.45 bar g) and nearly constant temperature by Kyungdong citygas company.